

**AIR QUALITY IMPACT ASSESSMENT FOR
THE 407 TRANSITWAY
(HIGHWAY 400 TO KENNEDY ROAD)**

Prepared for:

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L4B 3N4

November 2010

Printed on Recycled Paper Containing Post-Consumer Fibre




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EXECUTIVE SUMMARY

In the future, additional public transportation will be required to meet the increasing demands of population growth in the Greater Toronto Area. The addition of a bus rapid transit system in York Region will help to alleviate any anticipated pressure that current road and public transit systems will face in the future as a result of increased growth.

A Transit Project Assessment based on the “*Transit Projects and Greater Toronto Transportation Authority Undertakings, Ontario Regulation 231/08*”, is being undertaken to study the implementation of a 23 kilometre bus rapid transit (BRT) system (the 407 Transitway) that will be grade-separated and parallel to Highway 407 between Highway 400 and Kennedy Road in the municipalities of Vaughan, Richmond Hill and Markham, Ontario. The BRT system will consist of a two lane roadway occupied solely by buses. This air quality impact assessment examines existing and future air quality and climate change impacts based on the preferred alternative route of the undertaking.

Comparison of Existing Conditions with Future Scenarios

For both future scenarios with and without the 407 Transitway (2031), the study identifies that compared to existing conditions (2008), air quality will slightly improve for gaseous pollutants due to newer engine technologies and fuels, despite predicted increases in traffic resulting from population growth. However, air quality will deteriorate for particulate based compounds due to:

- increased traffic flow on Highway 407 resulting from population growth in the future and/or,
- increased road silt accumulation as a result of low bus volumes/heavier vehicles on the 407 Transitway.

Additionally, the pollutant burden of carbon dioxide equivalent (CO_{2e}) is expected to increase in the future as a result of increased traffic volumes due to population growth.

Comparison of Future Scenarios

The study shows that within the study area, when compared to the future no-build scenario (2031), adding the 407 Transitway will result in:

- negligible changes in gaseous pollutant concentrations and greenhouse gases (GHGs) throughout the study area;
- a slight increase in PM_{2.5} (particulate matter less than 2.5 µm in diameter) concentrations, particularly at receptors whose distance from a roadway (emission source) decreases with the addition of the Transitway;

- an increase in total suspended particulate (TSP) and PM₁₀ (particulate matter less than 10 µm in diameter) concentrations throughout the study area;
- approximately a 2% to 40% increase in TSP and PM₁₀ concentrations at sensitive receptor locations adjacent to the 407 Transitway; and,
- negligible changes in gaseous and particulate matter concentrations when station parking lot and passenger pick-up and drop-off (PPUDO) emissions are considered.

Recommended Mitigation

Mitigative measures to reduce the impact of road dust at nearby sensitive areas are recommended where possible. Barriers (i.e., trees/shrubs, or where planned for safety and/or noise issues solid barriers) located along the 407 Transitway at sensitive receptor locations will act as screens and reduce the particulate matter flowing horizontally from the roadway. When recommended mitigation measures are considered it is expected that particulate matter concentrations at sensitive receptor locations will be within MOE standards. As a result, it is recommended that mitigation measures be implemented for the following five residential/sensitive receptor locations:

- Residences on Hartley Court; north of the Transitway, west of the GO-Barrie rail line;
- Residences on Yellowwood Circle; north of Transitway, east of Dufferin Street;
- Residences on Sassafras Circle; Daniel Reaman Crescent and Lander Crescent; north of Transitway, east of Langstaff Road;
- Residences on Langstaff Road West; west of Transitway; and,
- St. Robert Catholic High School, south of Transitway, east of Leslie Street.

Mitigation through the planting of trees and shrubs has been considered and incorporated into the preliminary landscape design.

In addition, particulate matter emission estimates may have been overly conservative. Recently (June 2010), the U.S. EPA published draft guidance with an updated methodology for estimating road dust emissions (U.S. EPA, 2010). The revised methodology appears to give significantly lower levels of emissions compared to the U.S. EPA 2006 methods used in this assessment. The draft section proposing the revised calculation methodology as well as supporting documentation can be found at <http://www.epa.gov/ttn/chief/ap42/ch13/index.html>.

If during the detailed design phase of the project the proposed U.S. EPA methods become standard practice, the above recommendations to reduce the impact of particulate matter to nearby sensitive areas should be revisited.

Conservative Nature of Assessment

The air quality impact assessment is considered to be conservative based on the following:

- Industry standard conservative 90th percentile background monitoring values were added to model predicted contaminant concentrations;
- Background monitoring data for PM₁₀ and TSP was not available, therefore, the conservative assumption was made that PM₁₀ background concentrations are twice PM_{2.5} and TSP background concentrations are twice PM₁₀;
- The future with Transitway scenario assumes no reduction in vehicle traffic on Highway 407, however, based on discussions with the MTO and Delcan, it is reasonable to assume that the introduction of the 407 Transitway into the study area will reduce the number of vehicles present within the transportation corridor (i.e., Highway 7 and other regional roads); and,
- Recently (June 2010), the U.S. EPA published draft guidance with an updated methodology for estimating road dust emissions (U.S. EPA, 2010). The revised methodology appears to give significantly lower levels of emissions compared to the U.S. EPA 2006 methods used in this assessment.

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1.0 INTRODUCTION

1.1 PROJECT DESCRIPTION

A Transit Project Assessment based on the “*Transit Projects and Greater Toronto Transportation Authority Undertakings, Ontario Regulation 231/08*”, is being undertaken to study the implementation of a 23 kilometre bus rapid transit (BRT) system (the 407 Transitway) that will be grade-separated and parallel to Highway 407 between Highway 400 and Kennedy Road in the municipalities of Vaughan, Richmond Hill and Markham, Ontario. The Transitway will consist of a two lane roadway occupied solely by buses.

SENES Consultants Limited (SENES) was retained by LGL Limited (LGL) to complete a project-specific Air Quality Impact Assessment (AQIA) to establish the air quality effects that may arise due to the implementation of the undertaking. The preferred route of a BRT system along the Highway 407 right-of-way from Highway 400 to Kennedy Road developed by Delcan Corporation was used for this AQIA.

1.2 STUDY AREA

The study area is approximately 500 metres on either side of Highway 407 between Highway 400 and Kennedy Road. For air quality studies, however, physical boundaries have no meaning since air flows over and/or around everything. As a result, the air quality boundaries can be set arbitrarily to fit the important aspects of any project. Where possible, the project boundaries were used.

1.3 AIR QUALITY IMPACTS OF THE PROJECT ON THE ENVIRONMENT

Air quality manifests itself in two broad ways – through air pollutant concentrations in the air we breathe and through deposition of pollutants to surfaces. Air quality is usually assessed by examining the pollutants that are linked with a particular project. In this case, the pollutants of concern are:

- dust (particles of sizes smaller than 44 µm): three specific size ranges are important – Total Suspended Particulate (TSP), which are those particles approximately 44 µm in diameter and smaller; PM₁₀, which are those particles 10 µm in diameter and smaller; and, PM_{2.5}, which are those particles 2.5 µm in diameter and smaller. Dust is entrained in the air by the action of the wind, the wheels of a vehicle on road surfaces, deterioration of vehicle equipment (i.e., brake and tire wear) and directly from the exhaust of engines;
- carbon monoxide (CO): a gas formed by the incomplete combustion of carbon-based fuels that is emitted in vehicle exhaust;

- nitrogen dioxides (NO_x): gases formed when anything is burned in air that are emitted in vehicle exhaust;
- the following Volatile Organic Compounds (VOCs) are typically of concern in transportation projects: 1,3-butadiene, acetaldehyde, acrolein, benzene and formaldehyde which are primarily emitted in vehicle exhaust, but are also present in fuel vapour that escapes from the fuel tank; and,
- Greenhouse Gases (GHGs): carbon dioxide (CO₂), nitrous oxide (N₂O) and methane (CH₄) are emitted when any fuel is burned.

2.0 EXISTING ENVIRONMENTAL CONDITIONS

2.1 CLIMATE AND METEOROLOGICAL DATA

2.1.1 Introduction

Throughout the lower atmosphere (the troposphere), meteorological parameters vary widely in both time and space. For instance, the heat balance at the surface is disturbed when a single cloud moves across the sun.

Meteorology (weather) is the key to understanding air quality. The essential relationship between meteorology and atmospheric dispersion involves the wind in the broadest sense of the term. Wind fluctuations over a very wide range of time and space scales accomplish dispersion and strongly influence other processes associated with it.

In general, the wind flow over the earth is induced by large-scale pressure variations commonly shown on synoptic weather charts. The intensity of these pressure systems and their normal positions or trajectories, determines the general distribution of winds over a given area. Within this large-scale framework, there are many small-scale factors (e.g., local topography and obstacles) that influence the details of air movement in both the vertical and horizontal directions. For most air quality problems, it is the combination of elements of the broad and the detailed patterns that is important.

These patterns dictate where and how far from a source pollutants will travel. The characterization of the existing climatological (long term weather) conditions in the vicinity of a source of pollutants is, therefore, a critical aspect of assessing air quality.

The key meteorological parameters that must be taken into account are wind, temperature and atmospheric structure. The importance of these parameters is outlined below.

2.1.2 Wind

Wind has two significant components – direction and speed.

Direction

Wind direction is reported as the direction from which the wind blows and is based on surface (10 metre) observations. Over the course of a year, wind usually blows from all directions, but with varying frequencies. Certain directions occur more frequently than others. These are known as the prevailing wind directions.

A wind rose is simply a circular representation of the frequencies of each wind direction and/or speed over some period of time (usually a year or longer). Figure 2.1 presents a wind rose for Pearson International Airport (the closest representative meteorological station to the study area) for the years 1992-1996. Figure 2.1 is derived from the current Ontario Ministry of Environment default five year meteorological dataset for the Region of York-Durham (MOE, 2007), which is considered to be representative of existing conditions within the 407 Transitway study area. Wind direction in the area varies considerably over the period. On average, the prevailing winds are from the north-northwest and less often from the west.

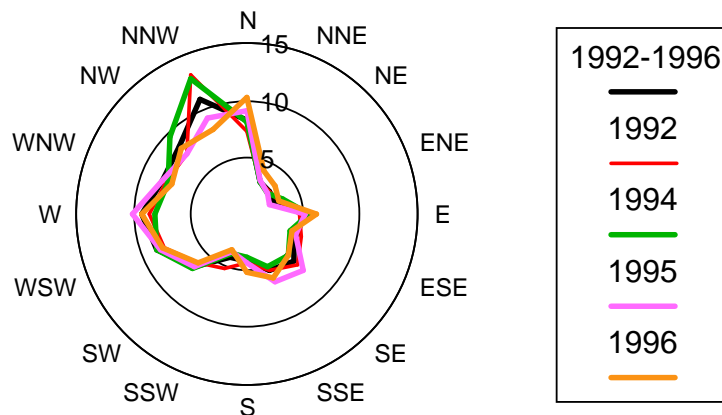
Speed

The distribution of average wind speed at the Pearson International Airport station is also presented in Figure 2.1. The average wind speed, based on the 1992-1996 period, is approximately 4 m/s (~14 km/hour).

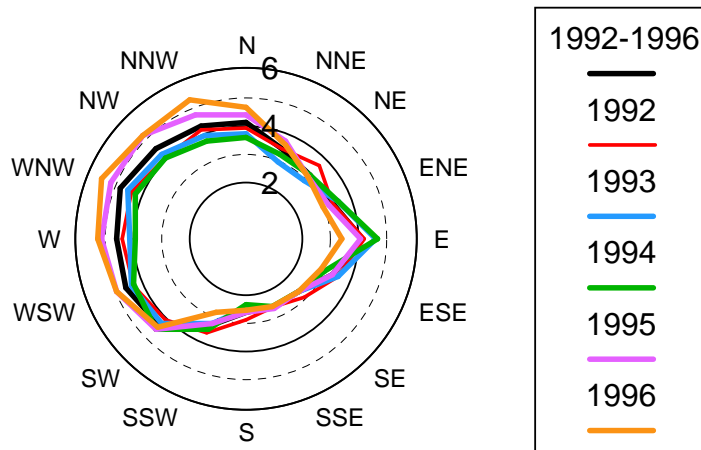
The concentration of any pollutant in the air decreases with increasing wind speed as a result of dilution. When wind speeds are high there is good dispersion of gases and particles throughout the atmosphere, but more potential for re-suspension of surface dust. When wind speeds are near zero, dispersion is poor and local circulations can lead to very high pollutant concentrations near the surface. Wind speed also increases with height as surface friction decreases. This leads to better dispersion from smokestacks since the wind speed is higher aloft. The lower wind speeds near the ground are the driving force behind the initial mixing and transport of pollutants from vehicles.

Figure 2.1 Wind Rose and Wind Speed for Pearson International Airport

Wind Direction Frequency (%) (wind from)



Average Wind Speed (m/s)



2.1.3 Temperature

There are two key temperature effects that influence air quality – temperature near the surface and temperature aloft.

Temperature near the Surface

Temperature near the surface can greatly affect the dispersion of particulate matter. When it is hot, the surface can dry out, making particulate matter available to be picked up by the wind. Cool temperatures, on the other hand, enable the surface to retain moisture longer, thereby binding the dust particles together and reducing windblown dust. The study area is typical of the Southern Ontario Great Lakes Region with relatively cool spring and fall seasons, hot and humid summers and cold, wet winters.

Temperature Aloft

The change in temperature vertically determines the stability of the atmosphere which is a key parameter controlling the dispersion of gases and particles.

Atmospheric stability is an inherent feature of the vertical temperature structure. It is a measure of the atmosphere's ability to mix pollutants. A stable atmosphere has little vertical motion (is less turbulent) and cannot disperse pollutants as well as a more turbulent, unstable atmosphere. A number of classification schemes have been developed for describing stability classes.

An atmospheric stability classification scheme, developed by Pasquill-Gifford and modified by Turner, is now widely used. Six atmospheric stability classes, A through F, are defined using commonly measured meteorological parameters including wind speed, temperature, lapse rate (rate of change of temperature with height), degree of solar insolation (the strength of the sun at a particular time of day) and the amount of cloud cover.

Class A is the most unstable class, while class F is the most stable. The intermediate Class D is described as a neutral atmosphere. Classes E and F represent progressively more stable conditions, and Classes C, B and A progressively more unstable conditions, respectively. A statistical summary of the atmospheric stability was generated based on the results from a United States Environmental Protection Agency (U.S. EPA) regulatory meteorological pre-processor [PCRAMMET] and applied to the data from the Toronto Pearson Airport station for the period 1992-1996. At this station, neutral stability D (neutral) occurs approximately 53% of the time, C (near neutral) conditions occur about 11% of the time, and stable conditions (E, F) occur about 30% of the time. Stable conditions can produce higher concentrations near the ground because of reduced vertical mixing. Unstable conditions (A, B) occur approximately 5% of the time.

2.1.4 Atmospheric Structure

The structure of the atmosphere is also defined by the vertical temperature change in another fundamental way – by setting a limit on the vertical distance through which pollutants can mix. This vertical extent through which a plume of pollutants can be mixed is called the “mixing height”. With a higher mixing height there is a larger volume of air available within which the pollutants can mix, producing lower concentrations. With a lower mixing height, a surface plume from a vehicle would be trapped close to the ground, resulting in higher concentrations.

The concept of mixing height is founded on the principle that heat transferred to the atmosphere at the earth's surface results in convection (vigorous vertical mixing) and the establishment of a dry-adiabatic lapse rate (Holzworth, 1967). In general, mixing height does not have much effect on modelled annual and 24-hour average ground level concentrations (Young and Radonjic, 1993). For 1-hour concentrations, however, mixing height can be very important. The use of variable mixing heights, that are as close as possible to the actual conditions, improves the ability of a model to accurately predict downwind concentrations.

Mixing height is calculated from the vertical temperature profile measured by weather balloon ascents. The distance between stations that release weather balloons is approximately 300 kilometres. The closest upper air station to Toronto is Buffalo, NY. Because mixing height is a regional parameter, the data measured in Buffalo is representative of conditions over Toronto.

2.2 AIR QUALITY STANDARDS

Several measures are used to describe impacts from roadways. Those used in this assessment are as follows:

- Total Suspended Particulate (TSP);
- Fine Particulate Matter less than 10 and 2.5 μm in diameter (PM_{10} and $\text{PM}_{2.5}$);
- Nitrogen Oxides (NO_x) with a discussion of NO_2 and NO components;
- Carbon Monoxide (CO);
- Volatile Organic Compounds (VOCs: 1,3-butadiene, acetaldehyde, acrolein, benzene and formaldehyde); and,
- Greenhouse Gases (GHGs: CO_2 , N_2O and CH_4).

The contaminants listed above and relevant criteria are discussed in some detail in the remainder of this section.

2.2.1 Total Suspended Particulate (TSP)

Total Suspended Particulate (TSP) is often used to characterize air quality near a dust source. TSP is measured with a high-volume (Hi-Vol) sampler over 24-hours and consists of particles less than 44 µm in diameter. An annual average is calculated as the geometric mean of samples measured every six days.

The provincial ambient air quality criteria for TSP are summarized in Table 2.1.

Table 2.1 MOE Ambient Air Quality Criteria for TSP

Pollutant	Averaging Period	Ambient Air Quality Criteria
Total Suspended Particulate (TSP)	24-hours	120 µg/m ³
	1 year*	60 µg/m ³

* Geometric Mean

The ambient TSP criteria were set to prevent a reduction in visibility. Particles suspended in the atmosphere reduce visibility or the visual range by reducing the contrast between an object being viewed and its background. This reduction is a result of particles scattering or absorbing light coming from both the object and its background, and from particles scattering light into the line of sight (Robinson, 1977). Particles with a radius of 0.1 to 1.0 µm are most effective at reducing visibility. In a rural area where TSP levels are on the order of 30 µg/m³, the visibility would be about 40 km. At 150 µg/m³, a common urban concentration, the range would be reduced to about 8 km. The MOE 24-hour criterion of 120 µg/m³ is based on a visual range of about 10 km.

The importance of TSP as an indicator of air quality is generally decreasing. Impacts from elevated TSP concentrations are extremely localized and are generally nuisance based rather than health based. Consequently, more emphasis is being placed on the finer particulate fractions, namely PM₁₀ and PM_{2.5}.

2.2.2 Fine Particulate Matter - PM₁₀ and PM_{2.5}

Many studies over the past few years have indicated that fine particulate matter (PM₁₀ and PM_{2.5}) in the air is associated with various adverse health effects in people who already have compromised respiratory systems and suffer from asthma, chronic pneumonia and cardiovascular problems. However, the available studies have not been able to link the adverse health effects in such people to any one component of the pollution mix. Fine particulate matter is a mixture of chemically and physically diverse dusts and droplets, and some of these components may be important in determining the effects of PM₁₀ and PM_{2.5} on health.

The current 24-hour suggested regulatory limits for fine particulate matter are presented in Table 2.2 as follows:

Table 2.2 Ambient Air Quality Criteria for PM₁₀ and PM_{2.5}

Pollutant	Averaging Period	Guideline Level	Ambient Air Quality Criteria
PM ₁₀	24-hours	Ontario Interim	50 µg/m ³
PM _{2.5}	24-hours	Proposed CWS (by 2010)	30 µg/m ³ *

CWS = Canada Wide Standard

*Compliance is measured as the 98th percentile over three years

2.2.3 Criteria Air Contaminants (NO_x, CO)

Criteria Air Contaminants (CACs), including nitrogen oxides and carbon monoxide are common air pollutants that are typically released into the air by activities such as fossil fuel combustion.

Nitrogen oxides (NO_x) is the generic term for a group of highly reactive gases, all of which contain nitrogen and oxygen in varying ratios. Nitrogen dioxide (NO₂) is the primary component of concern in NO_x. NO₂ is a reddish brown gas with a pungent odour, which upon reaction with other atmospheric compounds, becomes a major contributor to smog, acid rain, inhalable particulates and reduced visibility. NO₂ also plays a major role in atmospheric reactions that produce ground level ozone. Man-made sources of NO_x include all fossil fuel combustion such as heating buildings, commercial and industrial operations, etc. While motor vehicle exhaust is a significant source of NO_x, only a small percentage is emitted as NO₂ directly from the tailpipe (X. Yao et al, 2005). The main component of NO_x from tailpipes is NO which reacts in the atmosphere over time and distance to form NO₂. The rate of reaction is influenced by many factors including initial concentration, sunlight, ozone concentrations and others.

Carbon monoxide (CO) is a colourless, odourless gas that is produced as a result of incomplete oxidation of carbon during combustion. According to the MOE, in Ontario, over 60% of CO produced is from the transportation sector (MOE, 1999). The remainder is the result of other sources of fossil fuel combustion such as heating buildings, commercial and industrial operations, etc.

The provincial ambient air quality criteria for NO_x and CO are shown in Table 2.3.

Table 2.3 MOE Ambient Air Quality Criteria for Criteria Air Contaminants

Pollutant	CAS No.	Ambient Air Quality Criteria (AAQC)			
		Annual ($\mu\text{g}/\text{m}^3$)	24-hour ($\mu\text{g}/\text{m}^3$)	8-hour ($\mu\text{g}/\text{m}^3$)	1-hour ($\mu\text{g}/\text{m}^3$)
Nitrogen Oxides	10102-44-0	NS	200	NS	400
Carbon Monoxide	630-08-0	NS	15,700	36,200	NS

NS – No Standard.

2.2.4 Volatile Organic Compounds

Volatile Organic Compounds (VOCs) are defined technically as organic compounds having a saturation vapour pressure greater than 0.1 mm of mercury at 25°C and standard atmospheric pressure. Certain VOCs warrant special concern because they are capable of being transported very long distances in the atmosphere and play an important role in the formation of ground-level ozone and fine particles. Almost all VOCs contribute to ground-level ozone, and most do not break down in the troposphere during photochemical reactions.

VOCs are emitted into the atmosphere from a variety of sources, including vehicles, fossil fuel combustion, steel-making, petroleum refining, fuel refilling, industrial and residential solvent use, paint application, manufacturing of synthetic materials (e.g., plastics, carpets), food processing, agricultural activities and wood processing and burning.

The U.S. Environmental Protection Agency (U.S. EPA) has identified over 600 air pollutants present in gasoline/diesel exhaust of which 188 are considered to be hazardous air pollutants (HAPs) under the U.S. Clean Air Act (U.S. EPA, 2006a). The U.S. EPA has evaluated this list of HAPs and has identified 21 Mobile Source Air Toxics (MSATs) of which 6 are considered to be priority substances (U.S. EPA, 2000). The priority list of MSATs includes five (5) VOCs (acrolein, benzene, formaldehyde, acetaldehyde and 1,3-butadiene) with the other MSAT being particulate matter. Accordingly, acrolein, benzene, formaldehyde, acetaldehyde and 1,3-butadiene are the VOCs being considered in this study.

The provincial ambient air quality criteria for VOCs are shown in Table 2.4.

Table 2.4 Air Quality Criteria for VOCs

Pollutant	CAS No.	Averaging Period	Ambient Air Quality Criteria
Benzene ^a	71-43-2	24-hour	2.3 µg/m ³
Formaldehyde	50-00-0	24-hour	65 µg/m ³
Acetaldehyde	75-07-0	½-hour and 24-hour	500 µg/m ³
Acrolein ^b	107-02-8	1-hour	4.5 µg/m ³
		24-hour	0.4 µg/m ³
1,3-butadiene ^c	106-99-0	24-hour	10 µg/m ³

a. Proposed MOE AAQC for benzene (EBR Registry No. 010-7186; July, 2009)

b. Acrolein AAQC revised December, 2009 (EBR Registry No. 010-6241)

c. Proposed MOE AAQC for 1,3-butadiene (EBR Registry No. 010-6214; July, 2009)

Source: Ontario's Ambient Air Quality Criteria (February 2008)

Many VOCs are odorous compounds at higher concentrations. Odours from vehicular exhaust are generally acknowledged to be associated with the presence of aldehyde constituents, other minor volatile organic compounds and nitrogen oxides in the exhaust. The aldehydes are largely comprised of formaldehyde, acrolein and acetaldehyde. Table 2.5 indicates the pollutants considered in this study that contribute to odour emissions, together with their associated odour threshold. By definition, the odour threshold of a particular compound is the concentration at which 50% of the population can just detect the presence of an odour under laboratory conditions.

Table 2.5 Considered Constituents of Vehicular Odour Emissions

Pollutant	Odour Threshold (µg/m³)
Nitrogen Dioxide	230
Formaldehyde	300
Benzene	108,000
Acetaldehyde	120
1, 3 Butadiene	2,400
Acrolein	4,100

Source: American Industrial Hygiene Association, 1989.

2.2.5 Greenhouse Gases

Greenhouse Gases (GHGs) absorb and emit radiation within the thermal infrared range, which is the process regarded as the fundamental cause of the non-natural part of the “greenhouse effect.” Greenhouse gases include carbon dioxide (CO₂), methane (CH₄), nitrous oxide (N₂O), ozone and chlorofluorocarbons (CFCs). Fossil fuel combustion is the main source of GHG emissions

related to this project, which results in emissions of methane (CH₄), carbon dioxide (CO₂) and nitrous oxide (N₂O).

For a given mixture of different GHGs, carbon dioxide equivalent (CO_{2e}) is the unit of measure used to describe the amount of CO₂ that would have the same global warming potential as CO₂ when measured over a time period (typically a 100 year period). The carbon dioxide equivalency for a gas is calculated by multiplying the mass (of the gas) by its global warming potential. For example, the global warming potential for CH₄ over 100 years is 25 and for N₂O is 298 (IPPC, 2007). This means that the emission of 1 tonne of CH₄ is equivalent to the emission of 25 tonnes of CO₂, and the emission of 1 tonne of N₂O is equivalent to the emission of 298 tonnes of CO₂.

2.3 EXISTING AIR QUALITY

2.3.1 Historical Ambient Monitoring Data

The Ontario Ministry of the Environment (MOE) measures air contaminants at various locations throughout Ontario, and reports on the state of Ontario's air quality on an annual basis. To assess the current air quality in the study area, historical air quality monitoring data from the closest MOE monitoring stations to the study area were considered. Tables 2.6 through 2.8 outline the most recent measurement history (2004 to 2008) for NO_x, PM_{2.5} and CO and present a summary of the data in terms of mean, 90th percentile and 1-hour maximum and 24-hour maximum values (8 hour maximum for CO). The MOE Toronto North (34020) monitoring station located on Hendon Avenue near Yonge and Finch was the closest station having available NO_x and PM_{2.5} data. The MOE Toronto Downtown (31103) monitoring station located near the intersection of Bay and Wellesley was the closest station measuring CO. PM, PM₁₀, VOCs and GHGs have not been measured at these locations during the past five years.

The tables indicate that historically, CO has been well within the accepted standards. NO_x and PM_{2.5} have exceeded the standard from time to time, sometimes by as much as double the allowable concentration (usually during smog events which are regional in nature). In summary, the historical data outlines a typical urban/suburban airshed with occasional smog periods during which air quality is compromised. In Ontario, the smog season occurs from May through September, with most events of compromised air quality occurring as a result of transboundary pollution from polluted air masses that flow northward from the Ohio Valley in the United States.

Table 2.6 Recent Ambient Air Quality for PM_{2.5}

Station ID	Station Location	Averaging Time	PM _{2.5} (µg/m ³)					
			AAQC	Year				
				2004	2005	2006	2007	2008
#34020	Toronto North	Annual Background		9.0	10.0	9.0	9.0	9.0
		24-hr Mean	-	7.7	9.4	7.6	7.8	7.2
		24-hr 90 th Percentile	-	17.2	23.7	16	16.4	14.4
		1-hr Maximum	-	69	65	52	60	54
		24-hr Maximum	30*	43	51	36	40	35
		No. of Times above proposed CSW	-	12	19	2	7	1
Average		24-hr 90 th Percentile	-	17.5				

ND = No Data

*Compliance is measured as the 98th percentile over three years, therefore 10 exceedances (1% of 365x3) of the 24-hr criteria is within compliance for three years or nominally 3 exceedances per year on average for the three most recent monitoring years.

Note: All values are calculated from hourly data available from the <http://www.airqualityontario.ca/> website.

Table 2.7 Recent Ambient Air Quality Monitoring for Nitrogen Oxides

Station ID	Station Location	Averaging Time	Nitrogen Oxides (µg/m³)					
			AAQC	Year				
				2004	2005	2006	2007	2008
#34020	Toronto North	24-hr Mean	-	53	57	52	47	46
		1-hr 90 th Percentile	-	115	119	111	100	96
		24-hr 90 th Percentile	-	102	99	95	87	84
		1-hr Maximum	400	642	803	482	657	476
		24-hr Maximum	200	260	300	253	188	210
		No. of Times above 1-hr AAQC	-	18	26	11	9	9
		No. of Times above 24-hr AAQC	-	2	5	3	0	1
Average		1-hr 90 th Percentile	-	108.2				
		24-hr 90 th Percentile	-	93.4				

ND = No Data

Note: All values are calculated from hourly data available from the <http://www.airqualityontario.ca/> website.

Table 2.8 Recent Ambient Air Quality Monitoring for Carbon Monoxide

Station ID	Station Location	Averaging Time	Carbon Monoxide (µg/m³)					
			AAQC	Year				
				2004	2005	2006	2007	2008
#31103	Toronto Downtown	1-hr 90 th Percentile	-	607	630	584	412	229
		8-hr 90 th Percentile	-	591	613	573	424	218
		1-hr Maximum	36,200	2176	1821	1672	1947	1065
		8-hr Maximum	15,700	1431	1317	1168	1237	553
		No. of Times above 1-hr AAQC	-	0	0	0	0	0
		No. of Times above 8-hr AAQC	-	0	0	0	0	0
Average		1-hr 90 th Percentile	-	492.4				
		8-hr 90 th Percentile	-	483.6				

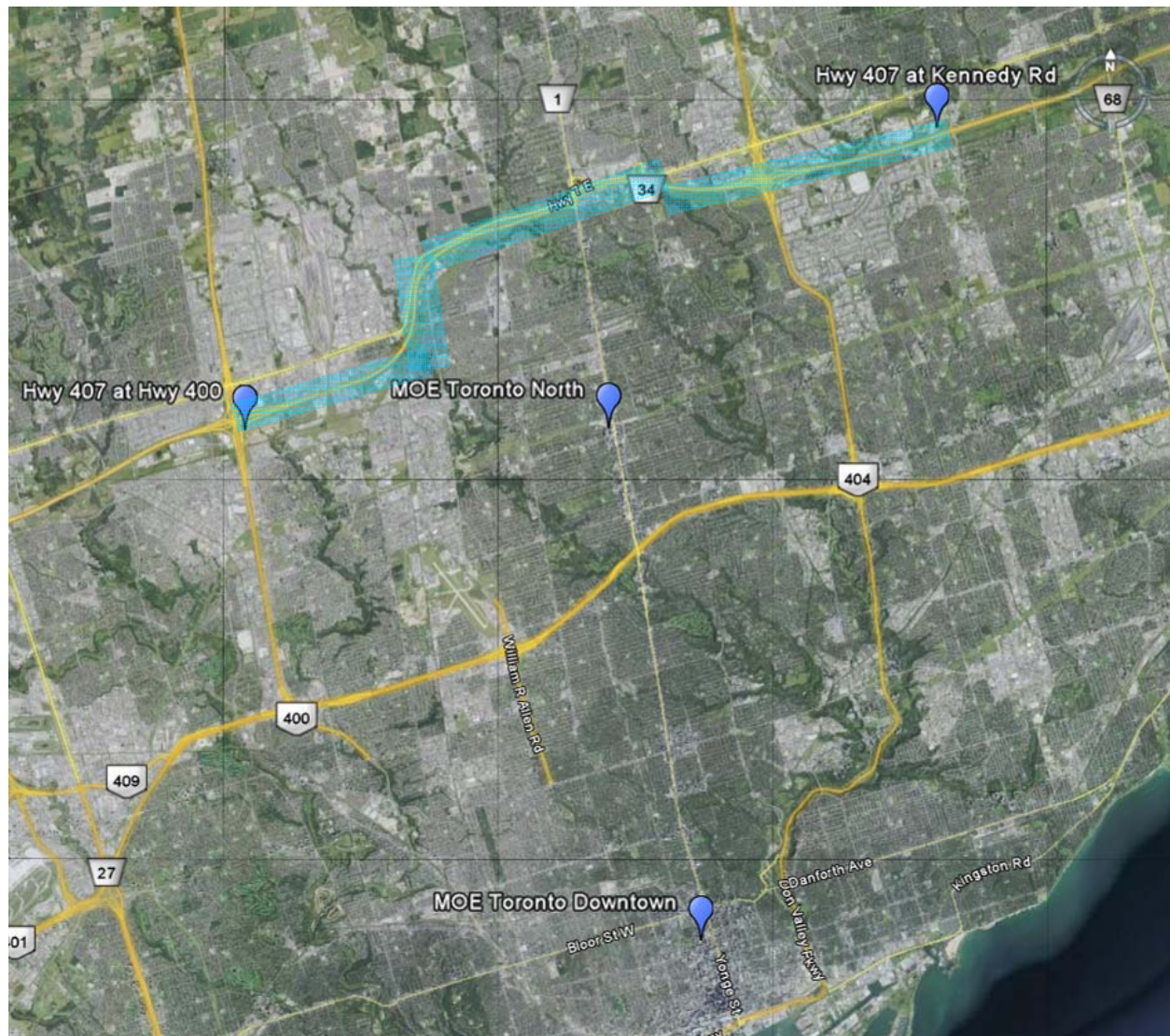
ND = No Data

Note: All values are calculated from hourly data available from the <http://www.airqualityontario.ca/> website.

All measured 8-hour values are based on 'rolling' 8-hr periods.

Figure 2.2 presents the location of the MOE air quality monitoring locations considered for this study. The approximate extent of the study area is shaded blue for reference.

Figure 2.2 MOE Toronto North and Downtown Monitoring Stations



2.4 BACKGROUND CONCENTRATIONS

Ambient background concentrations used in air quality assessments should represent the contribution from sources such as upwind industrial facilities, other roadways, transboundary pollution, etc. It is important to add background contaminant concentrations to modelled vehicle emission concentrations in order to assess the combined effect of all sources at a specific receptor location for comparison against relevant standards and guidelines because air pollution monitoring stations measure the total pollution in the atmosphere not just that coming from a part of it.

For this assessment, the average 2004 to 2008 90th percentile PM_{2.5}, NO_x and CO concentrations (a concentration that will only be exceeded 10% of the time) from the MOE monitoring stations outlined above were used as ambient background values. Although not located within the study area, monitoring station background values were considered to be representative of main road intersections within the study area (e.g., Highway 7 and Leslie Street). A quality assurance estimation showed that the total number of vehicles impacting the Yonge/Finch location was about 60,000 per day in 2001/2002 (City of Toronto, 2002). Similarly, 2001 traffic data for the intersection of Highway 7/Leslie Street showed that about 60,000 vehicles per day impact this location (SENES, 2005) suggesting that the monitoring station 90th percentile values at the Yonge/Finch location are representative of the worst case background concentrations within the study area. Moreover, it is SENES' opinion that 90th percentile values will actually over-estimate the true background concentrations because emissions near Yonge/Finch or Bay/Wellesley will be dispersed less due to the number of buildings in these locations, leading to higher concentrations in general at those locations.

Remaining sources of background not captured by available monitoring data were modelled. The contribution of Highway 407 was not considered to be part of the background value established from the monitoring data. Therefore, Highway 407 was included in the modelling so that all of the background contribution was captured in this assessment.

Ambient background concentrations developed from the monitoring data are outlined in Table 2.9.

Table 2.9 Representative MOE Monitoring Station Average 90th Percentile Background Concentrations (µg/m³)

Pollutant	PM_{2.5}[*] (24-hr)	NO_x (24-hr)	NO_x (1-hr)	CO (8-hr)	CO (1-hr)
Background	17.5	93	108	483.6	492.4
MOE Criteria	30	200	400	15,700	36,200

*Canada-Wide Standard

As outlined in the above table, the average 90th percentile CO concentrations are well within MOE AAQC, however, the average 90th percentile 24-hr NO_x and PM_{2.5} concentrations are 47% and 58% of the AAQC, respectively. Oxides of nitrogen exist in several forms in the atmosphere, with most of the vehicular emissions emitted as NO and the remainder as NO₂. NO_x is the sum of all forms of oxides of nitrogen expressed as equivalent NO₂. It should be noted that the AAQC is for NO₂; however, the emission factors used in this assessment are for NO_x. NO is converted over time in the atmosphere to NO₂ in complex reactions. The approach taken is conservative because the emissions estimated will be for NO_x, which will over-estimate the actual NO₂ emitted.

MOE Technical Support Staff have suggested 50 to 60% of PM₁₀ is considered to be PM_{2.5} and 50 to 80% of TSP is considered to be PM₁₀. In other words, PM₁₀ is 1.7 to 2 times the concentration of PM_{2.5} and TSP is 1.3 to 2 times the concentration of PM₁₀. Since there was no monitoring data available for TSP or PM₁₀ concentrations from the representative MOE monitoring stations, the background PM_{2.5} value of 17.5 µg/m³ was conservatively assumed to be 50% of the PM₁₀ value, and the PM₁₀ value was conservatively assumed to be 50% of the TSP value. As can be seen in Table 2.10 the estimated background particulate concentrations are between 59% and 70% of AAQC, which is conservatively high.

Table 2.10 24-hour Background Particulate Concentrations (µg/m³)

Pollutant	TSP*	PM₁₀*	PM_{2.5}
Background	70	35	17.5
Criteria	120	50	30

* PM₁₀ concentrations were estimated by doubling the measured PM_{2.5} concentration and TSP concentrations were estimated by doubling the PM₁₀ concentration.

The VOCs considered for this study are not generally monitored at any of the MOE Stations within the Region of York, with only benzene and 1,3-butadiene monitored at a select few MOE stations in Ontario. Therefore, urban concentrations measured in major cities similar to Toronto, as provided on the TOXNET website (<http://toxnet.nlm.nih.gov/cgi-bin/sis/htmlgen?HSDB>) were used as they would be conservatively high.

Table 2.11 Conservative Background VOC Concentrations ($\mu\text{g}/\text{m}^3$)

Pollutant	Acetaldehyde		Acrolein		Benzene*		1,3-Butadiene*		Formaldehyde	
	1-hr	24-hr	1-hr	24-hr	1-hr	24-hr	1-hr	24-hr	1-hr	24-hr
Background	4.0		0.7		4.4		21		6	
MOE AAQC	500	500	4.5	0.4	n/a	2.3	n/a	10	n/a	65

*Proposed MOE AAQC (July, 2009)

The data in Table 2.11 are likely to be conservatively high since many of the measurements originated from larger U.S. cities in the mid-1970's. Therefore, actual background concentrations are expected to be substantially lower.

It should be noted that the acrolein background of $0.7 \mu\text{g}/\text{m}^3$ is greater than the 24-hour AAQC ($0.4 \mu\text{g}/\text{m}^3$). Therefore, the modelled plus background concentrations will also be above the 24-hour AAQC. Additionally, the benzene background value ($4.4 \mu\text{g}/\text{m}^3$) and the 1,3-butadiene background value ($21 \mu\text{g}/\text{m}^3$) are greater than the proposed 24-hour AAQC ($2.3 \mu\text{g}/\text{m}^3$ and $10 \mu\text{g}/\text{m}^3$, respectively). Therefore, the modelled plus background concentrations of benzene and 1,3-butadiene will also be above the proposed 24-hour AAQC. Since the background acrolein, benzene and 1,3-butadiene background values were based on urban concentrations of 0.7 , 4.4 and $21 \mu\text{g}/\text{m}^3$, respectively (New Jersey, 1976) they are considered to be reasonable worst-case background concentrations.

3.0 ATMOSPHERIC EMISSIONS

To assess the impact on air quality within the study area based on the presence of the 407 Transitway, contaminant emissions of CO, NO_x, VOCs, GHGs (CO₂, CH₄, N₂O and CO_{2e}) and particulate matter (PM, PM₁₀ and PM_{2.5}) were calculated. Modelling was undertaken for all contaminants but GHGs. For GHGs, a pollutant burden analysis was completed whereby the total annual emissions in tonnes or kilotonnes per year of CO₂, CH₄, N₂O and CO_{2e} (CO₂ equivalent) were estimated.

3.1 DESCRIPTION OF ASSESSMENT SCENARIOS

To put the project into perspective over its lifetime, the assessment covered three different scenarios: Existing Conditions (2008), Future **Without** the 407 Transitway (2031), and Future **With** the 407 Transitway (2031). Detailed descriptions and assumptions used in each of the assessment scenarios are as follows.

3.1.1 Existing Conditions (2008)

The 407 Transitway will be constructed in the major traffic corridor of Highway 7 and Highway 407 from Highway 400 to Kennedy Road in the municipalities of Vaughan, Richmond Hill and Markham, Ontario. In particular, the Transitway will be built parallel to and within 100 metres of Highway 407 for most of the route. As a result, it is important to consider traffic impacts of the existing road network in and around the proposed Transitway as a background contribution. As discussed previously, background values established in Section 2.4 are representative of concentrations in and around Highway 7, but are not inclusive of Highway 407. Therefore, the current road network of Highway 407 (typically three lanes in each direction) and its use by an existing vehicle fleet was modelled so that all remaining background was captured.

Using the emissions estimating methods outlined in Section 3.2, an emissions inventory for existing conditions (2008) was developed for Highway 407 between Highway 400 and Kennedy Road. This inventory (excluding GHGs) was input into the CAL3QHCR transportation model (Section 4.0) and the distribution of maximum pollutant concentrations throughout the study area calculated based on hourly meteorological data. Estimated ambient background values (Tables 2.9 to 2.11) were added to modelled concentrations to determine the combined effect of the Transitway and all background sources at specific receptor locations.

A pollutant burden analysis was completed for GHGs whereby the total annual emissions in tonnes or kilotonnes per year were estimated.

3.1.2 Future Without the 407 Transitway (2031)

2031 is the expected year that the Transitway will be in full operation. The future (2031) scenario **without** the 407 Transitway assumes that there are no changes to the existing road network of Highway 407 compared to the Existing Conditions scenario (i.e., three lanes remain in each direction). However, in response to population growth, traffic volumes on Highway 407 will increase in the future. This future scenario also assumed that additional public transit (i.e., buses) will be present on Highway 407. As a worst-case scenario, it was assumed that the future bus fleet would be diesel-fuelled. A new emissions inventory was developed for the future scenario without the Transitway based on the above changes and the inventory (excluding GHGs) input into the CAL3QHCR transportation model. The same background values used for the Existing Conditions scenario were used for this future scenario. A pollutant burden analysis was completed for GHGs.

3.1.3 Future With the 407 Transitway (2031)

This future (2031) scenario is the same as the above future scenario except for the addition of a 23 kilometre bus rapid transit (BRT) system (the 407 Transitway) that will be grade-separated and approximately parallel to Highway 407 from Highway 400 to Kennedy Road in the municipalities of Vaughan, Richmond Hill and Markham, Ontario. The preferred route consists of a two lane roadway (one lane in each direction) occupied solely by buses as described in the main Environmental Project Report (EPR) for the undertaking. In this scenario, buses are restricted to the Transitway, meaning that buses from the previous scenario were moved from Highway 407 to the Transitway. Again, it was assumed that the future bus fleet on the Transitway would be diesel-fuelled as a worst-case scenario. Emissions from vehicles present on Highway 407 and the 407 Transitway were calculated and input (excluding GHGs) into the CAL3QHCR model and the same background values as before were added to modelled concentrations. Again, a pollutant burden analysis was completed for GHGs.

The 407 Transitway also includes seven (7) bus stations where buses will temporarily idle to allow passengers to board/alight buses. Three (3) of the bus stations are considered main intermodal stations (Spadina Subway/Jane, Yonge/Richmond Hill Centre and Kennedy stations) which will connect with larger transportation systems such as proposed subway line extensions. The remaining four (4) stations will be smaller stations where buses will stop for very short periods to allow passengers to board/alight buses. All bus stations will include added parking lots and some will have passenger pick-up and drop-off (PPUDO) areas.

It should be noted that bus idling emissions were not considered in this assessment. During peak hours there will be approximately 1 bus per minute travelling through each of the stations; therefore, buses will stop for very short periods to allow passengers to board/alight. Idling

emissions are estimated by the CAL3QHCR dispersion model during vehicle queuing at signalled road intersections. Neither the Transitway nor Highway 407 have signalled road intersections, therefore, idling emissions were estimated to be insignificant and were not considered in this assessment. However, the impacts from the addition of station parking lots and PPUDO areas were assessed. Only two stations (GO Barrie (Concord) and Leslie) were chosen for this assessment. The associated rationale for selecting these two stations is as follows.

3.1.3.1 Bus Stations Assessment

The impact of the GO Barrie (Concord) and Leslie station parking lots and PPUDO were assessed as worst-case scenarios due to their close proximity to sensitive receptor locations (R1 and R10, respectively, outlined in Section 4.5). If predicted air quality impacts are determined to be minimal at these two stations, then impacts from the remaining five stations on local air quality will also be minimal. Moreover, the impacts of Spadina Subway/Jane Station and Yonge/Richmond Hill Centre Station, which are intermodal stations connecting to the Spadina and Yonge subway line extensions, respectively, have already been assessed as part of previous Environmental Assessments (URS, 2006 and 2009). These assessments demonstrated that the addition of the intermodal stations did not significantly impact local air quality. In general, CO, NO₂ and PM_{2.5} concentrations increased by less than 4% with the addition of intermodal subway stations when compared to a similar “No-Build” scenario. Since the 407 Transitway bus stations will only make up a small component of these larger, intermodal subway stations, it is expected that there will not be any significant cumulative impacts from the addition of the Spadina Subway/Jane and Yonge/Richmond Hill Centre stations.

For the bus station assessment, only TSP and NO_x were modelled as indicators of the impact to air quality. Using traffic data supplied by IBI Group, emissions were estimated and the impacts assessed using the U.S. EPA’s Industrial Source Complex Short Term Version 3 (ISCST3) air dispersion model. Detailed descriptions and assumptions used for the bus station assessment are provided in Appendix D.

3.2 VEHICLE EMISSIONS ESTIMATION

3.2.1 Traffic Volumes

The rate of contaminant emissions from a section of road is proportional to the number and types of vehicles travelling along that road as well as vehicle speed. Hourly traffic flows for Highway 407 and the 407 Transitway were calculated based on average daily traffic flows as well as average weekday and weekend hourly traffic profiles. IBI Group provided annual

average daily traffic (AADT) volumes for Highway 407 and the proposed 407 Transitway for the following three scenarios:

- Existing Conditions – 2008;
- Future **Without** the 407 Transitway – 2031; and,
- Future **With** the 407 Transitway – 2031.

It should be noted that only traffic data for Highway 407 and the 407 Transitway were used in the modelling. Other roads within the transportation corridor (i.e., Highway 7) were considered to be part of background concentrations (see Section 2.4 above). Based on discussions with the MTO and Delcan, it is reasonable to assume that the introduction of the 407 Transitway into the study area will reduce the number of vehicles present within the transportation corridor. However, this is not reflected in Highway 407 traffic data and as a result, the vehicle emissions in the future with the 407 Transitway scenario shown in this study are likely higher than they may reasonably be expected to be.

3.2.2 Vehicle Emissions

All pollutants considered in this study are emitted in vehicle exhaust. Additionally, particulate (TSP, PM₁₀ and PM_{2.5}) is emitted from roadway surfaces as a result of tire/break wear, and re-suspension of surface dust by (1) the action of the tires on the surface and (2) the wake created by the passing of the vehicle. Both tailpipe and mechanically generated particulate were included in this study. Tailpipe emissions from vehicles are a function of many variables. Some of the more important parameters are listed below.

- age of the vehicle (newer vehicles emit less);
- number of kilometres which the vehicle has driven;
- emission control equipment that may have been tampered with;
- type of fuel (gasoline, diesel);
- Reid Vapour Pressure (RVP) of gasoline used (adjusted seasonally);
- ambient air temperature;
- vehicle speed;
- rate of acceleration;
- time spent idling;
- type of vehicle (automobile, light truck, heavy truck, bus, etc.); and
- cold or hot start mode.

Vehicular emissions are generally estimated by using emission factors in units of mass of contaminant emitted per vehicle, per distance travelled. To obtain a mass emission rate for a particular road section, the length of the road section is multiplied by the number of vehicles

using that section to obtain the total number of vehicle kilometres travelled (VKT). The VKT are then multiplied by the appropriate emission factors.

The vehicular emission rates were estimated for existing conditions (2008), and for the future year 2031. Emission factors were obtained by running the MOBILE6C model (the 'C' denotes the adjustment for the average Canadian fleet by Environment Canada). Nitrous oxide (N₂O) emission factors are from the 2006 IPCC Guidelines for National Greenhouse Gas Inventories (IPCC, 2006). The MOBILE6C model was run for SENES by Air Improvement Resources (AIR), who is one of the original developers of the MOBILE model. The model outputs emission factors in grams per vehicle kilometre travelled (g/VKT) for all contaminants of concern. All expected technological and regulatory changes affecting future emissions up to 2031 are built into the MOBILE6C model run in order to generate the most representative emission factors possible.

It should be noted that Table 3.1 indicates a reduction in tailpipe emissions between 2008 and 2031, which is due to expected emission reductions from more sophisticated engine technologies and fuels.

Table 3.1 summarizes the emission factors used in the existing conditions and future year for 100 km/h, which is the posted speed limit of both Highway 407 and the proposed 407 Transitway.

It should be noted that Table 3.1 indicates a reduction in tailpipe emissions between 2008 and 2031, which is due to expected emission reductions from more sophisticated engine technologies and fuels.

Table 3.1 MOBILE6C Tailpipe Emission Factors for 2008 and 2031

2008					
Cars					
Speed (km/h)	TSP	PM₁₀	PM_{2.5}	NO_x	CO
100	0.02759	0.02759	0.01746	1.3167	12.3690
Speed (km/h)	Benzene	Acetaldehyde	Formaldehyde	1,3-Butadiene	Acrolein
100	0.015826	0.00262	0.00599	0.00188	0.00031
Speed (km/h)	CO₂	CH₄	N₂O*		
100	340.33	0.02858	0.008		
Trucks/Buses					
Speed (km/h)	TSP	PM₁₀	PM_{2.5}	NO_x	CO
100	0.12682	0.12682	0.10787	6.6456	0.98114
Speed (km/h)	Benzene	Acetaldehyde	Formaldehyde	1,3-Butadiene	Acrolein
100	0.00261	0.00716	0.01944	0.00152	0.00087
Speed (km/h)	CO₂	CH₄	N₂O*		
100	840.28	0.01118	0.003		
2031					
Cars					
Speed (km/h)	TSP	PM₁₀	PM_{2.5}	NO_x	CO
100	0.01665	0.01665	0.00746	0.21313	7.7678
Speed (km/h)	Benzene	Acetaldehyde	Formaldehyde	1,3-Butadiene	Acrolein
100	0.00752	0.00128	0.00274	0.00083	0.00014
Speed (km/h)	CO₂	CH₄	N₂O*		
100	350.76	0.01429	0.008		
Trucks/Buses					
Speed (km/h)	TSP	PM₁₀	PM_{2.5}	NO_x	CO
100	0.02187	0.02187	0.011309	0.38898	0.10128
Speed (km/h)	Benzene	Acetaldehyde	Formaldehyde	1,3-Butadiene	Acrolein
100	0.001268	0.00348	0.00945	0.00074	0.00042
Speed (km/h)	CO₂	CH₄	N₂O*		
100	839.78	0.00497	0.003		

Note: Emission factors are in g/VKT (grams per vehicle kilometre travelled).

* Emission factors from 2006 IPCC Guidelines for National Greenhouse Gas Inventories

3.2.3 Mechanically Generated Dust Emissions

The U.S. EPA provides an emission factor (U.S. EPA AP-42 Section 13.2.1 Paved Roads, 2006b) to estimate the amount of dust suspended by vehicles on the road, according to the following equation:

$$E = k \left(\frac{sL}{2} \right)^{0.65} \times \left(\frac{W}{3} \right)^{1.5} - C$$

where:	E = particulate emission factor (g/VKT)
	k = particle size multiplier
	24 (g/VKT) for TSP
	4.6 (g/VKT) for PM ₁₀
	0.66 (g/VKT) for PM _{2.5}
	sL = silt loading (g/m ²)
	0.6 (< 500 vehicles per day)
	0.2 (500 – 5,000 vehicles per day)
	0.06 (5,000 – 10,000 vehicles per day)
	0.03 (> 10,000 vehicles per day)
	W = weight of fleet (tons/vehicle)
	3.0 US Tons for cars (average)
	15 US tons for buses/trucks (average)
	C = emission factor for 1980's vehicle fleet exhaust, brake wear and tire wear
	0.1317 (g/VKT) for TSP and PM ₁₀
	0.1005 (g/VKT) for PM _{2.5}
	VKT = vehicle kilometres travelled

The mechanically generated dust emissions from vehicular travel on paved roads are not expected to change over time.

It should be noted that AP-42 Section 13.2.1 indicates that there may be situations where low silt loading and/or low average weight will yield calculated negative emissions from the equation outlined above. If this occurs, it is recommended that the calculated emission factor be set to zero.

3.3 CONSTRUCTION PHASE

The construction of the 407 Transitway has the potential to affect the air quality in the vicinity of the site during the construction phase. Emissions that are associated with road construction activities are particulate matter (TSP, PM₁₀ and PM_{2.5}) and typical combustion emissions, such as CO, NO_x and VOCs, from construction equipment. As with any construction site, these emissions will be of relatively short duration and are unlikely to have any long-lasting effect on the surrounding area. As well, dust impacts can be successfully mitigated through the use of proper controls, such as:

- periodic watering of unpaved (non-vegetated) areas;
- periodic watering of stockpiles;
- limiting speed of vehicular travel;
- use of water sprays during the loading, unloading of materials; and,
- sweeping and/or water flushing of the entrances to the construction zones.

These types of controls aid in minimizing impacts to the environment during the construction phase. Night time construction activities should also be considered in order to reduce emissions from vehicles that are slowed down by any reduced road capacity during the day.

New developments in materials science and their application will continue to provide options for construction processes that could help to reduce emissions related to road and highway construction, rehabilitation and maintenance. Substitution of materials with more durable ones will result in overall emission reductions associated with the extended service life of structures and pavements. Also new developments in engine technologies and more advanced high-efficiency, low-emission type equipment and vehicles can significantly reduce associated emissions. Thus, it can be expected that construction related emissions from projects that are carried out in the years to come will be lower than if the same activities were undertaken today.

4.0 AIR DISPERSION MODELLING

4.1 MODELLING METHODOLOGY

Air quality is a measure of the amount of polluting chemical in a given volume of air. The typical unit of measurement is concentration or the number of micrograms of chemical, or particles, per cubic metre of air ($\mu\text{g}/\text{m}^3$). This concentration will vary from point-to-point and from minute-to-minute in response to changing atmospheric conditions (wind speed, wind direction, temperature, atmospheric stability and mixing height) and the amount of pollutant emitted.

To calculate the concentration at a given location near an emission source, an atmospheric dispersion model is used. These models take the emissions from a source and disperse them into the surrounding atmosphere, typically using historical hourly meteorological data from a local weather station.

To assess the changes in the study area, the model was run for ten pollutants and the resulting concentrations were obtained for three different scenarios:

- Existing conditions – 2008;
- Future **Without** the 407 Transitway – 2031; and,
- Future **With** the 407 Transitway – 2031.

The same meteorological conditions were used for all scenarios. The only differences between the three sets of model simulations of air quality were (1) the amount of emissions released and (2) the number, or location, of sources (road lanes) that were input into the model. In general terms, if the emissions are reduced, the resulting impact on the surrounding community (gas or particulate concentrations) will be reduced. Conversely, if the emissions increase, the impacts will increase.

The atmospheric dispersion model used for this study was CAL3QHCR, which is described in further detail in the following section. An example CAL3QHCR input file is provided in Appendix C.

4.2 CAL3QHCR

CAL3QHCR is a model developed specifically to predict the impacts of vehicle emissions from free flowing traffic conditions and near roadway intersections (U.S. EPA, 1995). The model combines the CALINE-3 (Benson, 1979) line source dispersion model and a traffic algorithm for estimating vehicular queue lengths at signalized intersections. The CALINE-3 line source

dispersion model predicts more realistic concentrations immediately around roads because of the initial mixing in the wake zone of the vehicle. This initial mixing, combined with the traffic algorithm for queuing (added emissions from idling vehicles), provides improved model predictions of the impact of vehicle tailpipe emissions adjacent to roadways.

The average vehicle travel speeds were chosen based on the posted speed limits on the roadways, which is 100 km/h.

CAL3QHCR model guidance documents recommend using a source release height of 0 m assuming light duty vehicles dominate the vehicle fleet. However, as heavy duty vehicles (i.e., trucks and buses) are expected within the study area, SENES used a release height of 1 m. Additionally, sections of the Transitway will be constructed to go over or under existing roadways (e.g., Highway 407), railways or ponds/streams. As such, sources were assigned appropriate release heights to reflect changes in elevation and were designated as being either “at grade”, “above grade” or “below grade” in the model.

The model was originally designed to simulate dispersion of CO and PM₁₀ from roadways. However, it is applicable to all gaseous pollutants, provided that minor alterations to the model source code are made. To model NO_x and VOC emissions, the model was modified to reflect the difference in the contaminant molecular weight.

Since emission factors differ by vehicle class, the vehicle mix was used to calculate a composite emission factor for each pollutant for a given roadway based on the fraction of cars and diesel trucks or buses that travel on it. A weekday and weekend hourly traffic profile was provided by IBI Group and was used to develop emission factors for each pollutant for each hour of the day.

4.3 METEOROLOGICAL DATA

For CAL3QHCR modelling, hourly meteorological data is required, including: mixing height, temperature, cloud cover, cloud opacity, wind speed and wind direction. For calculating hourly mixing heights, upper air measurements are needed. Using upper air observations (twice daily), morning and afternoon mixing heights are calculated and, based on these measurements, hourly mixing heights are estimated using the U.S. EPA's regulatory meteorological pre-processor PCRAMMET.

The meteorological data used for this assessment was the Ontario Ministry of Environment (MOE) default five year meteorological dataset for the Region of York-Durham. This data is based on 1992 to 1996 hourly surface meteorological data from Pearson International Airport, and upper air (mixing height) data from the Buffalo International Airport. Mixing heights are a

regional parameter and do not change significantly over moderate distances. Buffalo is the closest upper air meteorological station to Toronto.

Typically, five years of hourly meteorological data are used in dispersion modelling calculations, as recommended by the U.S. EPA in order to include all of the possible combinations of meteorological conditions expected to occur in the area to be modelled. The CAL3QHCR model can process only one year of data per model run, therefore results for each year of meteorological data were compared to determine the maximum concentration for each contaminant. The model was run with five years of meteorological data for ten contaminants over the three scenarios to determine maximum contaminant concentrations at ten sensitive receptors (see Section 4.5). To develop isopleths for illustrative purposes the worst case meteorological year (i.e., the year that most often gave the highest maximum ground-level concentrations) was selected (1993), and used to model concentrations at 2091 receptors (see Section 4.4).

4.4 RECEPTOR GRID

In order to avoid modelling artefacts (mathematical anomalies created by the model that do not occur in reality), it was important to ensure that there were no receptors on or unreasonably close to the modelled road source. The end-points of the centreline of each road link were determined from the digital maps supplied in UTM coordinates. Assuming the width of the road is W , a series of receptors were placed parallel to the road links at a width of $2W$ centred on the centreline of the road. This placed the points at a distance of $1.5W$ from the edge of the roadway. Receptors were placed every 100 m parallel to all arterial roads within the study area.

A second set of receptors were placed at a width of $5W$ or at a distance of $4.5W$ from the edge of the roadway, again with 100 m spacing as described above. A Cartesian grid with a spacing of 200 m was overlaid to cover the rest of the modelling domain and converted to discrete receptors. All Cartesian grid points that fell closer to the road than the $5W$ receptors were removed. The receptor height was selected as 1.5 m above the ground.

4.5 DISCRETE/SENSITIVE RECEPTORS

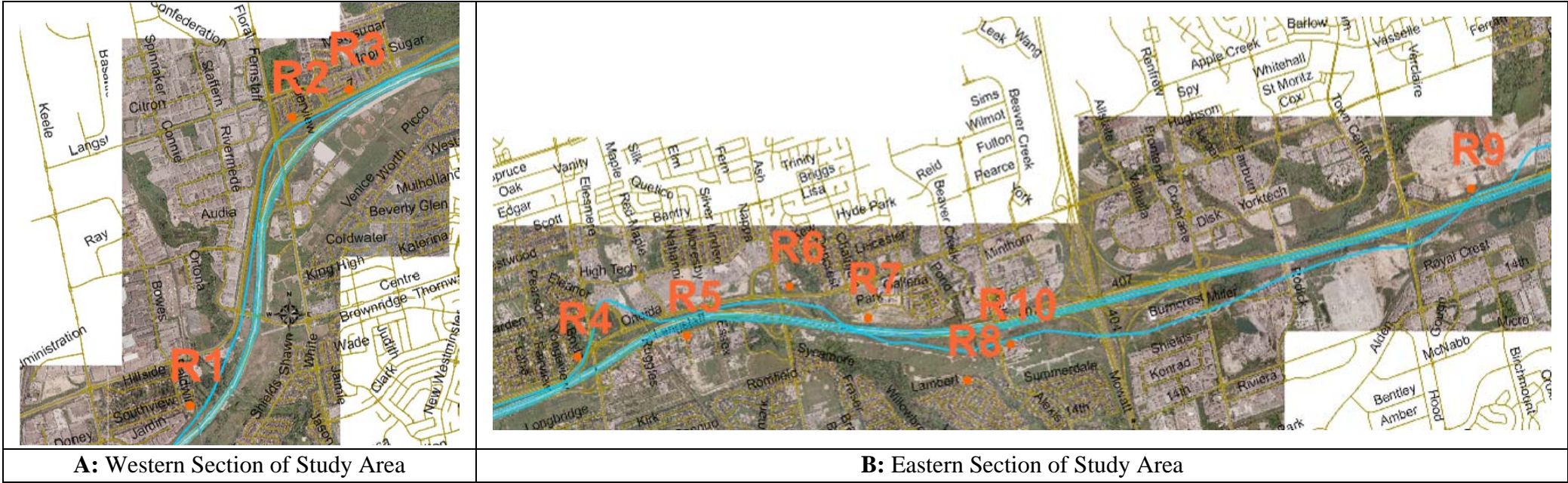
In addition to the modelling grid, a series of ten discrete/sensitive receptors were chosen to help summarize the modelling results and at which a comparison was made to applicable criteria. Chosen discrete/sensitive receptors included nearby existing/future residential areas or schools located throughout the study area at varying distances from the roadway.

The selected receptors are outlined in Table 4.1 and presented in Figure 4.1 below.

Table 4.1 Sensitive Receptors

	Receptor Description
R1	Residences on Hartley Ct; north of Transitway, west of GO Barrie Line
R2	Residences on Yellowwood Circle; north of Transitway, east of Dufferin St
R3	Residences on Sassafra Circle; north of Transitway, east of Langstaff Rd
R4	Residences on Langstaff Rd W; west of Transitway
R5	Residence on Cedar Ave, south of Transitway
R6	Apartment building, northeast corner of Bayview Ave and Highway 7
R7	Potential residential development, south of South Park Rd
R8	Residences on Huntington Park Dr; south of Transitway
R9	Potential residential development north of Transitway, east of Warden Ave
R10	St. Robert Catholic High School, south of Transitway, east of Leslie St

Figure 4.1 Location of Sensitive Receptors



5.0 ASSESSMENT OF AIR QUALITY

5.1 BACKGROUND

When following the Transit Project Assessment Process and assessing the merits of the proposed 407 Transitway compared to the future scenario without the Transitway, it is the incremental change in total model predicted concentrations between the two future cases that is the true measure of the future impact. The same background concentrations were added to the modelled concentrations for the Existing Conditions (2008) scenario, the Future Without the 407 Transitway (2031) scenario and the Future With the 407 Transitway scenario. Therefore, when assessing the incremental change in the combined concentrations, the background concentration cancels out. However, it is also important to understand the magnitude of the change in total predicted combined concentrations (i.e., background plus project related).

The constant ambient background concentrations established in Section 2.4 above were added to the model predicted concentrations (inclusive of the background contribution from Highway 407) to obtain a true estimate of ambient concentrations at each receptor location.

5.2 CALQ3HCR MODELLING RESULTS

The output from the model is the maximum predicted 1-hour average concentration at each of the modelled receptor points based on a full year of meteorological data (8760 simulated hours). Hourly data is post-processed to determine the maximum predicted 24-hour average (or 8-hour for CO) concentrations.

The results from the air dispersion modelling have been presented in graphical format with complete results provided in appendices at the back of the report. Contour plots (averaging period depends on the contaminant of concern), have been created for all three scenarios (i.e., Existing Conditions (2008), Future Without the 407 Transitway (2031) and Future With the 407 Transitway (2031)) and compared to applicable provincial MOE AAQCs or federal Canada-Wide standards. The results for all three scenarios have also been presented in tabular form for the ten specific sensitive receptor locations outlined above.

As outlined in Section 4.3, due to computational constraints a worst case meteorological year (1993) was used to develop graphical isopleths for each contaminant. A total of 2091 receptors are included in this modelling analysis to ensure an accurate depiction of isopleths (lines of equal concentration).

Nitrogen oxides (NO_x) graphical results are presented in Section 5.3 below, with all other gaseous compounds demonstrating trends similar to those for NO_x. As was noted in Section 2.4

above, the 24-hour background acrolein concentration is greater than the MOE AAQC. However, as outlined in Figure A.7 in Appendix A, the model predicted 24-hour acrolein values (excluding background) are less than the AAQC standards throughout the study area. Similarly, the benzene and 1,3-butadiene background concentrations are greater than proposed AAQC, but Figures A.10 and A.13 in Appendix A show that the model predicted 24-hour concentrations are less than the proposed standards when background is excluded.

PM₁₀ and PM_{2.5} graphical results are presented below in Sections 5.4 and 5.5, respectively with TSP demonstrating trends similar to those of PM₁₀. PM_{2.5} results are different from other particulate matter size fractions as described below. Complete graphical results and tabular results for all pollutants assessed are provided in Appendix A and Appendix B, respectively.

5.3 GRAPHICAL AND TABULAR PRESENTATION OF RESULTS - NO_x

As illustrated in Appendix A (graphical) and Appendix B (tabular), each of the gaseous contaminants studied show similar patterns to the NO_x results. The predicted 24-hour maximum NO_x concentrations for all scenarios are presented in Table 5.1. The maximum 24-hour average modelled concentrations for NO_x for all scenarios are presented as concentration isopleths over a base map in Figures 5.1a through 5.1c. The contours are lines of equal predicted maximum 24-hour concentrations. For presentation purposes each figure is separated into two sections, a western section and an eastern section of the study area. These figures do not represent a snapshot in time as the maximum concentrations at each receptor typically occur during different meteorological conditions (i.e., different hours and/or days) and thus do not occur simultaneously. For example, at a point south of a road, winds blowing from the north in January may give rise to the maximum 24-hour concentration, whereas for a point north of the road, the worst meteorological conditions may occur in June with a different wind direction. The concentration values presented include background, as discussed earlier. It can be seen in the figures that the contour lines closely follow the road links and drop off rapidly with distance from the centre of the road.

5.3.1 Comparison of Existing Conditions (2008) to Future Scenarios (2031)

As illustrated in Table 5.1, the predicted 24-hour maximum concentrations for existing conditions (2008) for NO_x are greater than the two future scenarios (2031). As outlined in Section 3.2.2 above, this is a result of emission reductions due to advancements in fuel and vehicle technologies, despite the predicted increases in traffic due to population growth. As indicated in it should be noted that Table 3.1 indicates a reduction in tailpipe emissions between 2008 and 2031, which is due to expected emission reductions from more sophisticated engine technologies and fuels. Table 3.1 above, the NO_x emission factor for cars in 2031 is approximately 16% of the emission factor in 2008 and approximately 6% for trucks/buses.

Table 5.1 Maximum 24-hour NO_x Concentrations – Existing and Future Scenarios

Receptor	Existing Conditions	Future No Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	142	105	-26%	105	-26%	200
R2	140	104	-26%	104	-25%	200
R3	173	112	-35%	112	-35%	200
R4	154	107	-30%	107	-30%	200
R5	184	114	-38%	113	-38%	200
R6	134	102	-23%	102	-23%	200
R7	175	111	-36%	111	-36%	200
R8	119	99	-17%	99	-17%	200
R9	138	106	-23%	106	-23%	200
R10	143	104	-27%	105	-27%	200

Note: All values include a conservative background NO_x concentration of 93.4 µg/m³.

Table 5.1 also indicates that there are no exceedances of the 24-hour NO_x for any scenario. In contrast, exceedances of the 1-hour NO_x AAQC are predicted for the Existing Conditions scenario only as shown in Appendix A and B. Due to the reduction in the tailpipe emission factor in the future, there are no exceedances of the 1-hour NO_x AAQC in either future scenario.

5.3.2 Comparison of Future with and without the 407 Transitway (2031)

The predicted 24-hour maximum concentrations at the ten sensitive receptors for the future with and without the 407 Transitway scenarios (2031) for NO_x are presented in Table 5.2. The table indicates the air quality impact on concentrations of NO_x as a result of the proposed 407 Transitway will be insignificant (less than 1%). A comparison of Figures 5.1b and 5.1c also illustrates negligible changes in NO_x concentrations between the future no-build and future with the 407 Transitway scenarios.

Figures and tabulations for all other gaseous compounds are provided in Appendix A and B, respectively and demonstrate results similar to those of NO_x. Exceedances of 24-hour AAQC for acrolein, benzene and 1,3-butadiene concentrations were predicted in this study. As noted previously, benzene and 1,3-butadiene standards are only proposed. Section 2.4 outlined that the background acrolein, benzene, and 1,3-butadiene concentrations already exceed applicable criteria which suggests that there is likely an underlying problem today with elevated concentrations of these three contaminants throughout urbanized areas in Southern Ontario. However, as with all gaseous compounds, based on the implementation of the proposed 407 Transitway, there will be negligible changes in acrolein, benzene and 1,3-butadiene concentrations within the study area compared to the future scenario without the Transitway.

Table 5.2 Maximum 24-hour NO_x Concentrations – Future Scenarios Comparison

Receptor	Future Without Transitway (µg/m³)	Future With Transitway (µg/m³)	% Change from Without Transitway	AAQC (µg/m³)
R1	105	105	0.01%	200
R2	104	104	0.14%	200
R3	112	112	0.10%	200
R4	107	107	-0.03%	200
R5	114	113	-0.24%	200
R6	102	102	0.01%	200
R7	111	111	-0.11%	200
R8	99	99	-0.09%	200
R9	106	106	0.12%	200
R10	104	105	0.28%	200

Note: All values include a conservative background NO_x concentration of 93.4 µg/m³.

Figure 5.1 Maximum 24-hour NO_x Concentrations for Existing and Future Scenarios

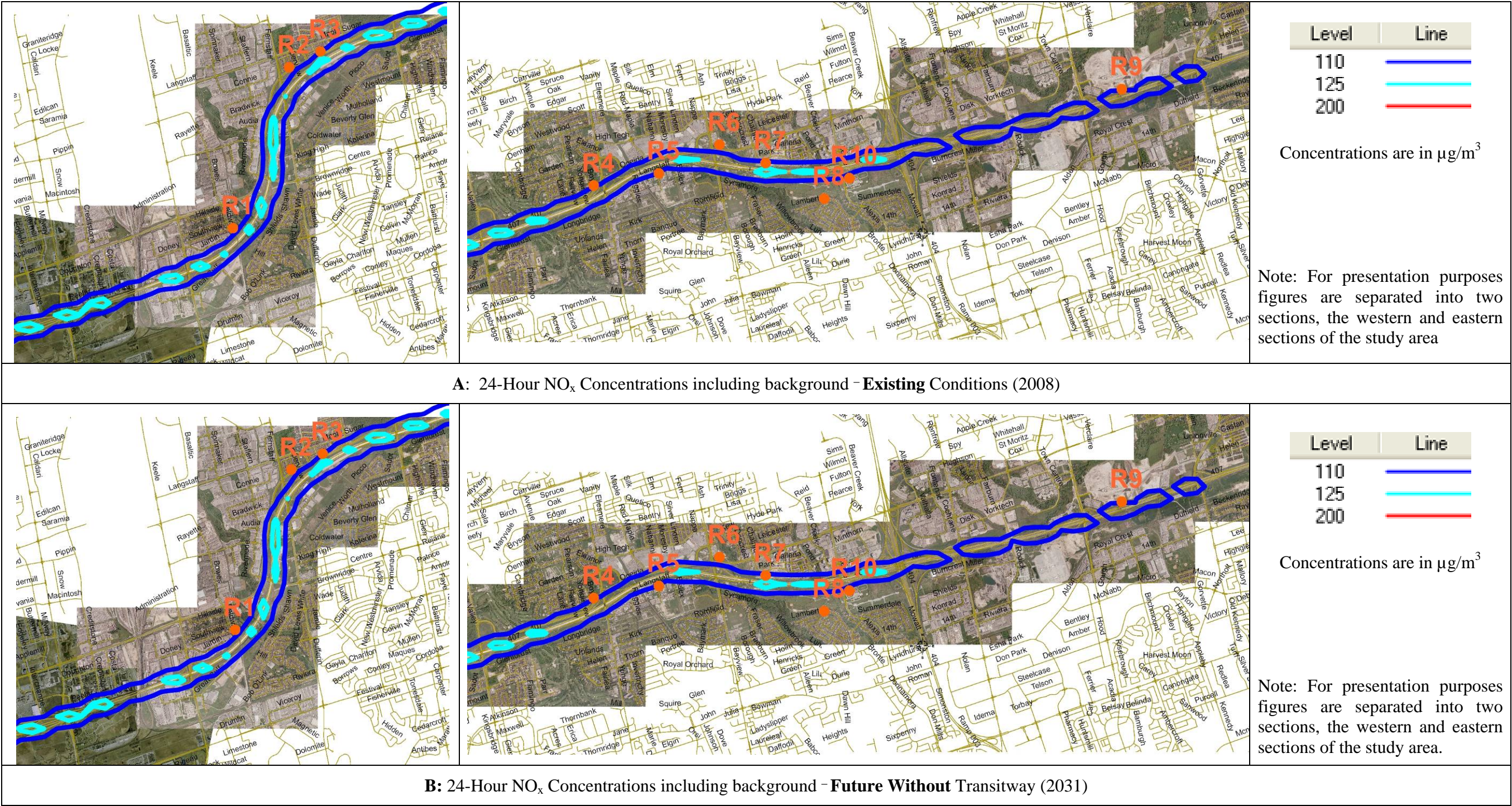
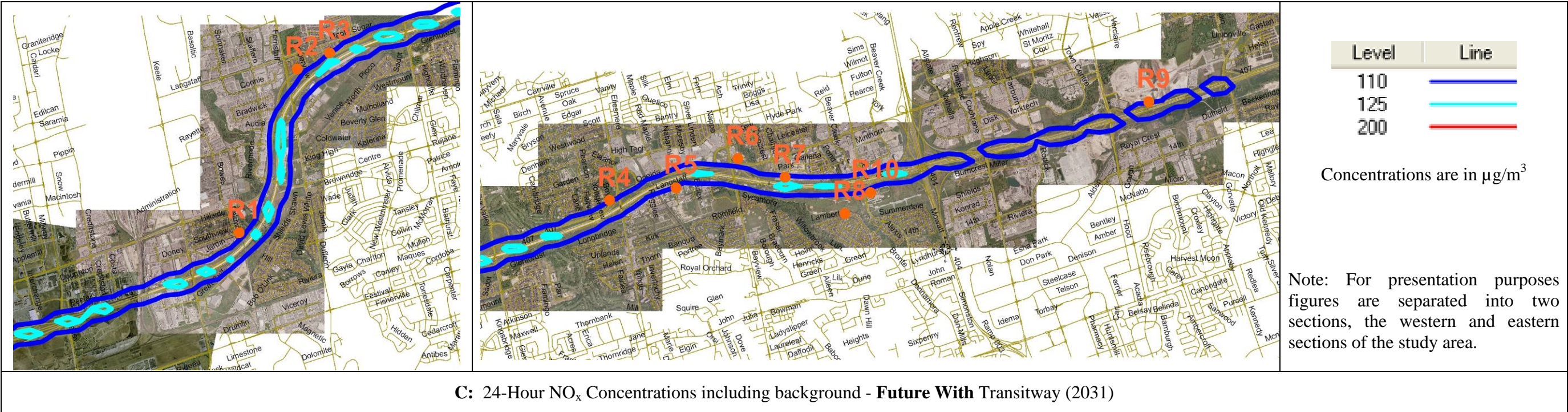


Figure 5.1 Maximum 24-hour NO_x Concentrations for Existing and Future Scenario (Cont'd)



5.4 GRAPHICAL AND TABULAR PRESENTATION OF RESULTS - PM₁₀

The maximum 24-hour average modelled concentrations of PM₁₀ for all scenarios are presented with contour lines over a base map in Figures 5.2a through 5.2c. The contours are lines of equal predicted maximum 24-hour concentrations. As outlined in Section 5.3 above, these maximum concentrations do not occur simultaneously, but are the maximum 24-hour concentrations predicted at each grid point during a one year period added to a conservative background concentration. It can be seen in the figures that the contour lines closely follow the road links and drop off rapidly with distance from the road centreline.

5.4.1 Comparison of Existing Conditions (2008) to Future Scenarios (2031)

As illustrated in Table 5.3, the predicted 24-hour maximum concentrations for the two future scenarios (2031) are greater than the concentrations predicted for existing conditions (2008) for all sensitive receptor locations. As indicated in it should be noted that Table 3.1 indicates a reduction in tailpipe emissions between 2008 and 2031, which is due to expected emission reductions from more sophisticated engine technologies and fuels.

Table 3.1 above, the PM₁₀ MOBILE6C emission factor for cars in 2031 is approximately 60% of the emission factor in 2008 and approximately 17% for trucks/buses. However, as over 95% of vehicle tailpipe particulate emissions are less than 2.5 µm, emissions of larger particulate fractions (i.e., PM₁₀ and TSP) are made up of re-suspended road dust rather than tailpipe emissions. Therefore, the total PM₁₀ emission factor (tailpipe + road dust) only slightly decreased in the future (2031) and increased PM₁₀ concentrations were predicted as a result of increased traffic within the study area due to population growth.

Table 5.3 also indicates that there are predicted exceedances of the PM₁₀ AAQC at three receptor locations for the Existing Conditions scenario and at eight receptor locations for the Future Without the 407 Transitway scenario. These predicted increases are due to an increase in traffic as a result of future population growth, as previously discussed. For the Future With the 407 Transitway scenario, there are exceedances of the PM₁₀ AAQC at all but one of the sensitive receptors. The greatest predicted increase from the Existing Conditions scenario to the Future With the 407 Transitway scenario is 62% at receptor R10 due to its close proximity to the Transitway (about 40 m). This receptor was previously about 120 m away from Highway 407 which is why this large increase was not seen for the Future Without the 407 Transitway scenario. Differences between the two future scenarios are further discussed in the following section.

Table 5.3 Maximum 24-hour PM₁₀ Concentrations – Existing and Future Scenarios

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		Canada-Wide Standard
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	45.4	51.6	13.6%	57.5	26.5%	50
R2	44.9	51.2	14.0%	60.3	34.4%	50
R3	51.8	63.0	21.5%	71.4	37.8%	50
R4	47.7	56.9	19.4%	62.5	31.1%	50
R5	54.3	67.4	24.2%	69.0	27.2%	50
R6	43.4	49.3	13.5%	55.2	27.2%	50
R7	51.9	64.1	23.5%	68.9	32.7%	50
R8	40.4	44.1	9.1%	47.5	17.4%	50
R9	43.3	52.6	21.4%	62.2	43.8%	50
R10	45.3	52.6	16.0%	73.4	61.9%	50

Note: All values include a background PM₁₀ concentration of 35.1 µg/m³.

5.4.2 Comparison of Future Particulate Matter with and without the 407 Transitway (2031)

The predicted 24-hour maximum concentrations at the ten sensitive receptors for the future with and without the 407 Transitway (2031) for PM₁₀ are presented in Table 5.4. This table indicates that there will be air quality impacts as a result of the addition of the 407 Transitway. Particularly, Table 5.4 suggests that PM₁₀ concentrations will increase anywhere from 2 to 20 µg/m³ (approximately 2% to 40%) at sensitive receptor locations with the addition of the Transitway compared to the future no-build scenario.

A comparison of Figures 5.2b and 5.2c also illustrates PM₁₀ impacts with the addition of the Transitway. The predicted increases are due to (1) an increase in road silt accumulation on the roadway as a result of low traffic volumes/heavier vehicles on the Transitway, and (2) a decrease in the distance from the nearest roadway for some receptor locations. As shown by the U.S. EPA AP-42 Road Dust Emission Factor equation in Section 3.2.3, road segments having lower 24-hour AADT (annual average daily traffic) counts will have a higher silt loading factor. As a result, more road dust is re-suspended. Additionally, the equation shows that heavier vehicles (i.e., trucks and buses) also generate more road dust. Thus, the increased PM₁₀ concentrations shown in Figure 5.2c are a consequence of the low number of buses exclusively occupying the 407 Transitway which causes more road dust to be re-suspended due to higher silt loading and heavier vehicles.

With the addition of the Transitway, the distance between all sensitive receptors and the closest roadway (i.e., the closest emission source) becomes shorter with the exception of R5 and R7. For example, R10 is located about 120 m away from Highway 407 in the absence of the

Transitway, however, when the Transitway is constructed, R10 will be closer to the Transitway at a distance of about 40 metres. As shown in Table 5.4, the greatest predicted impact of the Transitway occurs at R10 - the closest sensitive receptor to the Transitway.

Table 5.4 Maximum 24-hour PM₁₀ Concentrations – Future Scenarios Comparison

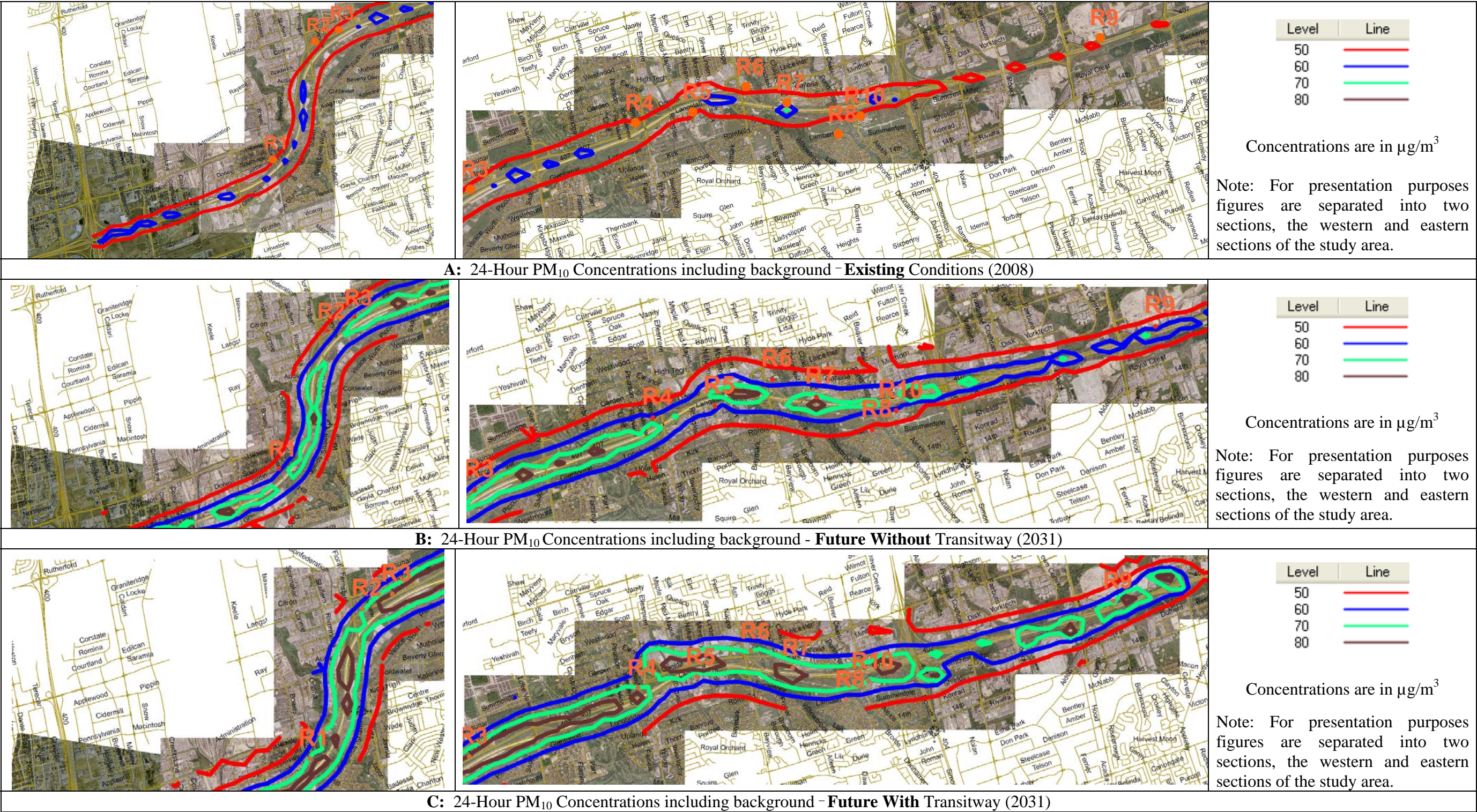
Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	Canada-Wide Standard (µg/m ³)
R1	52	57	11.4%	50
R2	51	60	17.9%	50
R3	63	71	13.4%	50
R4	57	62	9.8%	50
R5	67	69	2.4%	50
R6	49	55	12.0%	50
R7	64	69	7.5%	50
R8	44	47	7.6%	50
R9	53	62	18.4%	50
R10	53	73	39.5%	50

Note: All values include a background PM₁₀ concentration of 35.1 µg/m³.

Figures for TSP are provided in Appendix A and demonstrate results similar to those of PM₁₀; however, the predicted number of exceedances of the TSP AAQC was greater than for the PM₁₀ AAQC. As mentioned previously, a large fraction of PM₁₀ and TSP air emissions are from re-suspended road dust rather than tailpipe emissions, with TSP making up an even smaller fraction of tailpipe emissions than PM₁₀. Therefore, the fraction of TSP in road dust emissions will be greater than the fraction of PM₁₀, resulting in more exceedances with the addition of the Transitway. Tabular TSP results at the discrete/sensitive receptor locations are presented in Appendix B.

In all, based on the implementation of the proposed 407 Transitway, there will be an increase in PM₁₀ and TSP contaminant concentrations immediately adjacent to the Transitway. In the following section, a discussion of PM₁₀ and TSP exceedances of MOE criteria is provided.

Figure 5.2 Maximum 24-hour PM₁₀ Concentrations for Existing and Future Scenarios



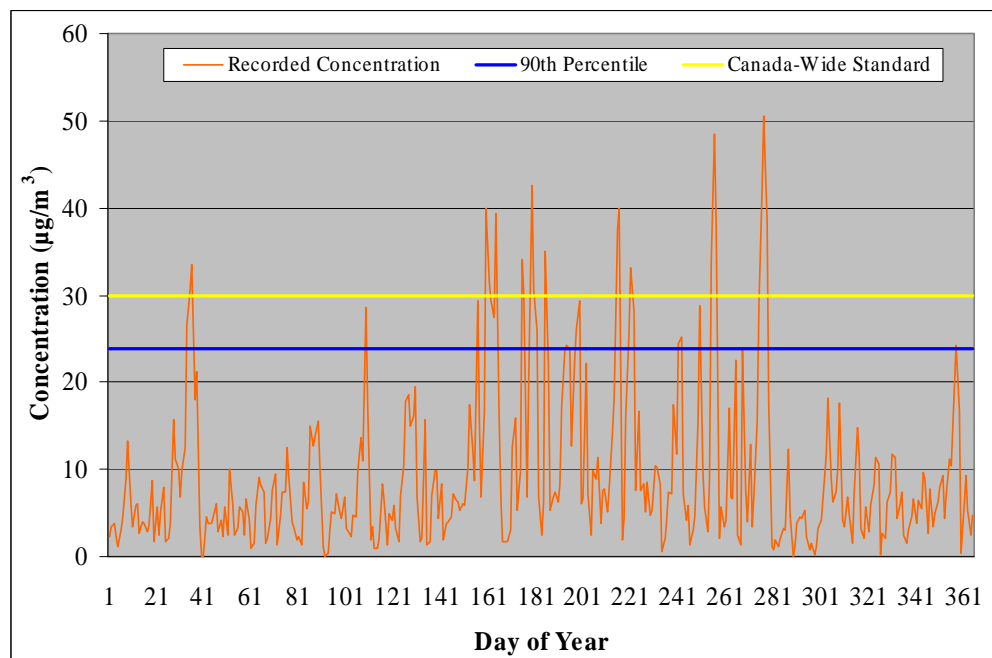
5.4.3 PM₁₀ and TSP Exceedances

5.4.3.1 Conservativeness of Using the 90th Percentile Background for Calculating Exceedances

As discussed in Section 2.4, the 90th percentile of ambient PM_{2.5} monitoring data was used to determine the background concentrations of PM₁₀ and TSP. In order to attempt to capture the highest 24-hour concentration of a contaminant to compare against applicable MOE criteria, the MOE usually requires that air quality assessments use the 90th percentile concentration of ambient air monitoring data as the ambient background value. The 90th percentile value used for PM₁₀ (and TSP) is conservatively high for two reasons: 1) it was conservatively assumed that PM₁₀ concentrations are 2 times higher than monitored PM_{2.5} concentrations (see Section 2.4 and Table 2.10 for discussion); and 2) the 90th percentile is reflective of a background concentration which is actually lower 90% of the time and higher 10% of the time.

While using the 90th percentile background may under-predict the absolute maximum concentrations reported, it can over-predict the number of exceedances of MOE criteria caused directly by the addition of a transportation element because the background concentration is artificially elevated for most of the time. This concept is illustrated in Figure 5.3 using ambient PM_{2.5} monitoring data for the Toronto North MOE station. As shown in Figure 5.3, the use of the 90th percentile as the background concentration is an overestimate of the actual background concentration for a significant part of the year. In addition, Figure 5.3 shows that the day-to-day variability in ambient (background) concentrations is typically several µg/m³ and can approach or even exceed the 30 µg/m³ standard for PM_{2.5}.

Figure 5.3 2005 Toronto North PM_{2.5} Daily Background Concentration



5.4.3.2 Comparison of PM₁₀ Concentrations Using a Constant and Variable Background

To illustrate the conservativeness of using a constant 90th percentile background value to predict the number of exceedances caused directly by the implementation of the Transitway, a sensitivity analysis was undertaken in which PM₁₀ concentrations were predicted using the constant background established in Section 2.4 as well as using a variable background. To predict 24-hour PM₁₀ concentrations using a variable background, ambient PM₁₀ concentrations obtained from the Toronto North monitoring station (ambient PM_{2.5} concentrations multiplied by 2) were added to model predicted 24-hour concentrations on a day-by-day basis. For this analysis, a meteorological data set corresponding to a year of MOE PM_{2.5} monitoring data was required. As such, a 2005 meteorological data set for Toronto Pearson Airport, prepared by SENES for a previous transportation project using CAL3QHCR, was used. 2005 was selected as it was the worst-case meteorological year for that particular project and it corresponded to a year that MOE PM_{2.5} monitoring data was available.

Results

The results of the sensitivity analysis are presented in Table 5.5. As can be seen from the table, the predicted PM₁₀ concentrations as well as the total number of exceedances are greater when a variable background concentration is used. The source responsible for the exceedances

(background or the Transitway) was investigated for R10 – the receptor previously showing the greatest impact from the addition of the Transitway as outlined in Section 5.4.1.

Table 5.5 Maximum 24-hour PM₁₀ Concentrations and Exceedances – Constant and Variable Background Comparison

Receptor	Future Without Transitway				Future With Transitway			
	Constant		Variable		Constant		Variable	
	Concentration (µg/m ³) ¹	Exceedances ²	Concentration (µg/m ³) ¹	Exceedances ²	Concentration (µg/m ³) ¹	Exceedances ²	Concentration (µg/m ³) ¹	Exceedances ²
R1	50.4	1	112.1	38	55.5	4	116.5	41
R2	49.8	0	111.4	38	56.4	5	116.5	41
R3	57.1	2	115.5	42	63.2	16	120.8	46
R4	54.9	1	114.3	41	60.2	8	119.3	45
R5	57.4	5	101.4	38	57.7	6	101.3	38
R6	45.2	0	109.5	38	49.8	0	113.2	42
R7	59.3	14	120.2	46	62.7	34	123.5	49
R8	41.7	0	101.2	32	44.0	0	101.2	33
R9	50.6	1	112.5	41	59.8	9	119.1	43
R10	52.1	1	101.2	36	67.9	14	101.2	40

¹All values include an ambient background PM₁₀ concentration of 35.1 µg/m³.

²Interim MOE AAQC for PM₁₀ is 50 µg/m³.

Predicted PM₁₀ Concentrations and Exceedances at R10

Figures 5.4 and 5.5 provide a graphical representation of the daily concentrations of PM₁₀ at R10 for the Future With the 407 Transitway scenario. As can be seen in the figures, background concentrations dominate when either a constant 90th percentile or variable background is used.

When adding a constant background to model predicted concentrations at R10, there were a total of 14 exceedances with the Transitway compared to 1 exceedance without (Table 5.5). Since the 90th percentile background value is below 50 µg/m³, it can be concluded that 13 of the 14 predicted exceedances were caused by the addition of the Transitway. In contrast, there were 36 exceedances predicted for the Future Without the Transitway scenario and 40 exceedances predicted for the Future With the Transitway scenario when a variable background was used. As Figure 5.5 illustrates, there are a number of days when the background PM₁₀ concentration already exceeds the MOE AAQC. Specifically, there were 32 days when the AAQC was exceeded. This leaves only 4 days when exceedances of the AAQC can be attributed to the traffic increment (i.e., Highway 407) in the future no-build scenario and 8 days in the future scenario with the added Transitway. This result shows that the addition of the Transitway only caused 4 more exceedances compared to the 13 exceedances predicted when a constant background was used. Therefore, in actuality, the number of predicted exceedances caused by the Transitway increment decreased when a variable background was used. It just so happened that there were a significant number of days in 2005 when ambient PM₁₀ concentrations already exceeded the MOE AAQC which inflated the number of exceedances compared to the case when a constant background was used.

In all, these results suggest that using a 90th percentile background value will over-predict the number of exceedances resulting directly from the addition of the Transitway. However, the total number of exceedances predicted may increase when using a variable background, depending upon the number of ambient (background) exceedances already occurring.

In addition, the number of exceedances predicted for PM₁₀ (and TSP) is also likely to be overestimated regardless of the scenario being assessed because it was conservatively assumed that PM_{2.5} is 50% of PM₁₀ and that PM₁₀ is 50% of TSP.

Figure 5.4 Daily PM₁₀ Concentration at R10 using a Constant Background

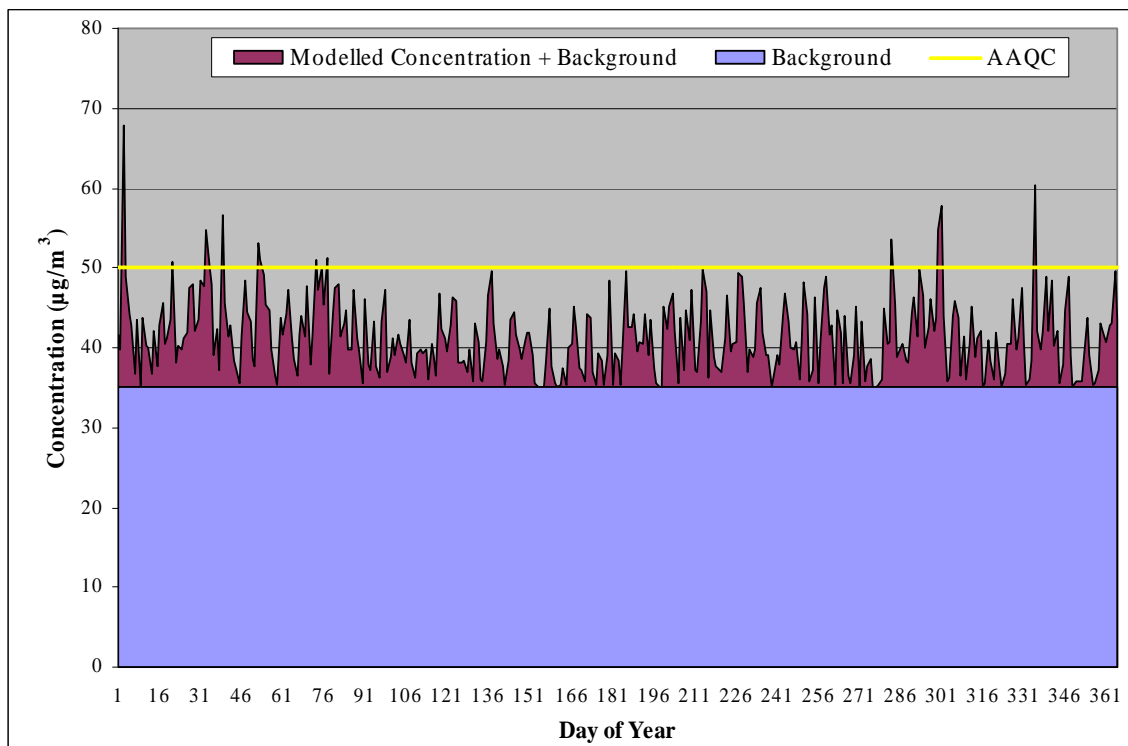
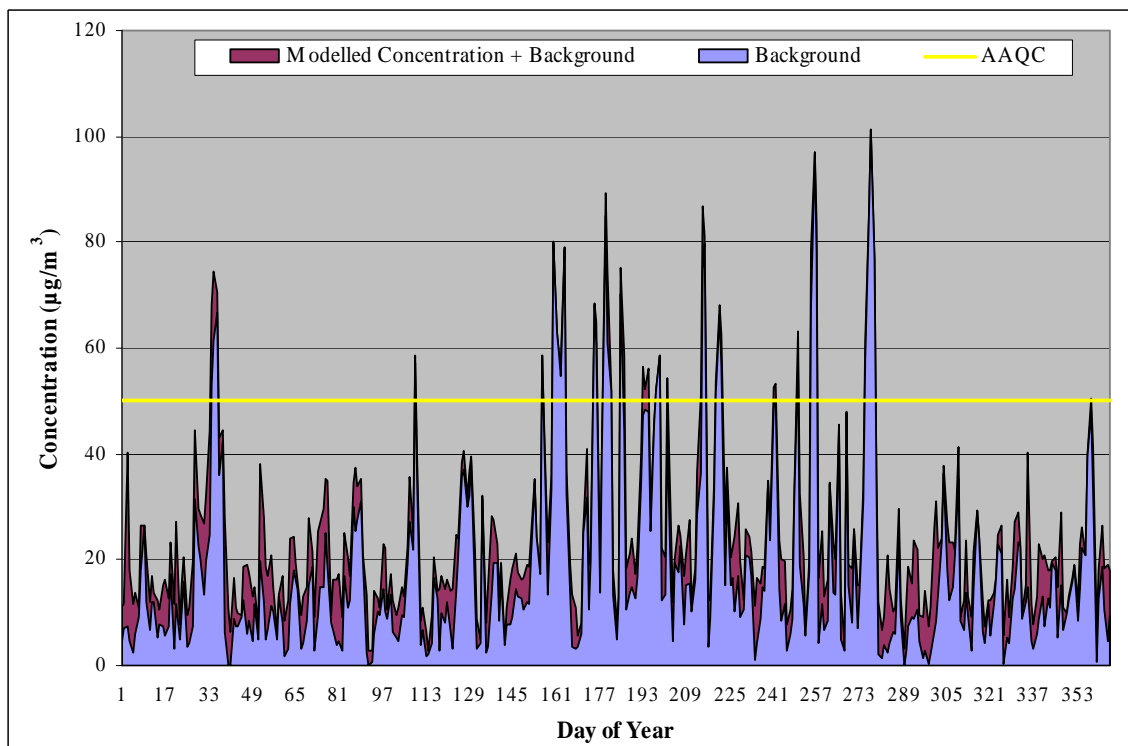


Figure 5.5 Daily PM₁₀ Concentration at R10 using a Variable Background



5.4.4 Control of TSP and PM₁₀ Emissions from the 407 Transitway

Section 4.5 identified all possible sensitive receptors in the study area where an impact on local air quality from the addition of the Transitway may occur. Locations included nine (9) existing/possible future residential areas, and one school, St. Robert Catholic High School. Predicted impacts of TSP and PM₁₀ on local air quality within these residential areas and at the school were summarized in Table 5.4. As was indicated in the table, all receptors with the exception of R5, R7 and R8 were significantly impacted by increased road dust associated with the addition of the Transitway. As a result, it is recommended that road dust impacts of the Transitway be mitigated in and around all significantly impacted residential/sensitive areas.

Control measures are recommended to reduce future impacts of road dust (i.e., TSP and PM₁₀) generated by the 407 Transitway. The U.S. EPA (2006b) recommends road dust controls that either prevent or mitigate high silt loading on roadways. Preventative options include traffic controls such as speed reduction, load restriction etc., whereas mitigative options include road cleaning practices such as vacuum sweeping, water flushing or broom sweeping and flushing combined (U.S. EPA, 2006b).

The U.S. EPA (2006b) remarks that the cost-effectiveness of mitigative options is generally poor and becomes even poorer as the size of an area to be controlled increases. As well, the cost-effectiveness will also be low if there is only a short amount of time required for the silt loading to return to its equilibrium (i.e., for dust to settle back on the roadway) (U.S. EPA, 2006b). Since TSP and PM₁₀ were projected to significantly impact seven sensitive areas along the Transitway, a large area of road would have to be controlled. Moreover, dust will be able to settle back down on the Transitway (in the absence of significant winds) since the volume of buses is too low to continuously suspend road dust into the air so that it can be dispersed by the wind. Additionally, suspended road dust generated by Highway 407 could also settle onto the adjacent Transitway. Therefore, the time to replenish the silt loading on the Transitway is likely to be short and, combined with the fact that a large area of roadway must be controlled, direct mitigative options do not appear to be a feasible method of control.

Moreover, preventative methods are also not a possible control option since the speed and type of vehicle (i.e., buses) cannot be changed on the 407 Transitway.

Since it appears impractical to control the level of silt loading on the Transitway, mitigative measures to reduce the **impact** of road dust at nearby sensitive areas should be undertaken. Barriers (i.e., trees/shrubs, or where planned for safety and/or noise issues solid barriers) located along the Transitway in locations identified as being significantly impacted by road dust will act as screens and significantly reduce (with a 2 metre high screen) the particulate matter flowing horizontally from the roadway (Watson and Chow, 2000). Therefore, planting a tree/shrub

screen adjacent to the Transitway is suggested, where possible, for mitigating impacts of TSP and PM₁₀. Specific areas where barriers are recommended are identified in Table 5.6. At all locations, the barrier should be at least 2 metres high and be planted or installed adjacent to the Transitway. As outlined in the table, it is also recommended that a barrier be created along the west property line of St. Robert Catholic High School because road dust can impact this location when winds blow from a northwest direction.

Mitigation through the planting of trees and shrubs has been considered and incorporated into the preliminary landscape design.

In addition, particulate matter emission estimates may have been overly conservative. Recently (June 2010), the U.S. EPA published draft guidance with an updated methodology for estimating road dust emissions (U.S. EPA, 2010). The revised methodology appears to give significantly lower levels of emissions compared to the U.S. EPA 2006 methods used in this assessment. The draft section proposing the revised calculation methodology as well as supporting documentation can be found at <http://www.epa.gov/ttn/chief/ap42/ch13/index.html>.

If during the detailed design phase of the project the proposed methods become standard practice, the recommendations outlined in Table 5.6 to reduce the impact of particulate matter to nearby sensitive areas should be revisited.

Table 5.6 Recommended Mitigation Options to Minimize Road Dust Impacts

Sensitive Area	Nearby Sensitive Receptor	Recommended Mitigation
Residences on Hartley Court; north of the Transitway, west of the GO Barrie Line	R1	Trees/shrubs or another barrier type for noise and/or safety purposes should be constructed on the north side of the Transitway, east of the GO Barrie rail line if feasible.
Residences on Yellowwood Circle; north of Transitway, east of Dufferin Street	R2	Trees/shrubs or another barrier type for noise and/or safety purposes should be constructed on the north side of the Transitway, beginning at Yellowwood Circle and ending at Thornhill Woods Drive if feasible.
Residences on Sassafras Circle; Daniel Reaman Cres. and Lander Cres., north of Transitway, east of Langstaff Road	R3	
Residences on Langstaff Road W; west of Transitway	R4	Since the Transitway is elevated in this area, it will not be possible to use a separate barrier as a mitigation option. Safety barriers constructed on the Transitway overpass at Yonge Street will block and retain some of the road dust at the base of the safety barrier.
Residence on Cedar Avenue, south of Transitway	R5	This area is not significantly impacted by the addition of the Transitway.
Apartment building, northeast corner of Bayview Avenue and Highway 7	R6	This section of the Transitway is below grade (approximately 8 m) and as a result, a retaining wall will be built on either side of the Transitway. This will act as a barrier and retain road dust at the base of the retaining wall.
Potential residential development, south of South Park Road	R7	This area is not significantly impacted by the addition of the Transitway.
Residences on Huntington Park Dr; south of Transitway	R8	This area is not significantly impacted by the addition of the Transitway.
Potential residential development north of Transitway, east of Warden Avenue	R9	If residences are ever constructed, trees/shrubs or another barrier type for noise and/or safety purposes will have to be constructed by the future builder on the north side of the Transitway from approximately the Markham Centre Tributary to the Stouffville Line where necessary.
St. Robert Catholic High School, south of Transitway, east of Leslie Street	R10	Trees/shrubs or another barrier type for noise and/or safety purposes should be constructed on the south side of the Transitway, just east of Leslie and extending approximately 500 m eastward. As well, it is recommended that trees be planted along the west property line of St. Robert Catholic High School. The trees and shrubs should form a visual boundary between the school and the Transitway.

5.5 GRAPHICAL PRESENTATION OF RESULTS - PM_{2.5}

The maximum 24-hour average modelled concentrations for PM_{2.5} for all three scenarios are presented with contour lines over a base map in Figures 5.6a through 5.6c. The contours are lines of equal predicted maximum 24-hour concentrations. As outlined in Section 5.3 above, these maximum concentrations do not occur simultaneously, but are the maximum 24-hour concentrations predicted at each grid point during a one year period added to a conservatively high background concentration.

It can be seen in the figures and Table 5.7 that the predicted PM_{2.5} concentrations decrease for the future (2031) scenario without the Transitway. This is a result of emission reductions resulting from advancements in fuel and vehicle technologies, despite the predicted increases in traffic due to population growth. As indicated in Table 3.1 above, the PM_{2.5} emission factor for cars in 2031 is approximately 43% of the emission factor in 2008 and 10% for trucks/buses. In contrast, predicted PM_{2.5} concentrations increase at all but two receptor locations (R5 and R7) for the future (2031) scenario with the Transitway. Although the MOBILE6C PM_{2.5} emission factor decreases in the future, the addition of the 407 Transitway increases road dust emissions significantly and also shortens the distance between some receptors and the nearest source of emissions (i.e., roads). The greatest predicted increase from existing conditions to the Future With the 407 Transitway scenario is 12.6% at receptor R10.

As outlined in Section 3.1.3 above, AP-42 Section 13.2.1 – Paved Roads indicates that there may be situations where low silt loading and/or low average vehicle weight will yield calculated negative emissions. If this occurs, AP-42 Section 13.2.1 recommends the calculated PM_{2.5} road dust emissions be set to zero. Keeping in mind the background value for PM_{2.5} (17.5 µg/m³), Figures 5.6a and 5.6b suggest little PM_{2.5} emissions from vehicle traffic along the majority of Highway 407. This is a result of low silt loading due to Highway 407 segments having 24-hour AADT (annual average daily traffic) counts greater than 10,000 which will result in zero predicted emissions from the fine component of road dust. In contrast, roadways with a 24-hour AADT (annual average daily traffic) count less than 10,000 (i.e., the 407 Transitway) will emit PM_{2.5} road dust emissions. Also, the average vehicle weight on the Transitway is greater than Highway 407 since it is occupied only by buses. Thus, the increased PM_{2.5} concentrations shown in Figure 5.3c are a result of low 24-hour AADT counts and a higher average vehicle weight on the Transitway which causes more road dust to be generated.

The figures below also suggest that PM_{2.5} behaves differently from PM₁₀ and TSP. As discussed in Section 5.4.2, PM₁₀ and TSP concentrations are primarily a function of mechanically generated dust whereas PM_{2.5} is typically a function of tailpipe emissions.

The predicted 24-hour maximum concentrations at the ten sensitive receptors for the future with and without the 407 Transitway (2031) for PM_{2.5} are presented in Table 5.8. The table indicates there will be some significant air quality impacts as a result of the proposed bus rapid transit system, namely at R10. As with PM₁₀, the greatest predicted impact of PM_{2.5} occurred at R10 with an increase of 12.6% compared to the future scenario without the Transitway. As discussed previously, R10 and the Transitway are only separated by a distance of about 40 metres, whereas the distance between Highway 407 and R10 is 120 metres. Due to the close proximity of R10 to the 407 Transitway and the increased amount of road dust emissions on the Transitway, an impact on air quality is to be expected.

Tables 5.6 and 5.7 also show that the background concentration of 17.5 µg/m³ represents the majority of the overall estimated PM_{2.5} concentrations. As well, there are no predicted exceedances of the proposed Canada Wide Standard for PM_{2.5} at any of the receptor locations.

Table 5.7 Maximum 24-hour PM_{2.5} Concentrations – Existing and Future Scenarios

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		Canada-Wide Standard
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	18.2	17.8	-2.2%	18.7	2.5%	30
R2	18.2	17.8	-2.1%	18.9	4.0%	30
R3	18.6	18.0	-3.4%	19.0	1.8%	30
R4	18.4	17.9	-2.7%	19.0	3.4%	30
R5	18.8	17.9	-4.7%	18.4	-2.0%	30
R6	18.1	17.7	-1.9%	18.5	2.5%	30
R7	18.6	18.0	-3.5%	18.6	-0.3%	30
R8	17.9	17.7	-1.2%	18.0	1.0%	30
R9	18.2	17.9	-1.7%	19.0	4.5%	30
R10	18.2	17.8	-2.2%	20.5	12.6%	30

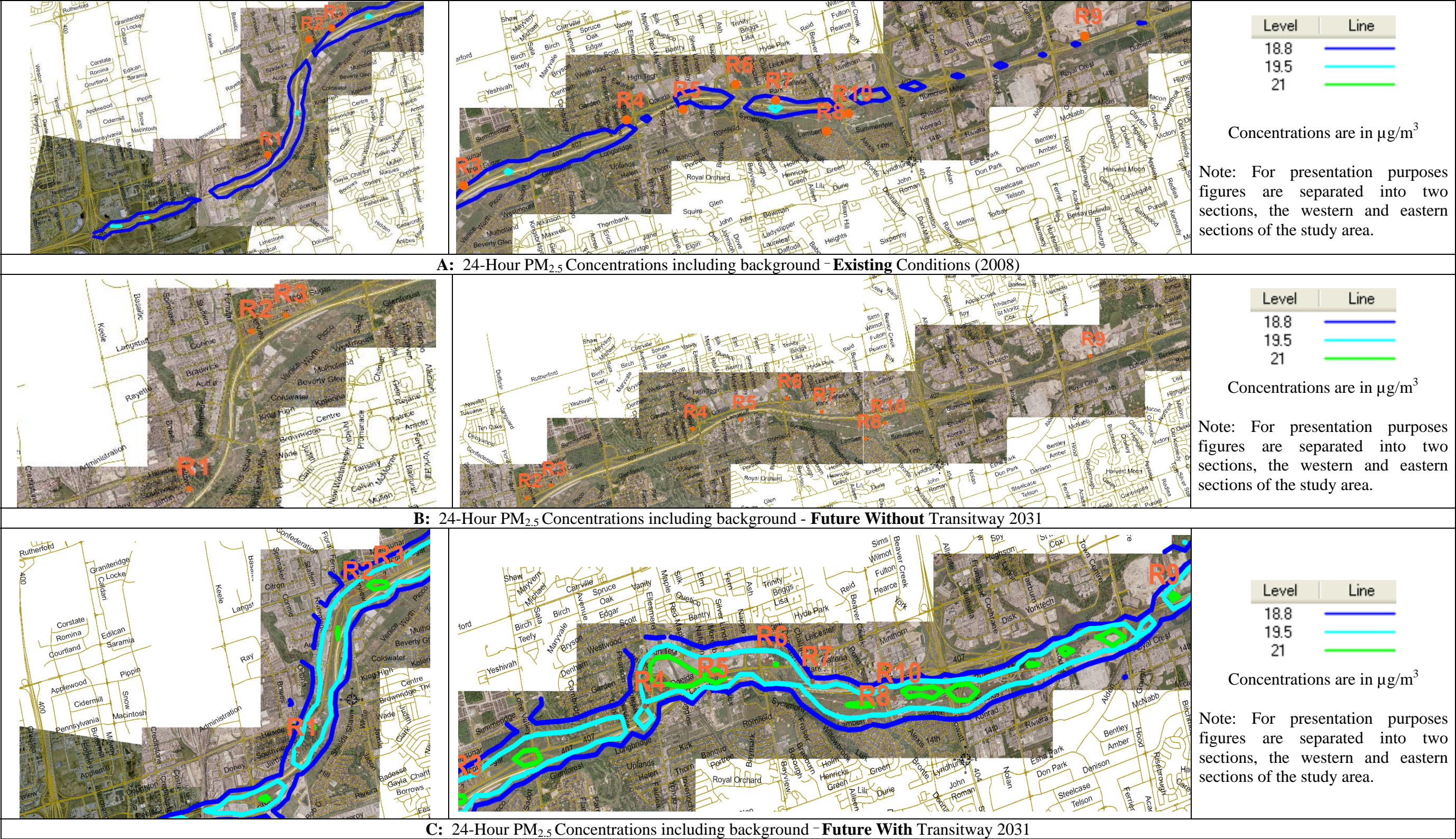
Note: All values include a background PM_{2.5} concentration of 17.5 µg/m³.

Table 5.8 Maximum 24-hour PM_{2.5} Concentrations – Future Scenarios Comparison

Receptor	Future Without Transitway (µg/m³)	Future With Transitway (µg/m³)	% Change from Without Transitway	Canada-Wide Standard (µg/m³)
R1	17.8	18.7	4.8%	30
R2	17.8	18.9	6.2%	30
R3	18.0	19.0	5.3%	30
R4	17.9	19.0	6.3%	30
R5	17.9	18.4	2.8%	30
R6	17.7	18.5	4.5%	30
R7	18.0	18.6	3.4%	30
R8	17.7	18.0	2.2%	30
R9	17.9	19.0	6.3%	30
R10	17.8	20.5	15.2%	30

Note: All values include a background PM_{2.5} concentration of 17.5 µg/m³.

Figure 5.6 Maximum 24-hour PM_{2.5} Concentrations for Existing and Future Scenarios



5.6 STATION MODELLING RESULTS

Detailed results of the station modelling are provided in Appendix D. In all, the assessment showed that the additional impact of the Leslie and GO Barrie (Concord) stations on air quality is negligible. Since these stations were considered to represent the worst-case scenarios, impacts from the remaining stations will also be negligible.

5.7 POLLUTANT BURDEN ANALYSIS OF GREENHOUSE GASES

To assess the potential changes in greenhouse gas (GHG) pollutant burden within the study area based on the addition of the 407 Transitway, contaminant emissions of CO₂, CH₄, and N₂O in terms of CO_{2e} were calculated for all three assessment scenarios.

The results of the pollutant burden analysis are presented below for CO_{2e}. Complete results for the individual gases are presented in Appendix F.

5.7.1 Carbon Dioxide Equivalent (CO_{2e})

As outlined in Table 5.9 below, the annual CO_{2e} pollutant burden within the study area corridor is estimated to increase by approximately 83% in the future. Since the CO₂ emission factor will increase in the future (Table 3.1) along with the volume of traffic in response to population growth, the CO_{2e} pollutant burden will also increase. When comparing the two future scenarios, it can be seen that there is a very small reduction in annual CO_{2e} pollutant burden (about 1 kilotonne or 0.2%). This small difference is based on approximately the same number of vehicles occupying Highway 407, but with the future bus fleet moved to the 407 Transitway. It was estimated that for the future scenario **without** the Transitway, buses would travel an approximate distance of 24.5 km on Highway 407. In contrast, buses would travel 23 km on the Transitway, accounting for this small reduction in CO_{2e} pollutant burden. Note that this difference is within the error of estimating the distances travelled by the Highway 407 and the Transitway vehicle fleets. Therefore, the difference in the annual CO_{2e} pollutant burden between the two future scenarios is negligible.

Table 5.9 CO_{2e} Pollutant Burden

Scenario	CO _{2e} Pollutant Burden in kilotonnes/year	% Change from Existing Conditions in kilotonnes/year
Existing Conditions (2008)	344	-
Future Without Transitway (2031)	632	+83.4%
Future With Transitway (2031)	631	+83.1%

A negligible change in annual CO_{2e} pollutant burden due to the addition of the 407 Transitway was estimated in the above table. However, future traffic volume estimates were based on expected increases in population growth and did not take into consideration the number of vehicles that may be taken off of the road when the 407 Transitway is in full operation. As a result, it is difficult to quantify the change in annual GHG pollutant burden due to the addition of the Transitway.

6.0 CONCLUSIONS AND MITIGATION PLAN

6.1 CONCLUSIONS

6.1.1 Discussion of Existing Conditions

The results of the study show, through monitoring and modelling, that the existing air quality in the study area is typical of an urban setting, which is characterized by elevated pollutant concentrations in relation to rural areas, with periodic compromised air quality due to nitrogen oxides and fine particulate based contaminants, which typically occur during smog events.

Available historical monitoring data near to the study area indicates that:

- CO concentrations are well within all applicable standards;
- PM_{2.5} concentrations periodically exceed the 24-hour Canada-Wide standard; and
- NO_x concentrations periodically exceed the 1-hour and 24-hour AAQC standards, typically during smog events.

6.1.2 Comparison of Existing Conditions with Future Scenarios

For both future scenarios with and without the 407 Transitway (2031), the study identifies that compared to existing conditions (2008), air quality will slightly improve for gaseous pollutants due to newer engine technologies and fuels, despite predicted increases in traffic resulting from population growth. However, air quality will deteriorate for particulate based compounds due to:

- increased traffic flow on Highway 407 resulting from population growth in the future and/or,
- increased road silt accumulation as a result of low bus volumes/heavier vehicles on the 407 Transitway.

Additionally, the annual pollutant burden of carbon dioxide equivalent (CO_{2e}) is expected to increase in the future as a result of increased traffic volumes due to population growth, coupled with an increase in the MOBILE6C emission factor for carbon dioxide (CO₂).

6.1.3 Comparison of Future Scenarios

The results show that within the study area, when compared to the future no-build scenario (2031), adding the 407 Transitway will result in:

- negligible changes in gaseous pollutant concentrations and greenhouse gases (GHGs) throughout the study area;

- a slight increase in PM_{2.5} (particulate matter less than 2.5 µm in diameter) concentrations, particularly at receptors whose distance from a roadway (emission source) decreases with the addition of the Transitway;
- an increase in total suspended particulate (TSP) and PM₁₀ (particulate matter less than 10 µm in diameter) concentrations throughout the study area;
- approximately a 2% to 40% increase in TSP and PM₁₀ concentrations at sensitive receptor locations adjacent to the 407 Transitway; and,
- negligible changes in gaseous and particulate matter concentrations when station parking lot and passenger pick-up and drop-off (PPUDO) emissions are considered.

In all, the implementation of a 23 kilometre bus rapid transit system from Highway 400 to Kennedy Road in the municipalities of Vaughan, Richmond Hill and Markham, Ontario will result in increases in particulate matter (mainly TSP and PM₁₀) concentrations at sensitive receptor locations within the study area. The ambient air quality criterion for TSP is based on visibility, and the criterion for PM₁₀ is based on health effects. Therefore, the study shows that there will be an appreciable increase in one contaminant (PM₁₀) with health based standards. The recommended broad-based mitigation measures outlined below are proposed to reduce PM₁₀ impacts, and will also reduce TSP impacts.

6.2 BROAD-BASED MITIGATION PLAN

Mitigation measures are recommended to reduce future particulate based (TSP and PM₁₀) air quality impacts from the 407 Transitway which includes increased tree planting or constructing other solid barriers for noise and/or safety purposes adjacent to the Transitway which are at least 2 metres tall where possible. Trees/shrubs or solid barriers for noise and/or safety purposes located along the Transitway will act as screens and significantly reduce the particulate matter emission rate for material flowing horizontally from the roadways (Watson and Chow, 2000). In particular, it is recommended that trees be planted (or a solid barriers for noise and/or safety purposes be constructed) adjacent to the Transitway near St. Robert Catholic High School (receptor R10) and existing/planned residential areas with the exception of receptors R5, R6, R7, R8 and R9. Table 5.6 provided a summary of recommended mitigation options.

Mitigation through the planting of trees and shrubs has been considered and incorporated into the preliminary landscape design.

In addition, particulate matter emission estimates may have been overly conservative. Recently (June 2010), the U.S. EPA published draft guidance with an updated methodology for estimating road dust emissions (U.S. EPA, 2010). The revised methodology appears to give significantly lower levels of emissions compared to the U.S. EPA 2006 methods used in this assessment. The

draft section proposing the revised calculation methodology as well as supporting documentation can be found at <http://www.epa.gov/ttn/chief/ap42/ch13/index.html>.

If during the detailed design phase of the project the proposed methods become standard practice, the recommendations outlined in Table 5.6 to reduce the impact of particulate matter to nearby sensitive areas should be revisited.

The construction of the 407 Transitway has the potential to affect the air quality in the vicinity of the site during the construction phase. As with any construction site, these emissions will be of relatively short duration and are unlikely to have any long-lasting effect on the surrounding area. Dust impacts should be mitigated through the use of proper controls, such as:

- periodic watering of unpaved (non-vegetated) areas;
- periodic watering of an material stockpiles;
- limiting the speed of construction vehicular travel;
- use of water sprays during the loading, unloading of materials; and
- sweeping and/or water flushing of the entrances to the construction zones.

These types of controls aid in minimizing the impacts on the environment during the construction phase. Night time construction activities should also be considered in order to reduce emissions from vehicles that are slowed down by any reduced road capacity during the day.

6.3 CONSERVATIVE NATURE OF ASSESSMENT

The air quality impact assessment is considered to be conservative based on the following:

- Industry standard conservative 90th percentile background monitoring values were added to model predicted contaminant concentrations;
- Background monitoring data for PM₁₀ and TSP was not available, therefore, the conservative assumption was made that PM₁₀ background concentrations are twice PM_{2.5} and TSP background concentrations are twice PM₁₀;
- The future with Transitway scenario assumes no reduction in vehicle traffic on Highway 407, however, based on discussions with the MTO and Delcan, it is reasonable to assume that the introduction of the 407 Transitway into the study area will reduce the number of vehicles present within the transportation corridor (i.e., Highway 7 and other regional roads); and,
- Recently (June 2010), the U.S. EPA published draft guidance with an updated methodology for estimating road dust emissions (U.S. EPA, 2010). The revised methodology appears to give significantly lower levels of emissions compared to the U.S. EPA 2006 methods used in this assessment.

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APPENDIX A

**GRAPHICAL PRESENTATION OF
MODELLING RESULTS**

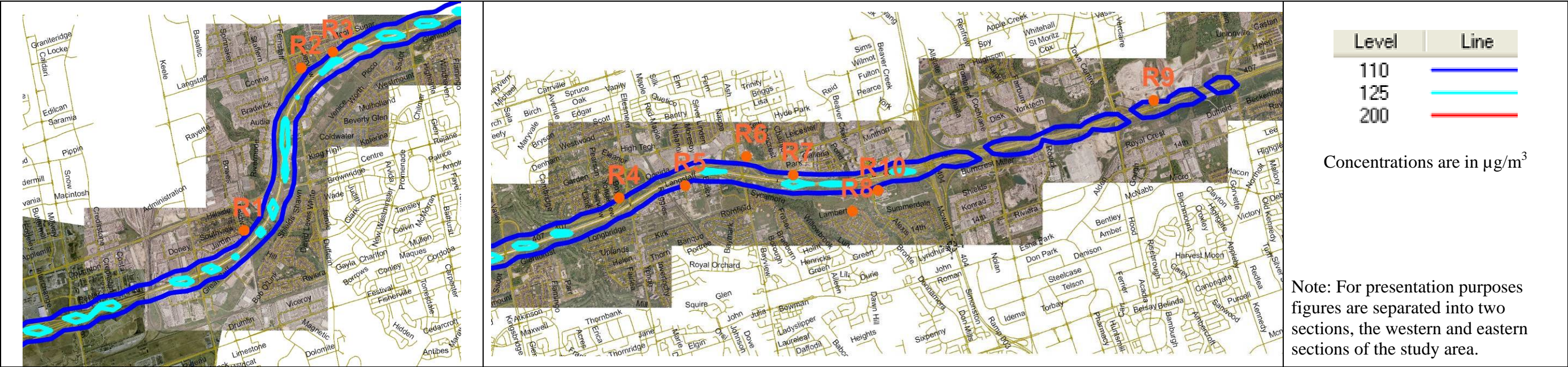


Figure A.1a 24-Hour NO_x Concentrations including background in $\mu\text{g}/\text{m}^3$ - **Future Without Transitway (2031)**

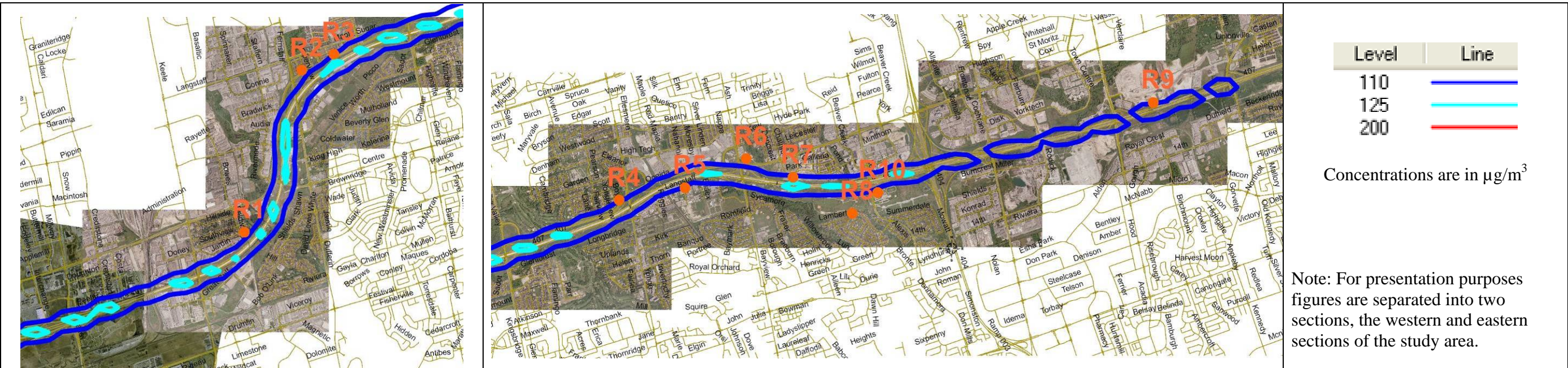
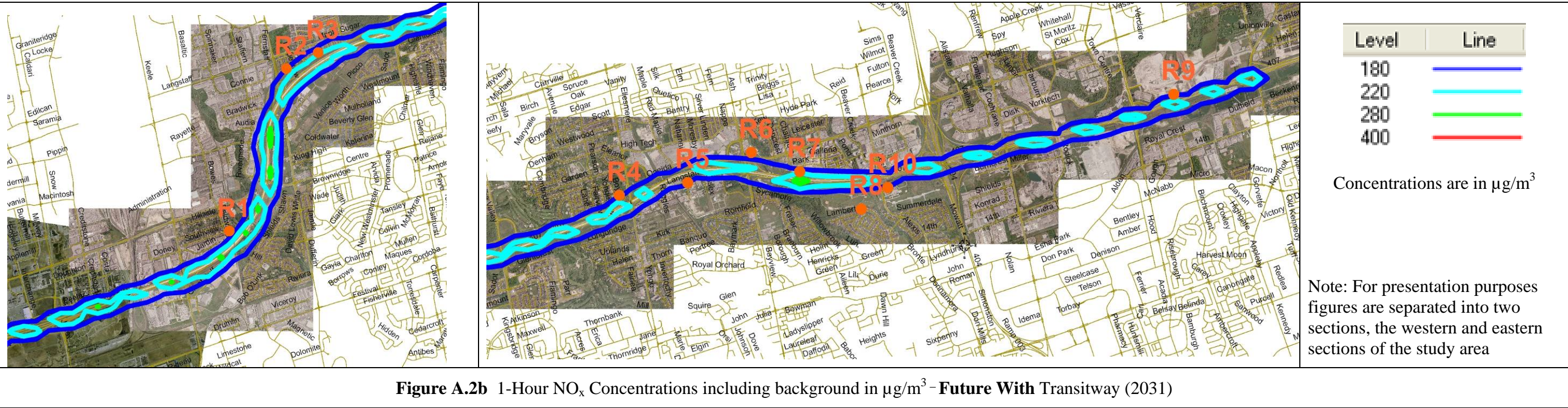
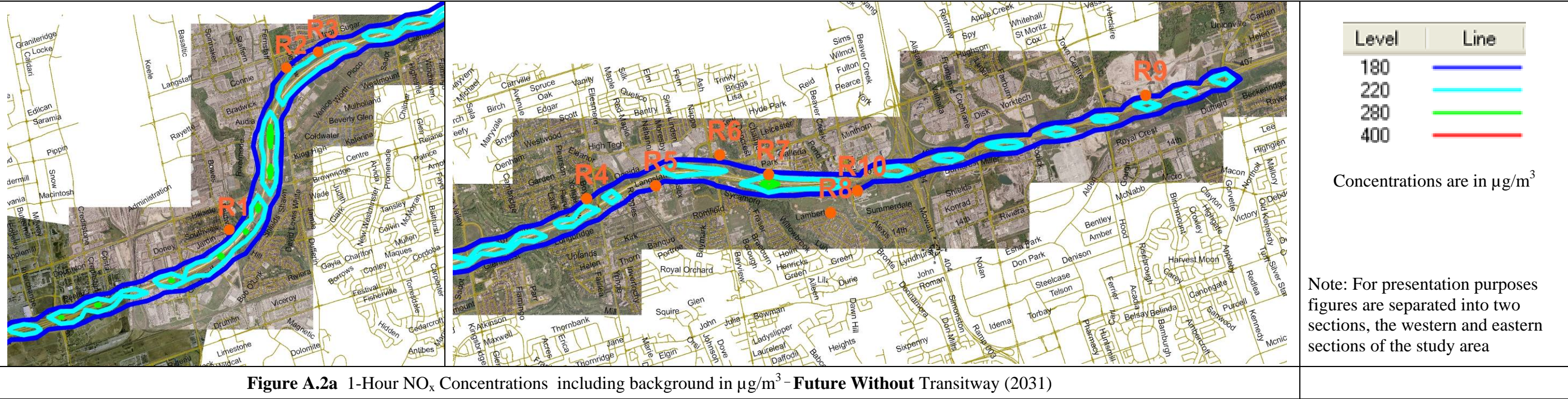
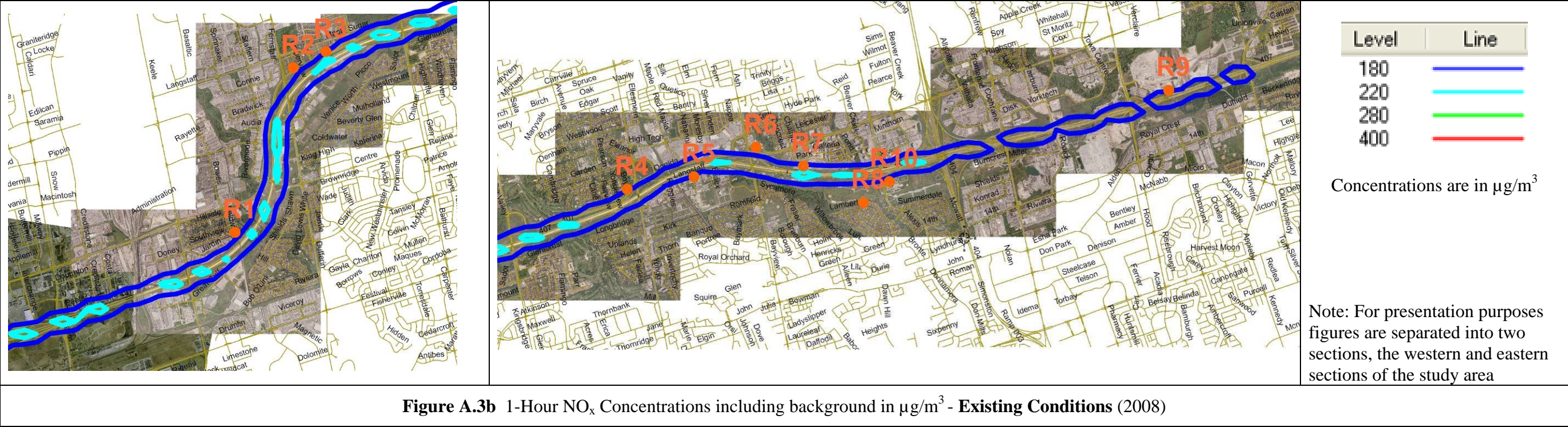
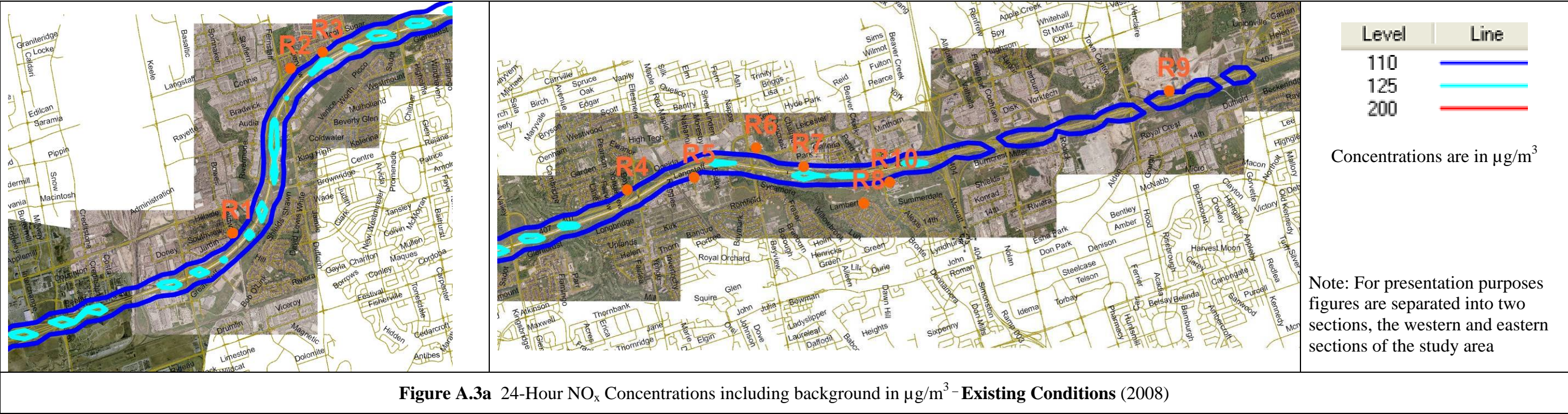
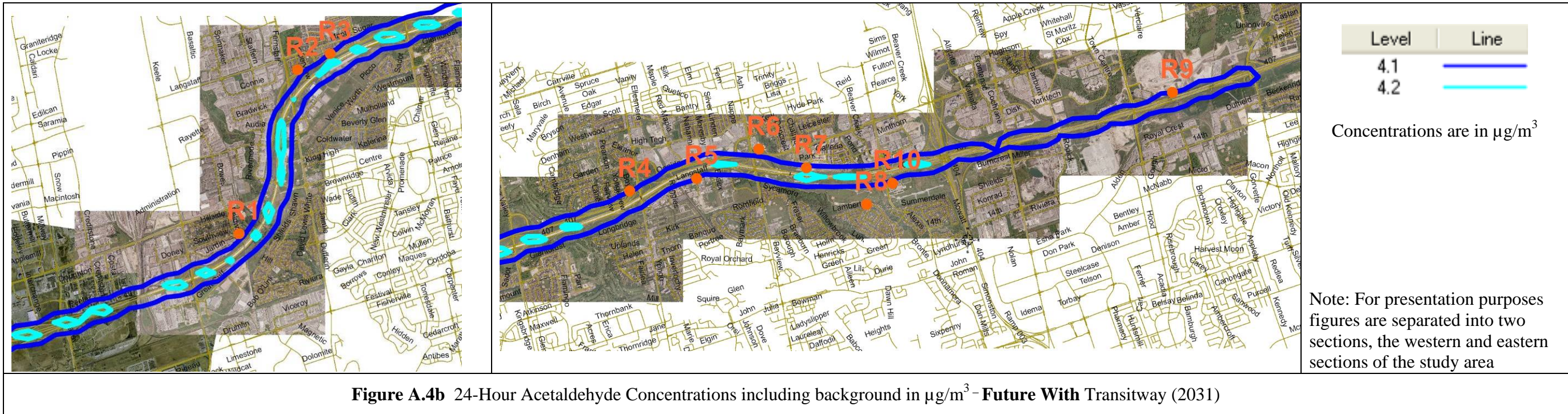
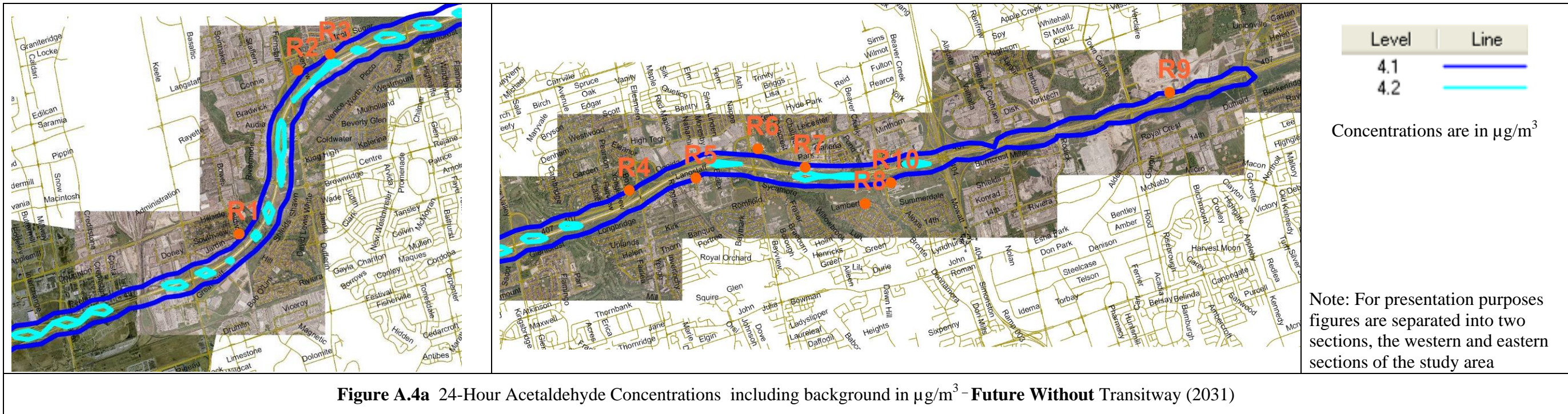
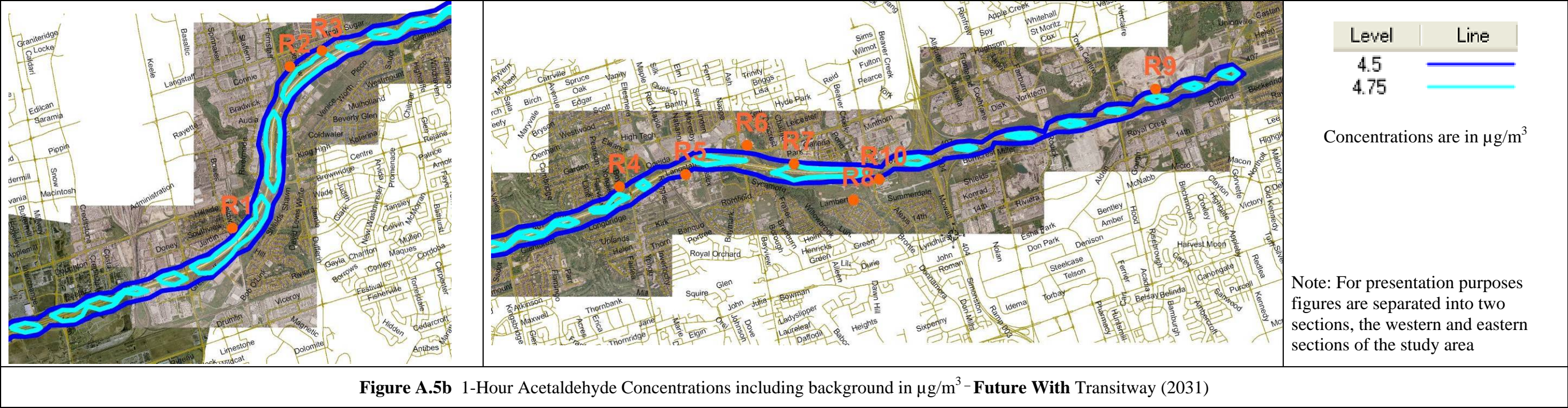
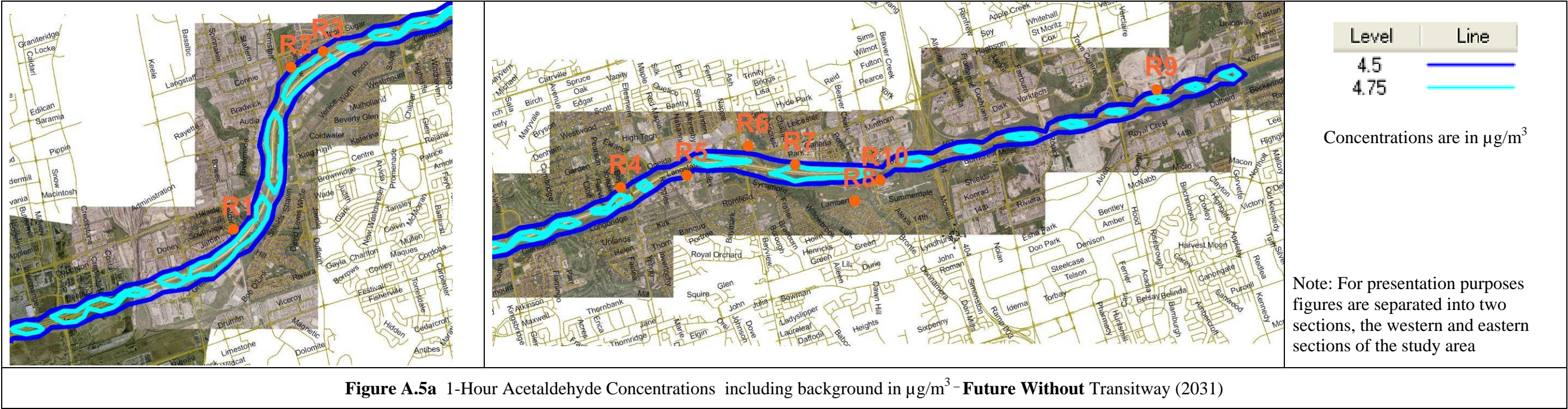


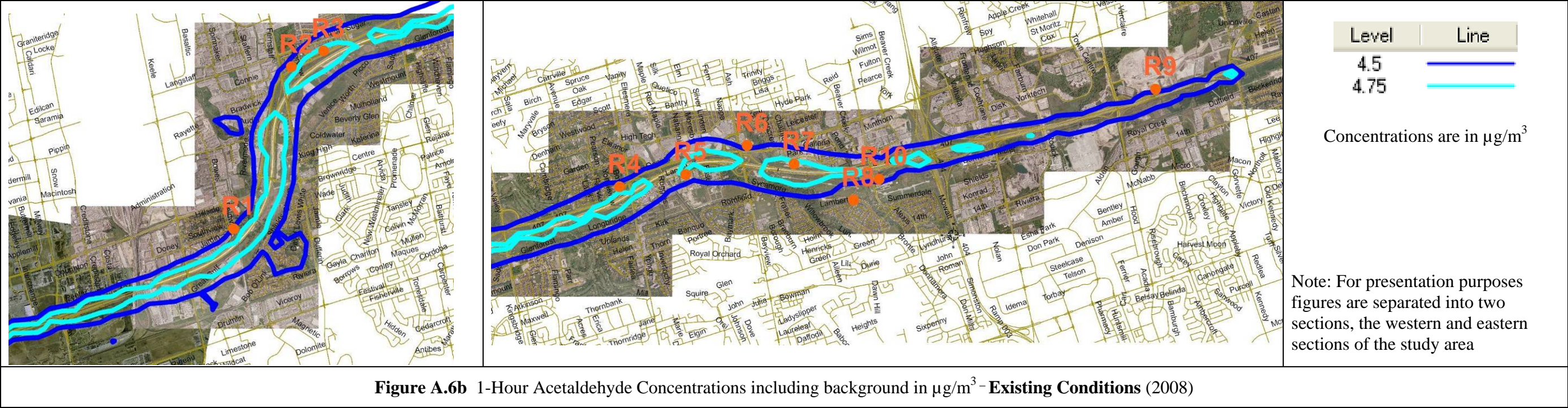
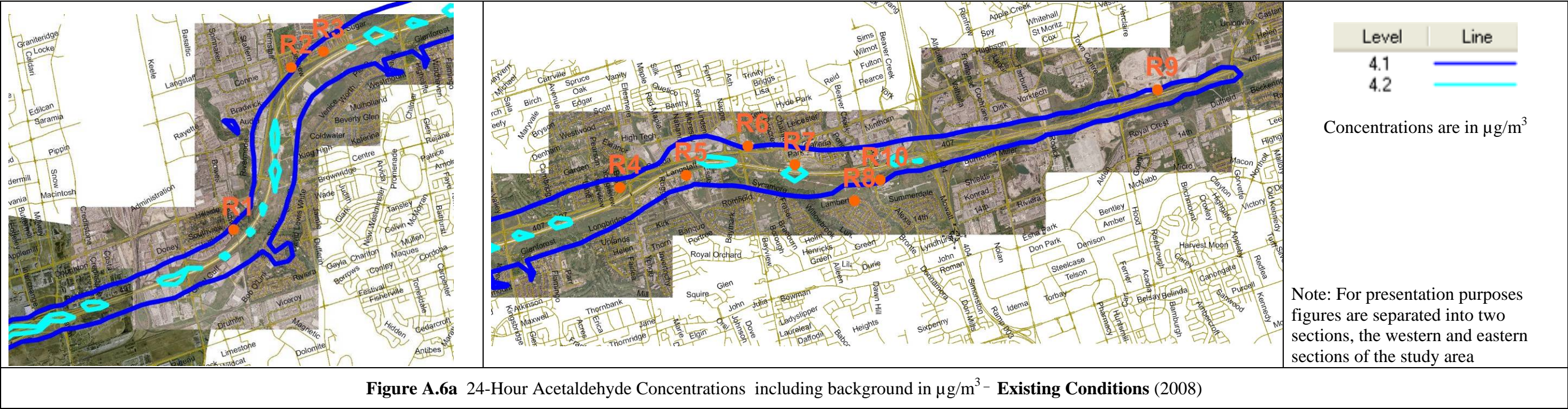
Figure A.1b 24-Hour NO_x Concentrations including background in $\mu\text{g}/\text{m}^3$ - **Future With Transitway (2031)**

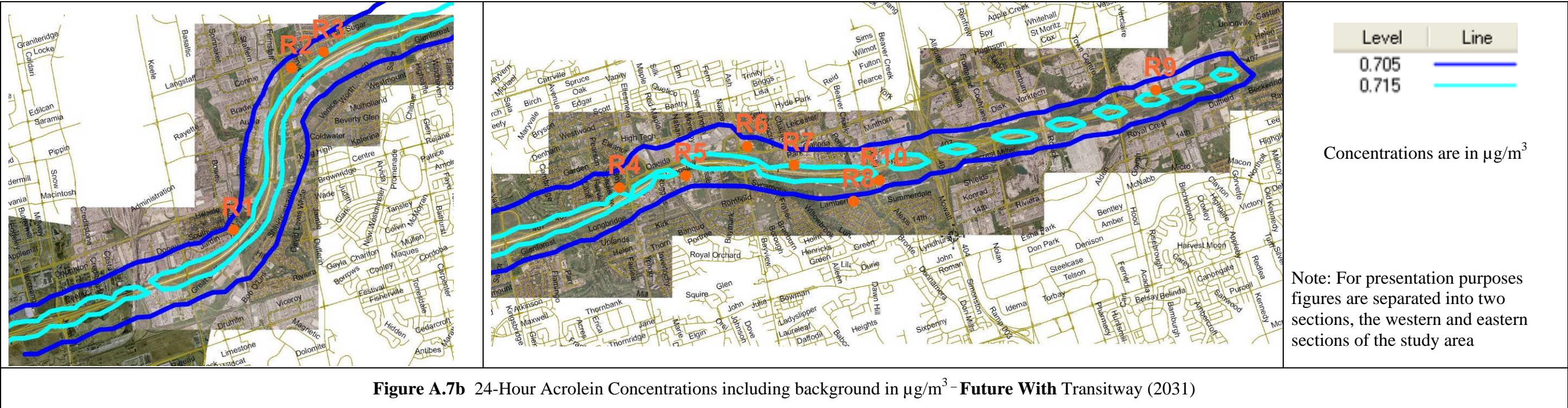
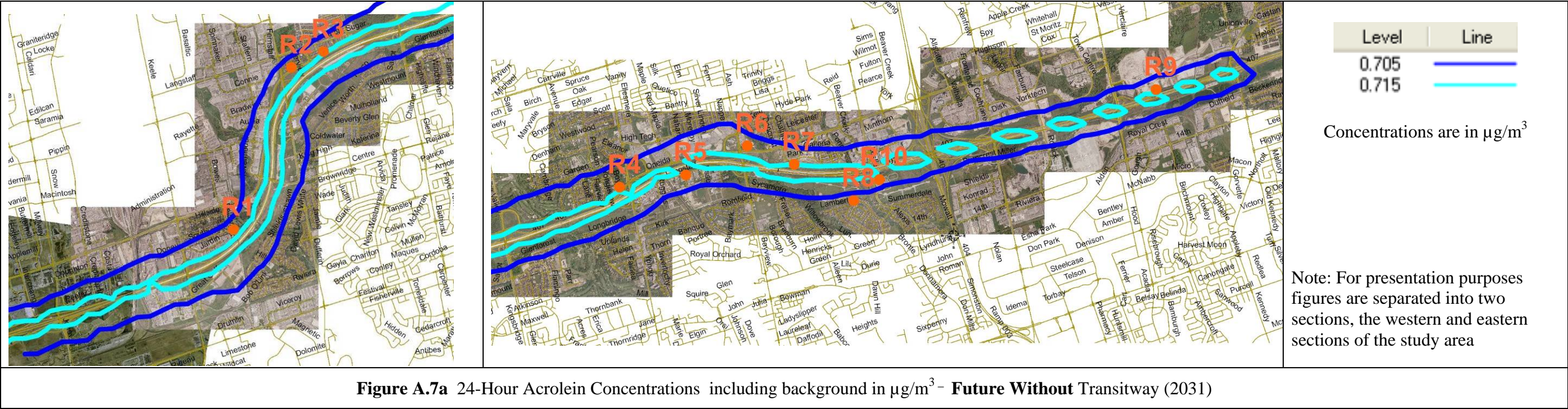


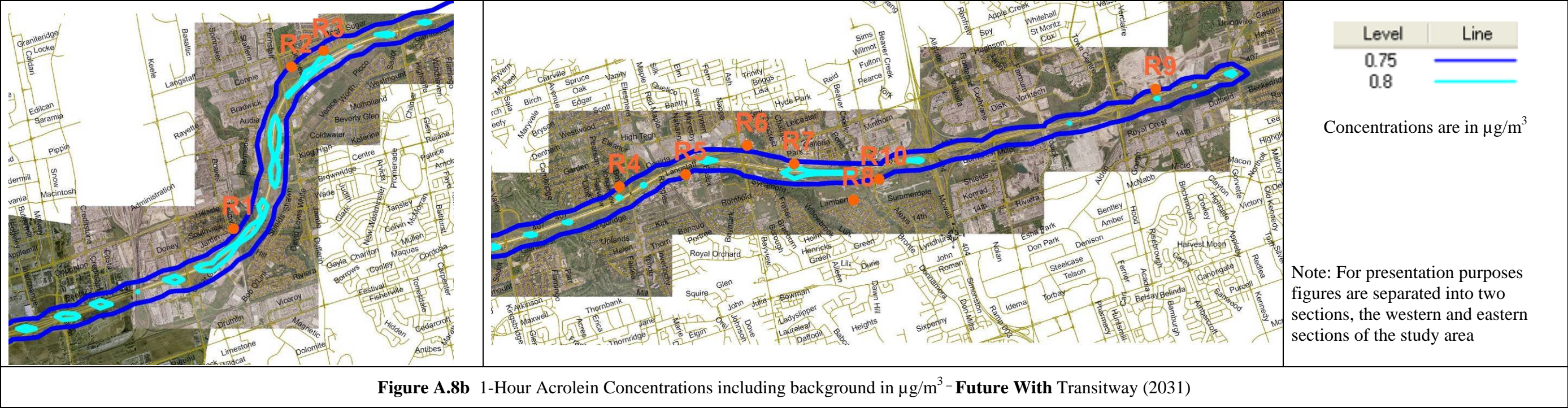
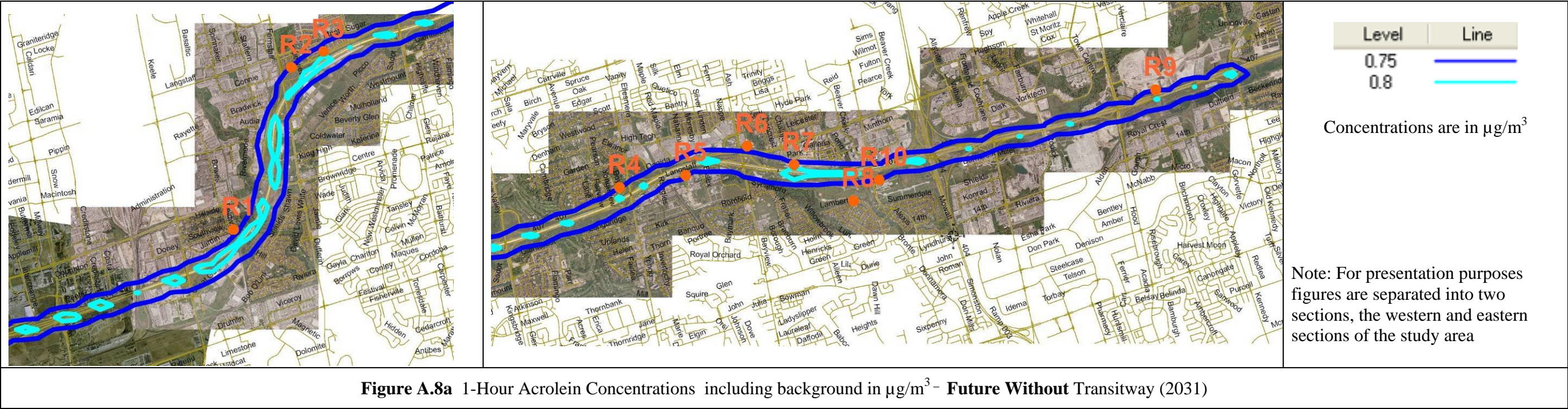


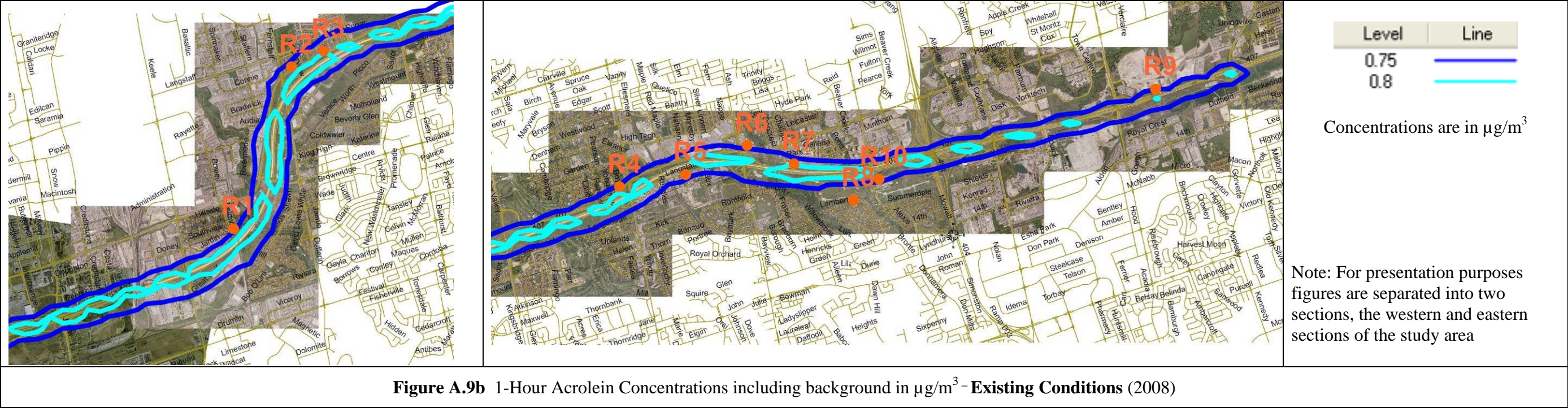
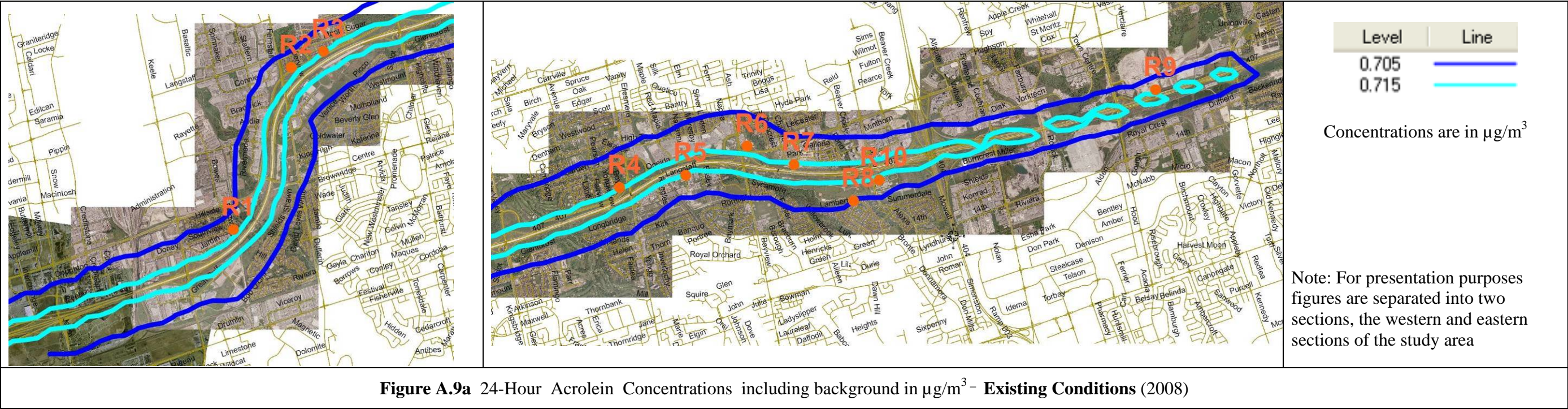












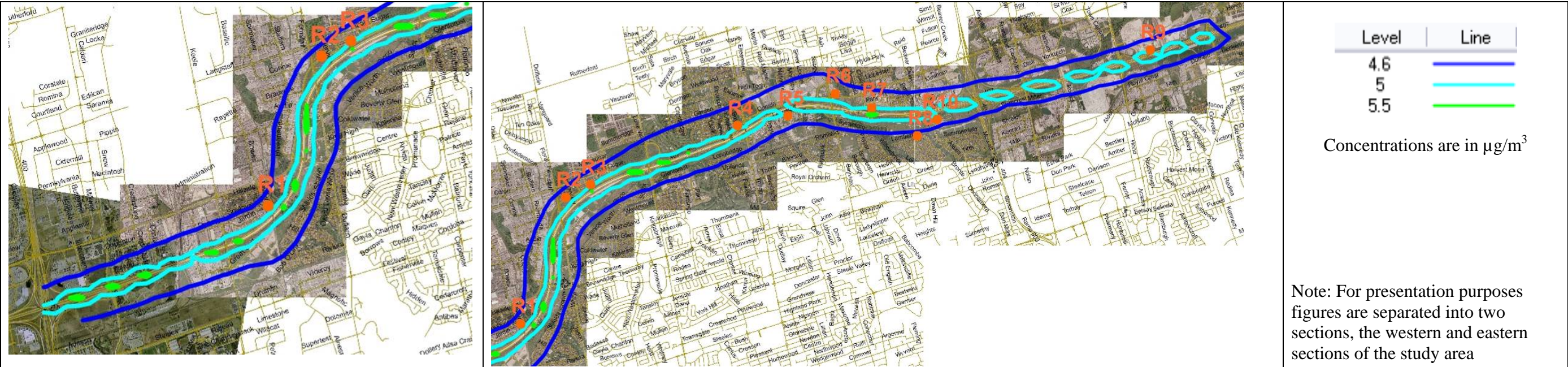


Figure A.10a 24-Hour Benzene Concentrations including background in $\mu\text{g}/\text{m}^3$ - **Future Without Transitway (2031)**

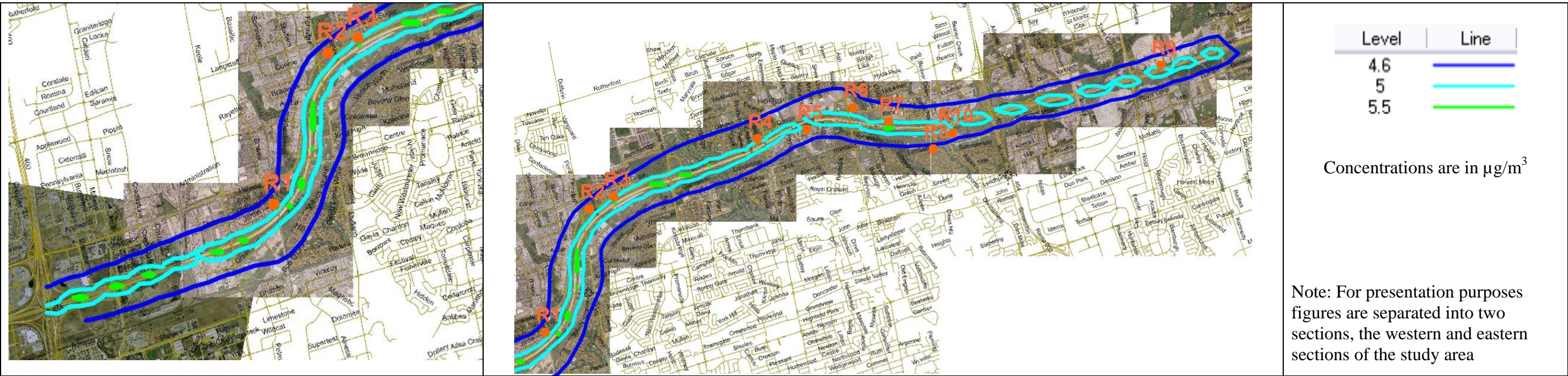


Figure A.10b 24-Hour Benzene Concentrations including background in $\mu\text{g}/\text{m}^3$ - **Future With Transitway (2031)**

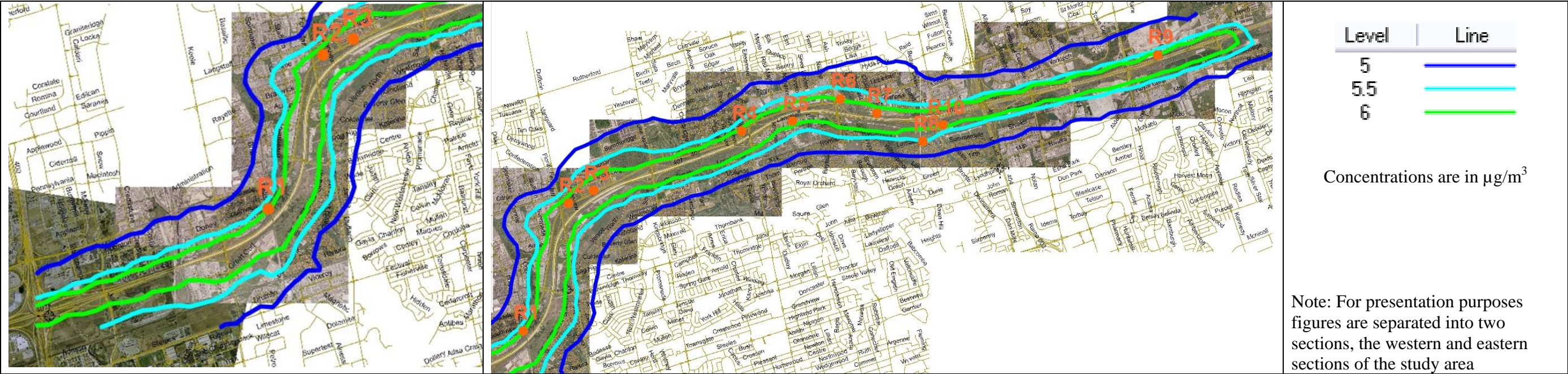


Figure A.11a 1-Hour Benzene Concentrations including background in $\mu\text{g}/\text{m}^3$ - **Future Without** Transitway (2031)

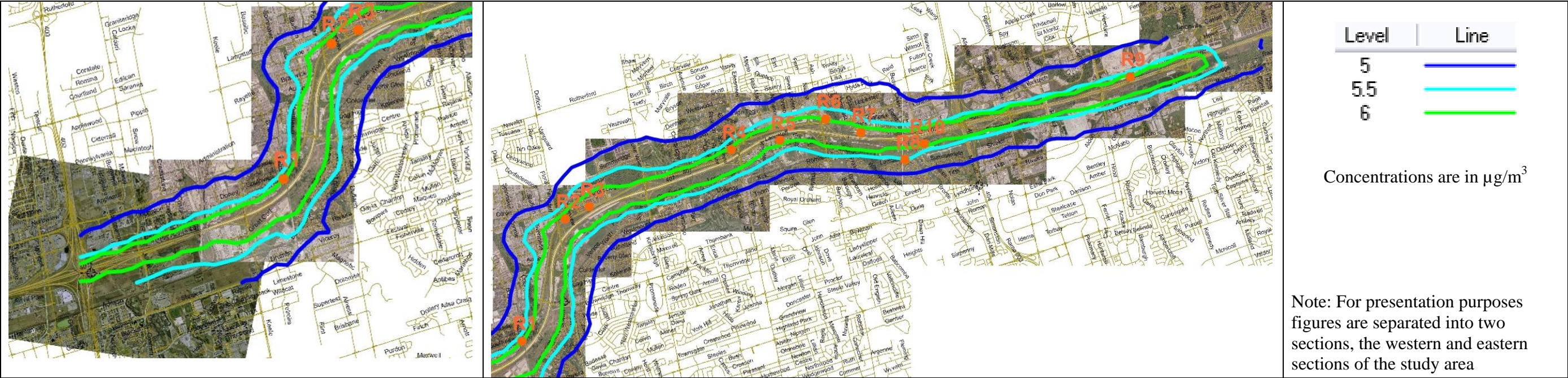
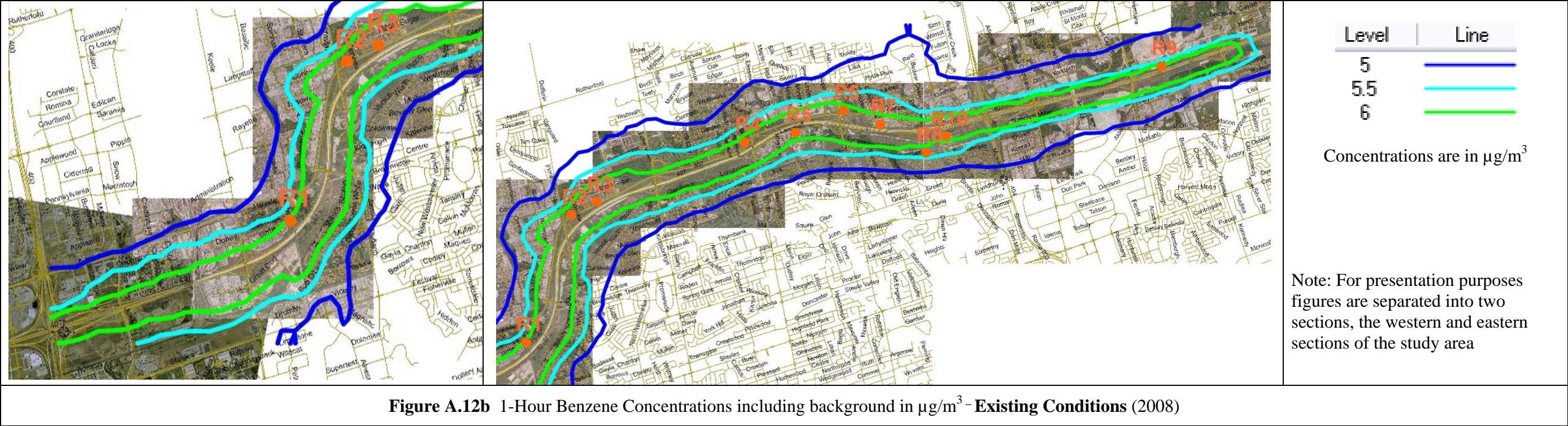
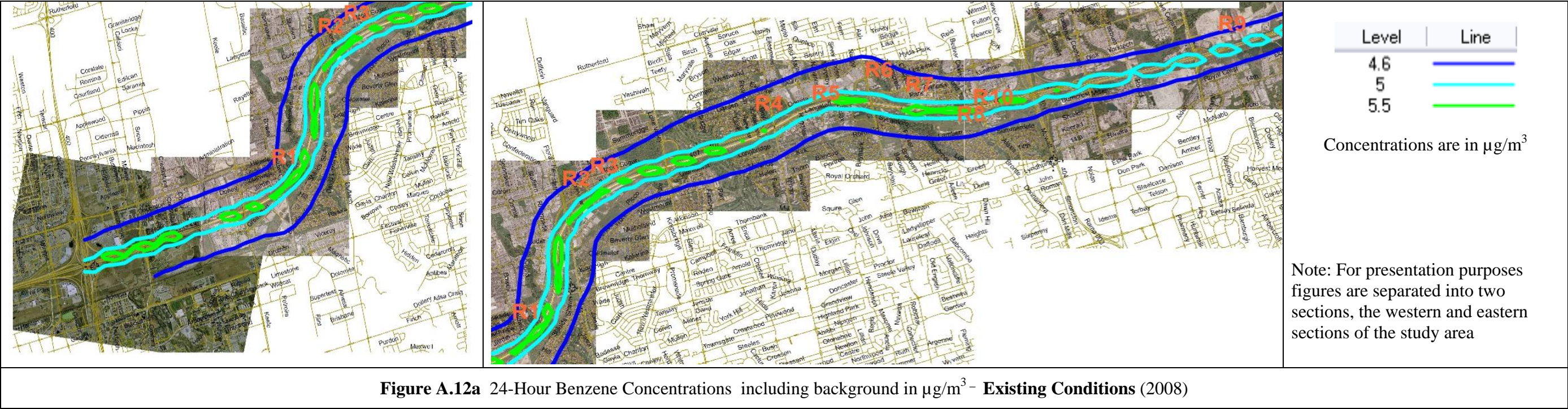
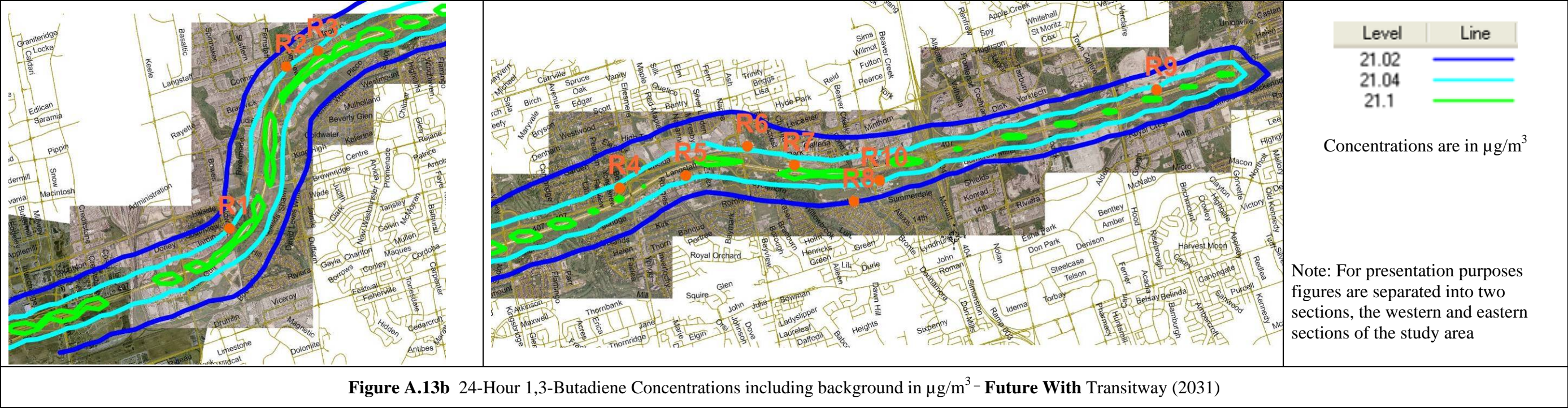
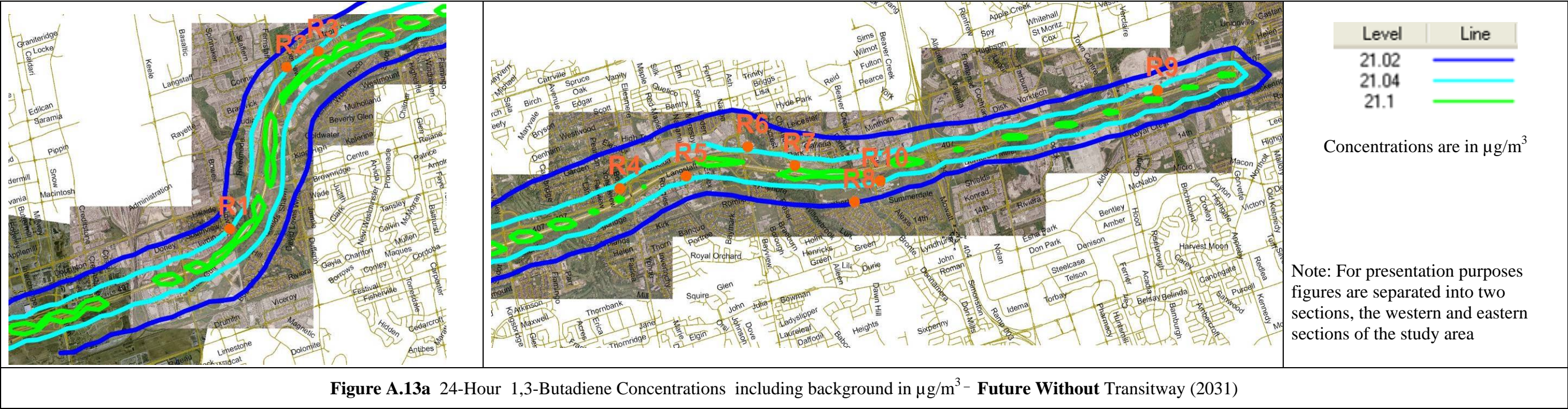
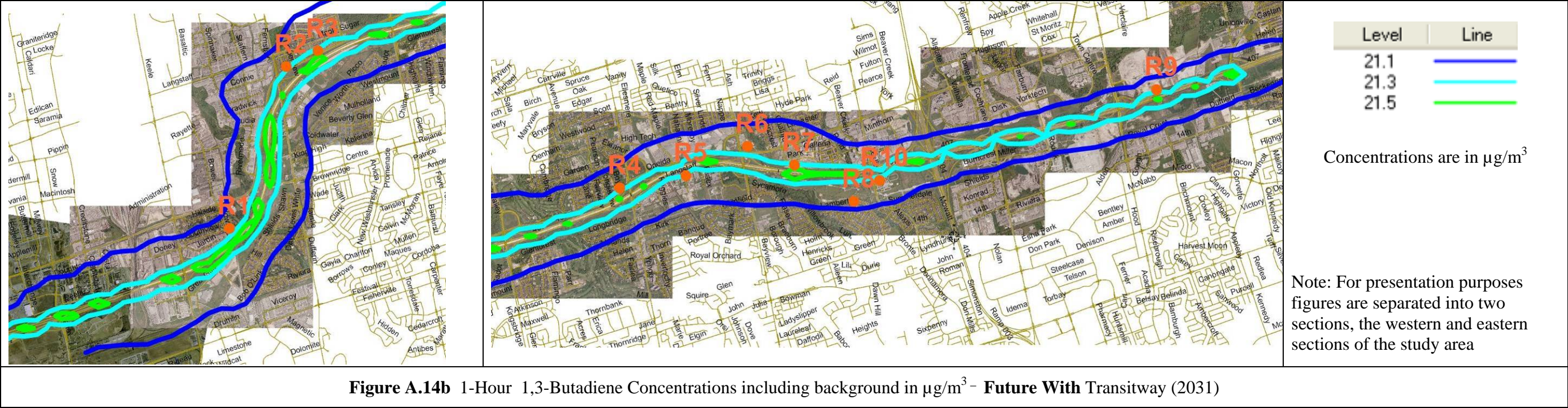
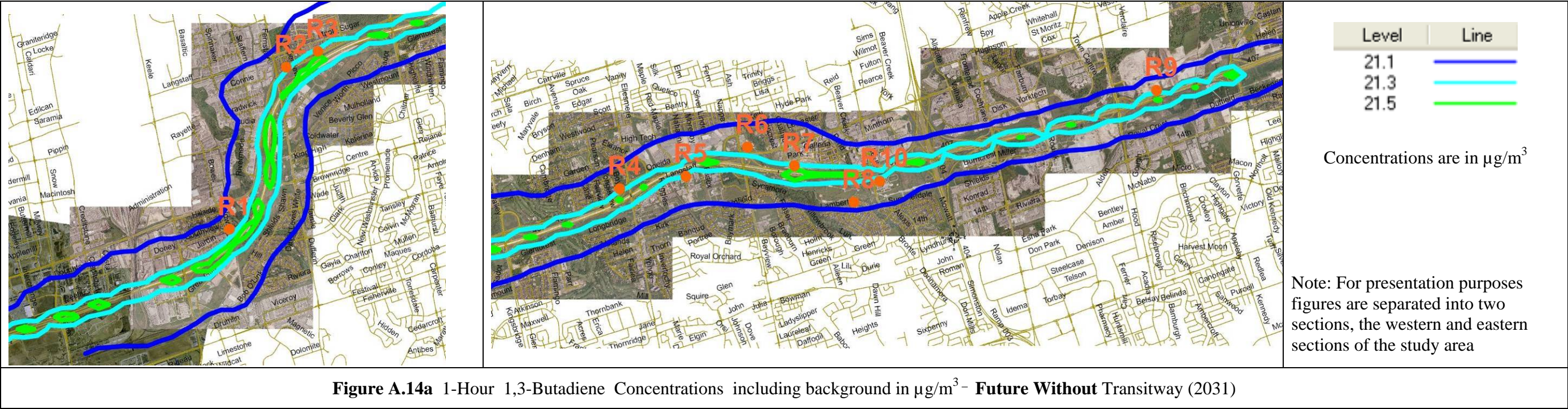
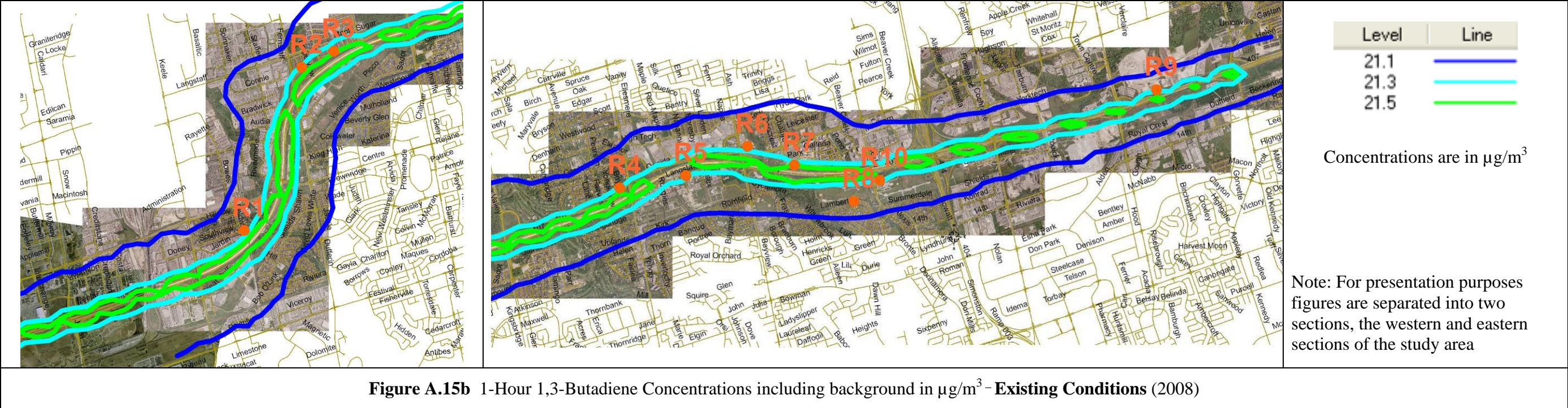
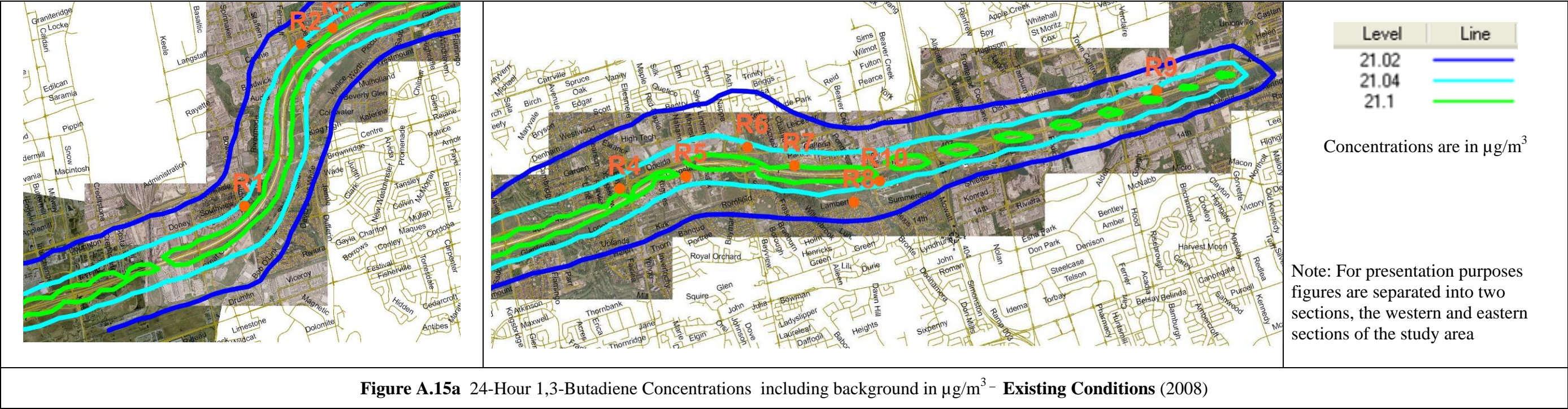


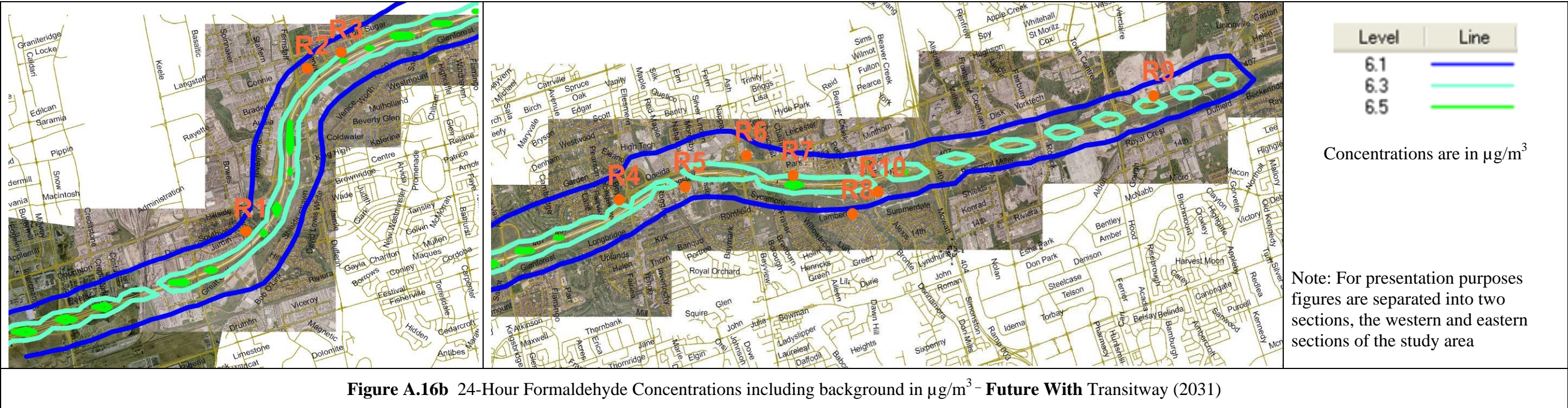
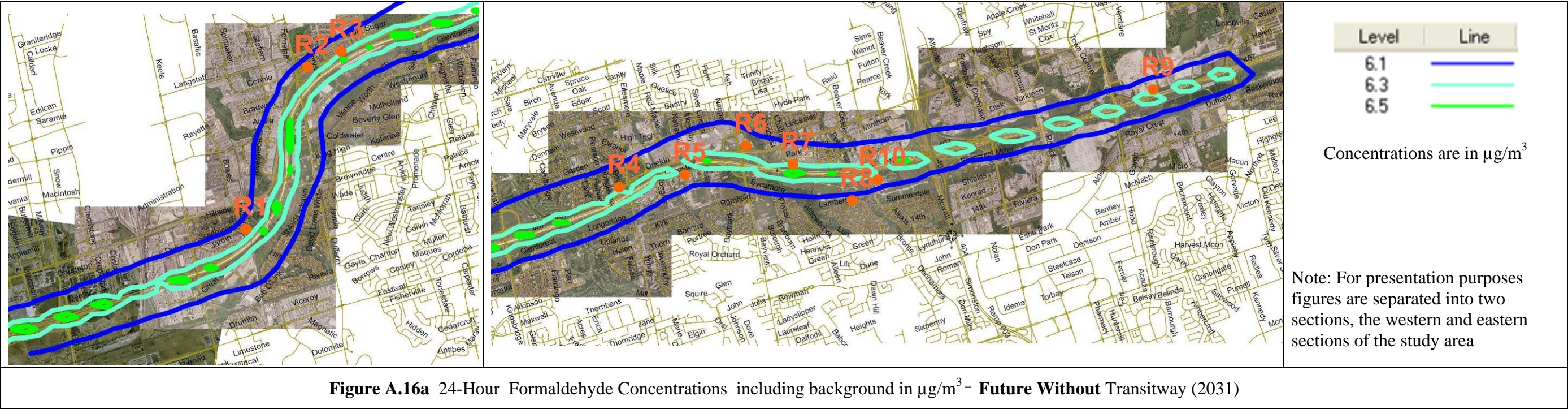
Figure A.11b 1-Hour Benzene Concentrations including background in $\mu\text{g}/\text{m}^3$ - **Future With** Transitway (2031)

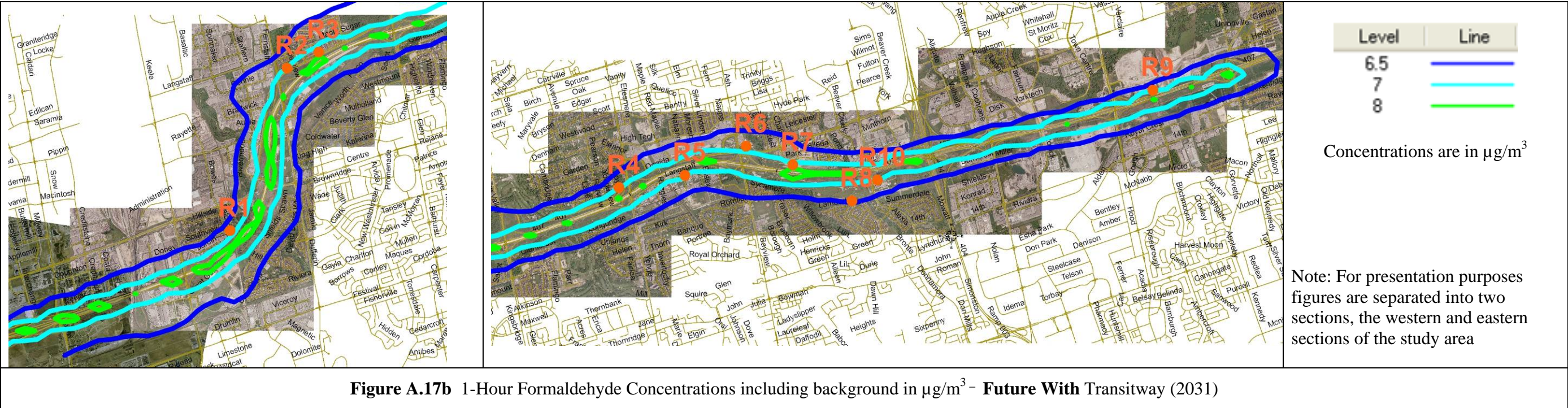
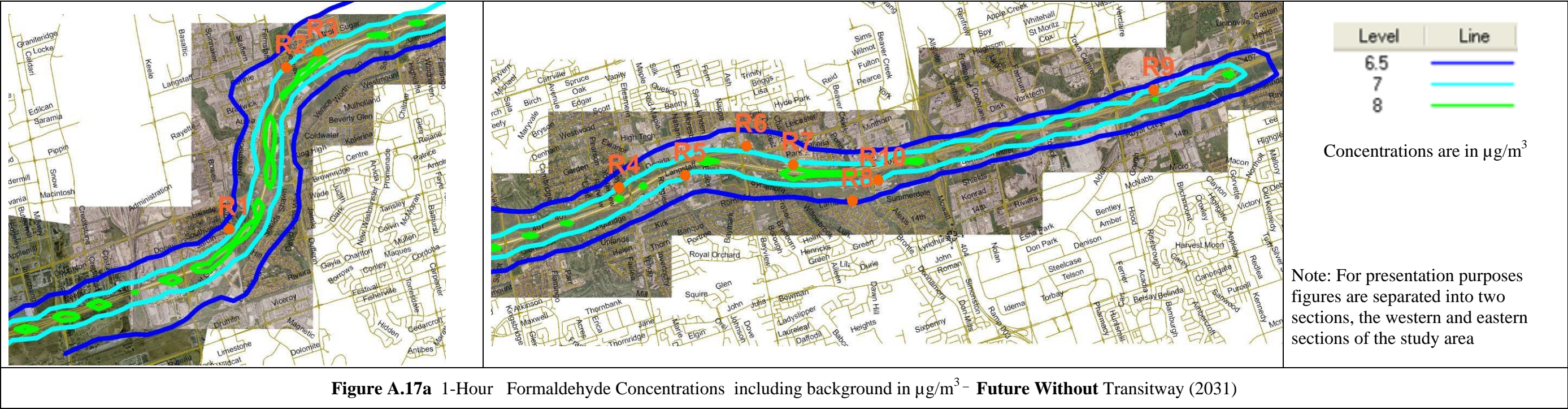












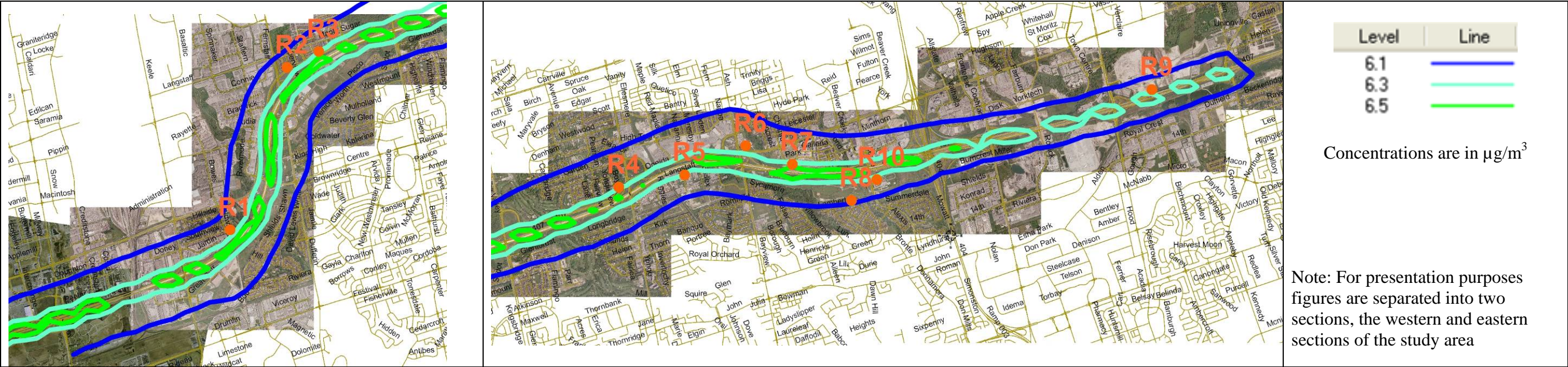


Figure A.18a 24-Hour Formaldehyde Concentrations including background in $\mu\text{g}/\text{m}^3$ - Existing Conditions (2008)

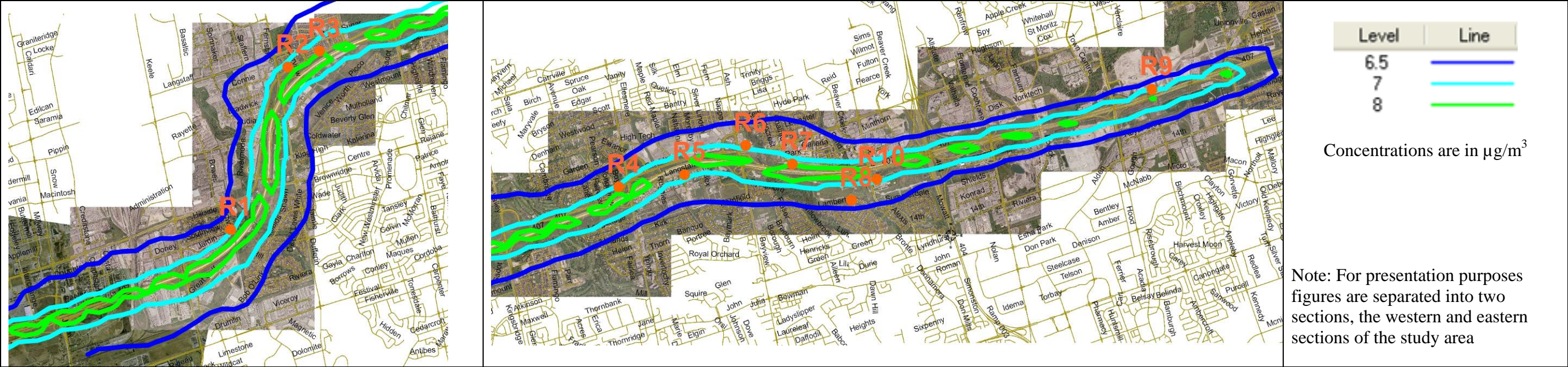
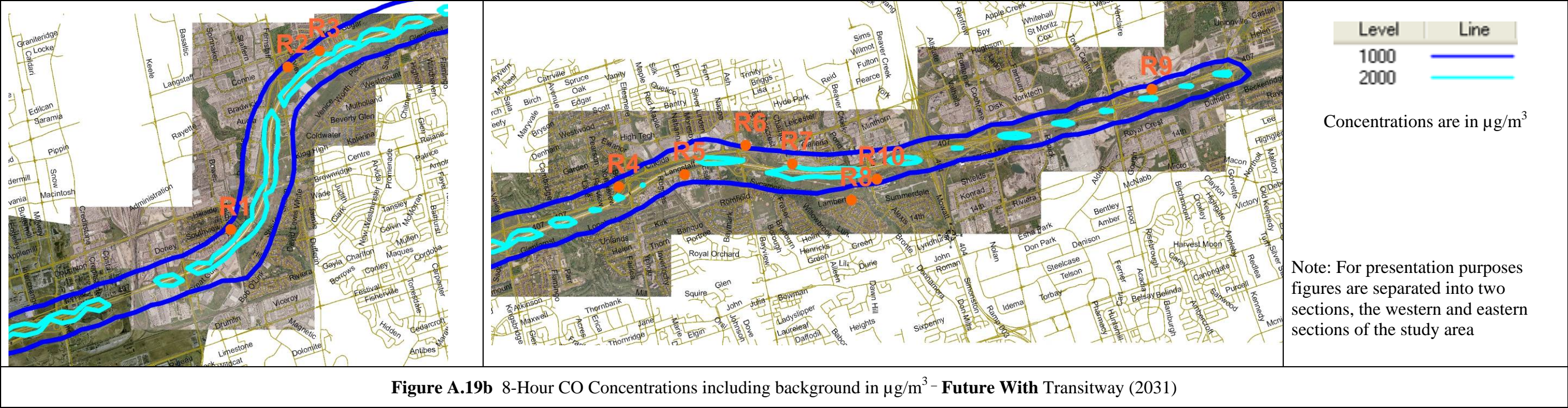
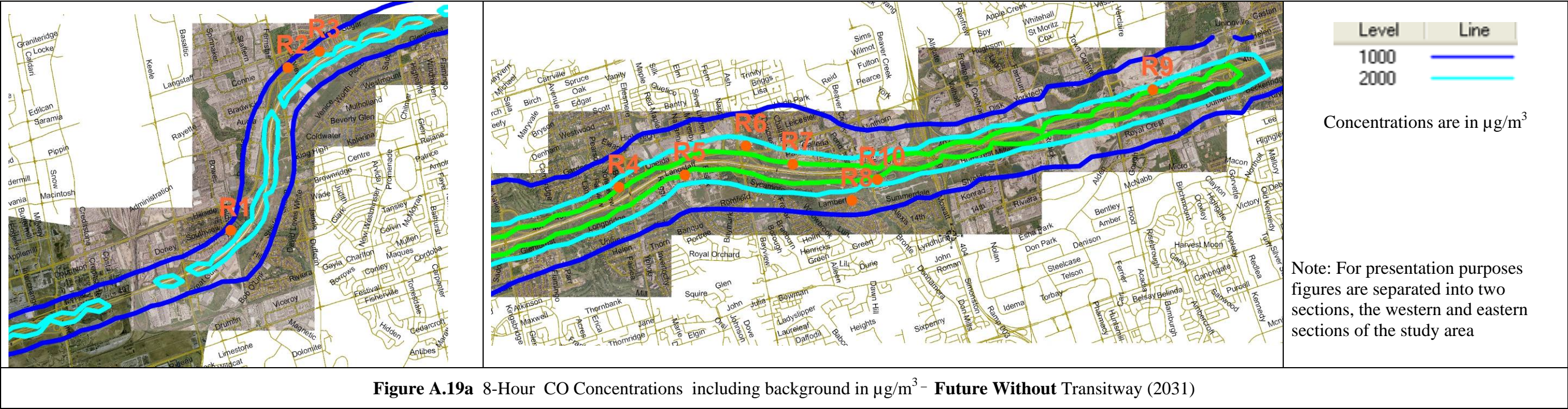
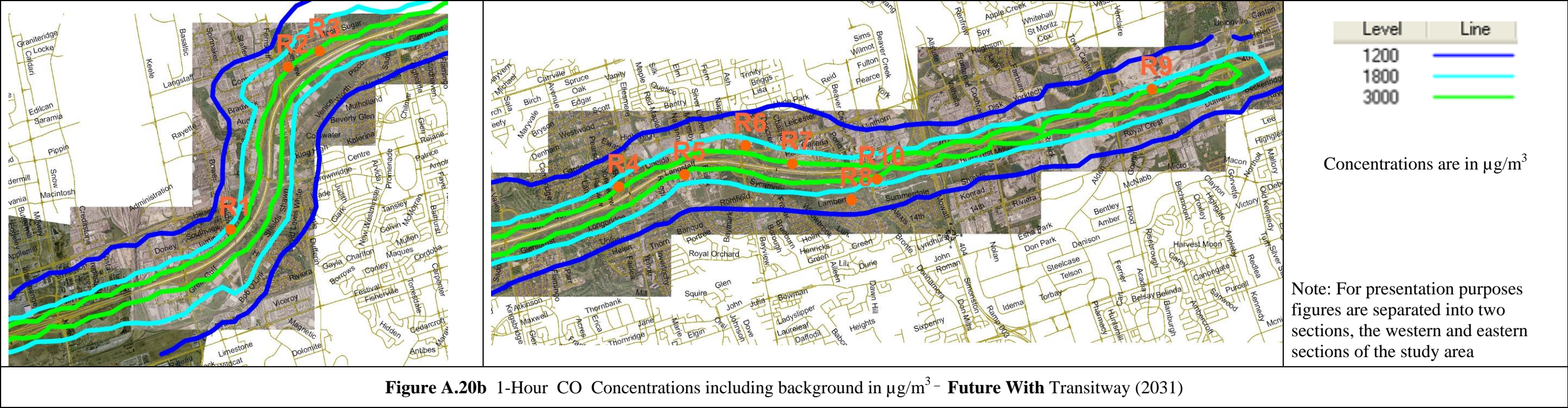
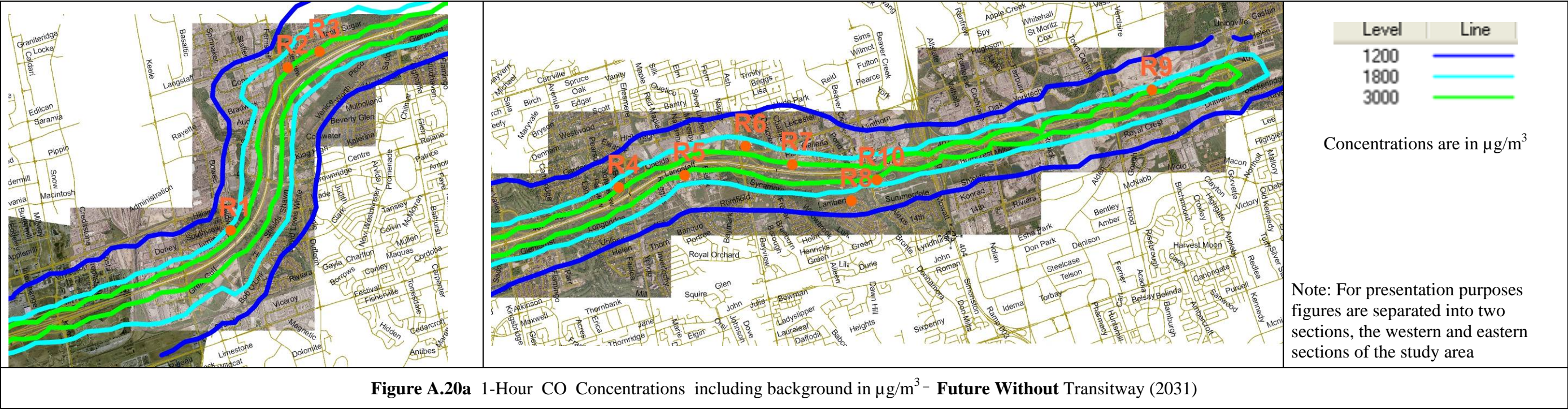
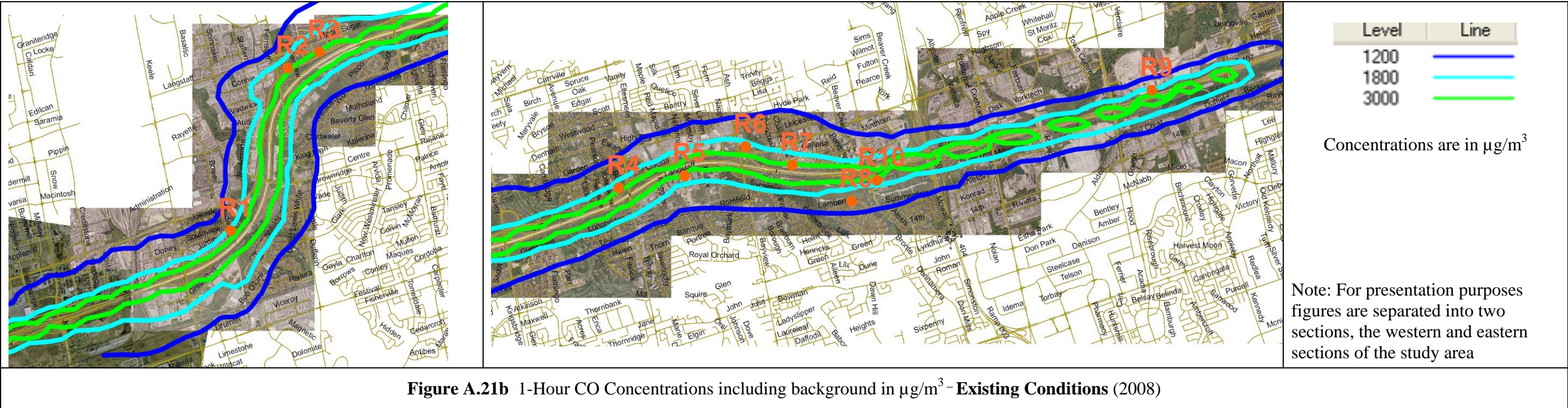
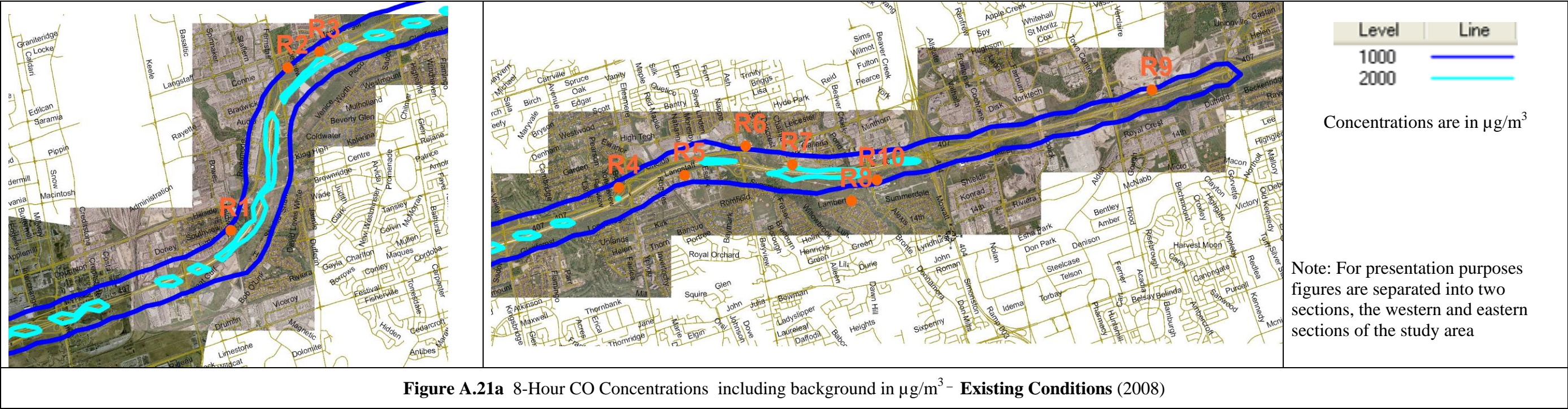
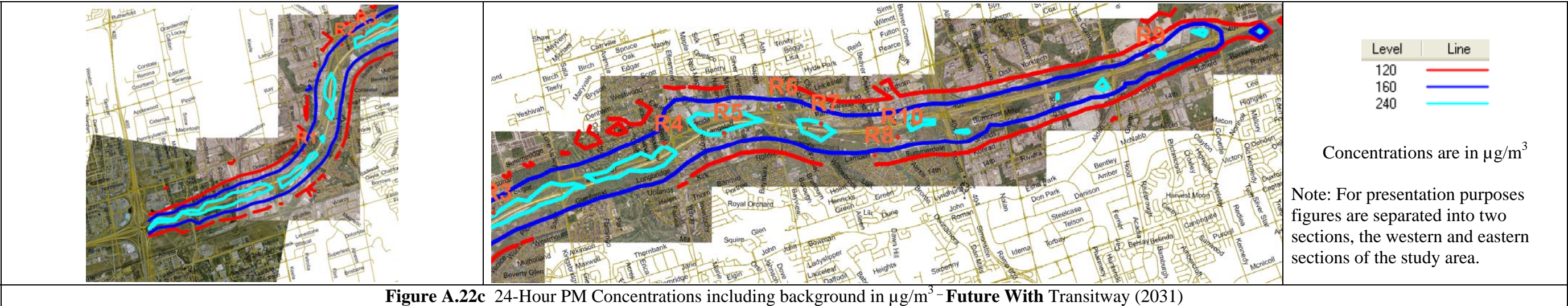
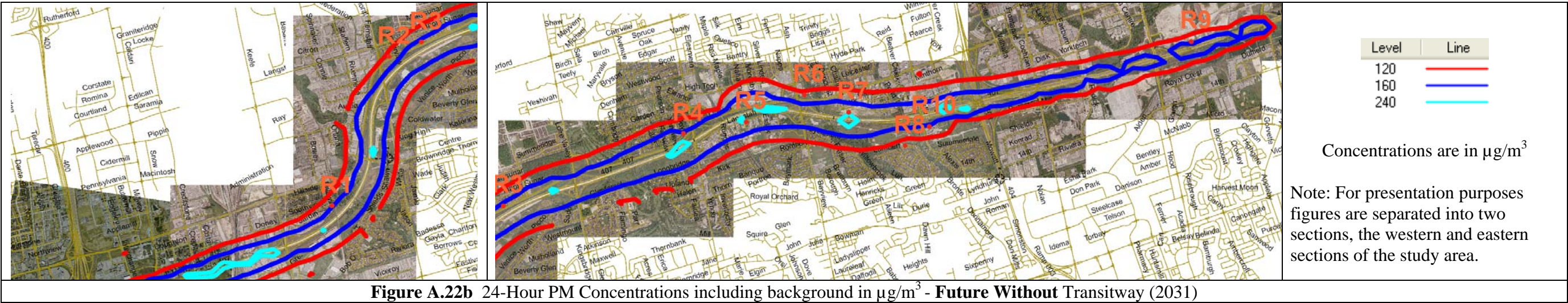
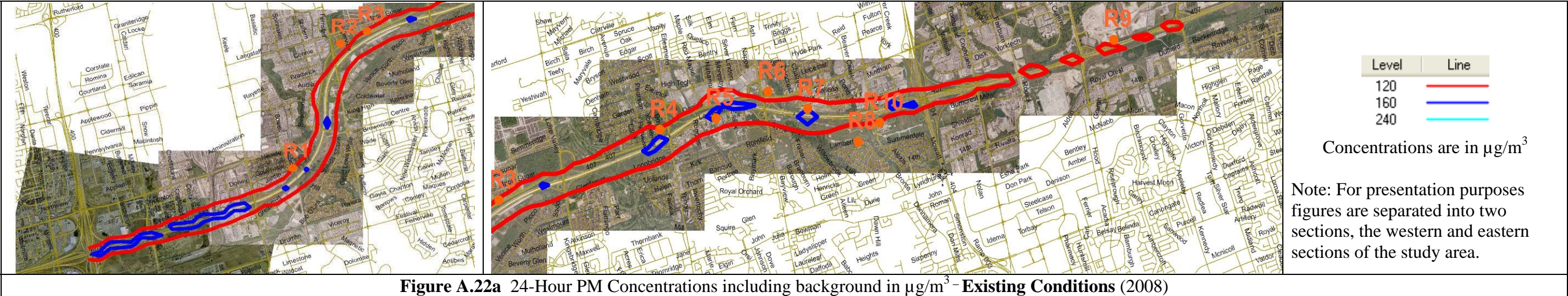


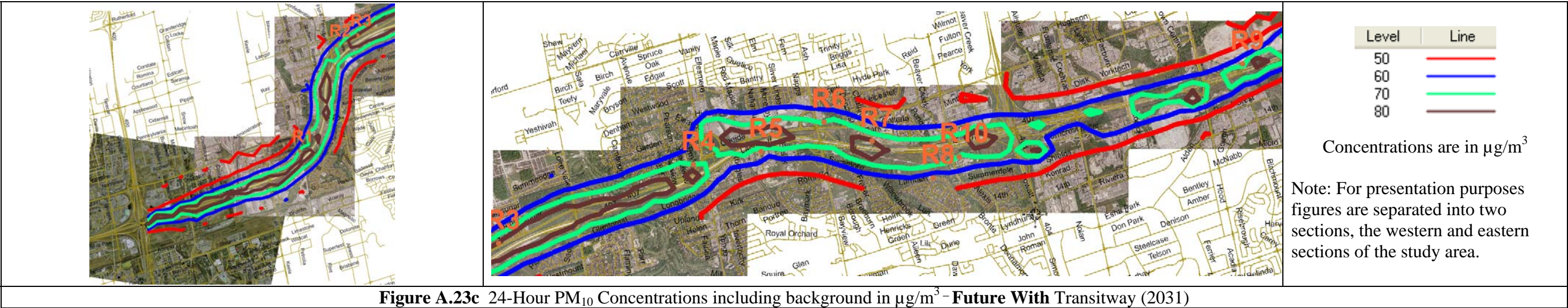
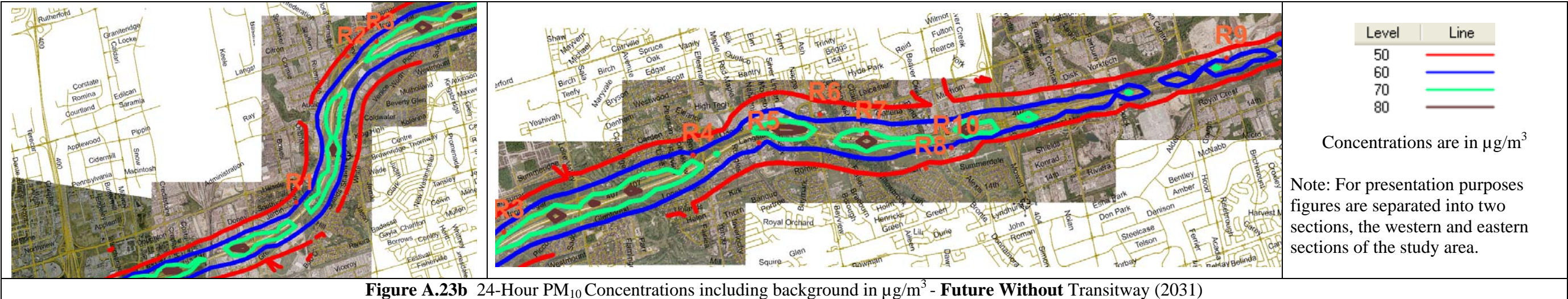
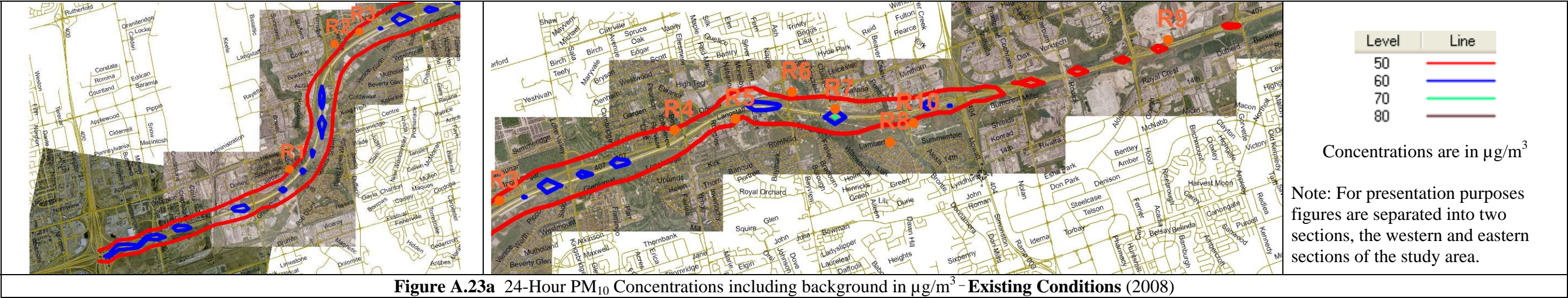
Figure A.18b 1-Hour Formaldehyde Concentrations including background in $\mu\text{g}/\text{m}^3$ - Existing Conditions (2008)

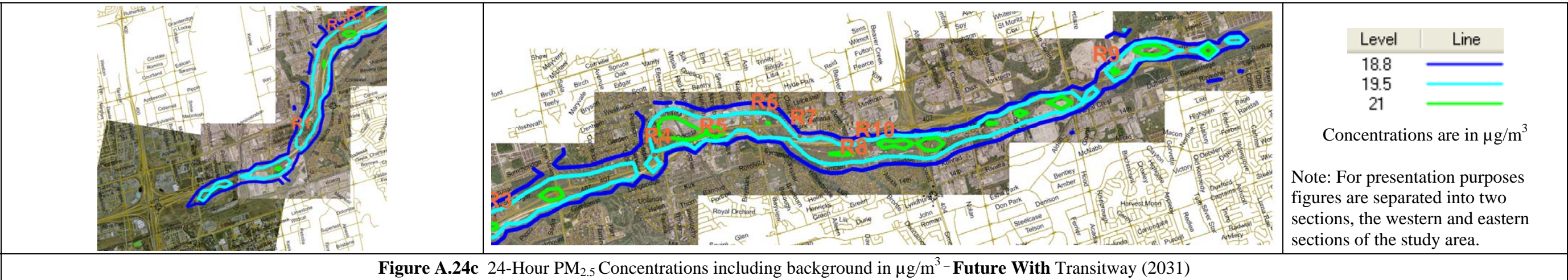
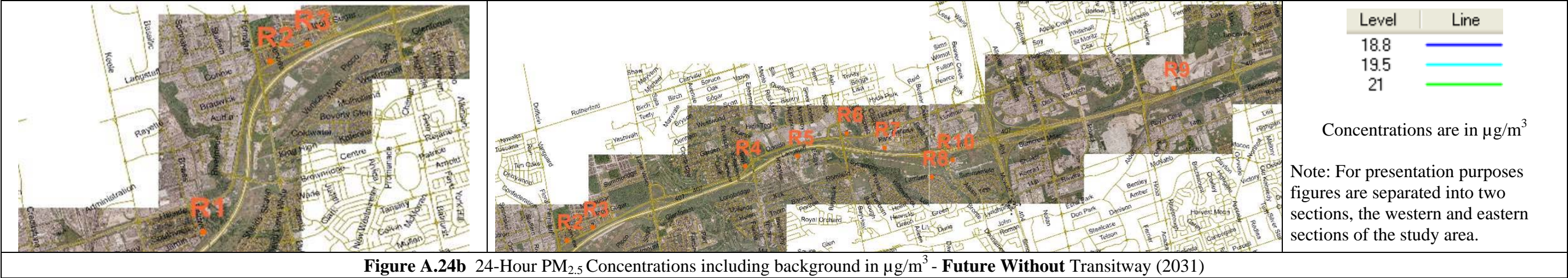
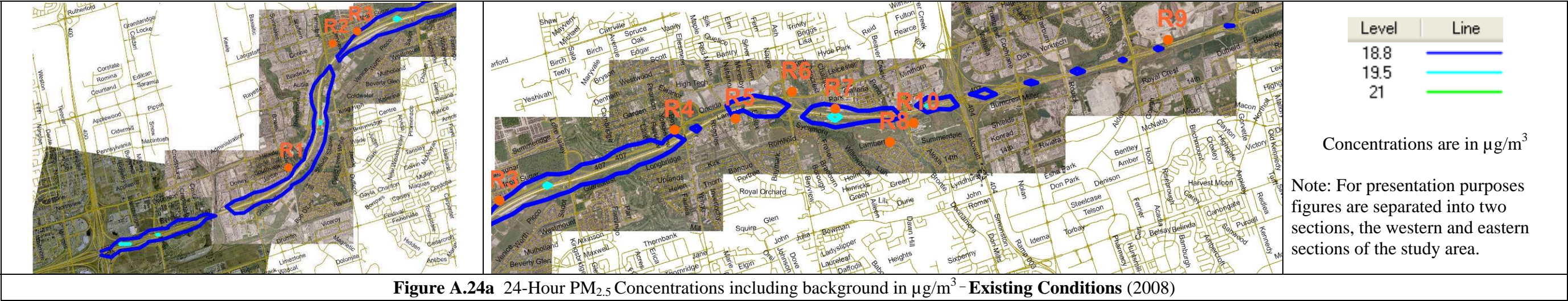












APPENDIX B

**TABULAR PRESENTATION OF
MODELLING RESULTS AT
SENSITIVE RECEPTORS**

Table B.1 a Model Predicted Maximum 24-hr PM_{2.5} Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		Canada-Wide Standard
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	18.2	17.8	-2.2%	18.7	2.5%	30
R2	18.2	17.8	-2.1%	18.9	4.0%	30
R3	18.6	18.0	-3.4%	19.0	1.8%	30
R4	18.4	17.9	-2.7%	19.0	3.4%	30
R5	18.8	17.9	-4.7%	18.4	-2.0%	30
R6	18.1	17.7	-1.9%	18.5	2.5%	30
R7	18.6	18.0	-3.5%	18.6	-0.3%	30
R8	17.9	17.7	-1.2%	18.0	1.0%	30
R9	18.2	17.9	-1.7%	19.0	4.5%	30
R10	18.2	17.8	-2.2%	20.5	12.6%	30

Note: All values include a background PM_{2.5} concentration of 17.5 µg/m³.

Table B.1 b Model Predicted Maximum 24-hr PM_{2.5} Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	Canada-Wide Standard (µg/m ³)
R1	17.8	18.7	4.8%	30
R2	17.8	18.9	6.2%	30
R3	18.0	19.0	5.3%	30
R4	17.9	19.0	6.3%	30
R5	17.9	18.4	2.8%	30
R6	17.7	18.5	4.5%	30
R7	18.0	18.6	3.4%	30
R8	17.7	18.0	2.2%	30
R9	17.9	19.0	6.3%	30
R10	17.8	20.5	15.2%	30

Note: All values include a background PM_{2.5} concentration of 17.5 µg/m³.

Table B.2 a Model Predicted Maximum 24-hr PM₁₀ Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		Canada-Wide Standard
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	45	52	14%	58	27%	50
R2	45	51	14%	60	34%	50
R3	52	63	22%	71	38%	50
R4	48	57	19%	63	31%	50
R5	54	67	24%	69	27%	50
R6	43	49	14%	55	27%	50
R7	52	64	24%	69	33%	50
R8	40	44	9%	48	17%	50
R9	43	53	21%	62	44%	50
R10	45	53	16%	73	62%	50

Note: All values include a background PM₁₀ concentration of 35.1 µg/m³.

Table B.2 b Model Predicted Maximum 24-hr PM₁₀ Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	Canada-Wide Standard (µg/m ³)
R1	52	57	11%	50
R2	51	60	18%	50
R3	63	71	13%	50
R4	57	62	10%	50
R5	67	69	2%	50
R6	49	55	12%	50
R7	64	69	8%	50
R8	44	47	8%	50
R9	53	62	18%	50
R10	53	73	40%	50

Note: All values include a background PM₁₀ concentration of 35.1 µg/m³.

Table B.3 a Model Predicted Maximum 24-hr TSP Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	97	119	22%	139	43%	120
R2	94	114	21%	146	54%	120
R3	109	143	31%	171	57%	120
R4	110	142	29%	175	59%	120
R5	134	184	37%	193	43%	120
R6	91	107	18%	124	37%	120
R7	121	161	34%	177	47%	120
R8	83	93	12%	102	23%	120
R9	95	123	30%	160	68%	120
R10	98	120	23%	181	84%	120

Note: All values include a background PM concentration of 70.2 µg/m³.

Table B.3 b Predicted Maximum 24-hr TSP Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	119	139	17%	120
R2	114	146	27%	120
R3	143	171	20%	120
R4	142	175	23%	120
R5	184	193	5%	120
R6	107	124	16%	120
R7	161	177	10%	120
R8	93	102	10%	120
R9	123	160	29%	120
R10	120	181	50%	120

Note: All values include a background TSP concentration of 70.2 µg/m³.

Table B.4 a Model Predicted Annual TSP Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	47	53	14%	60	28%	60
R2	44	49	12%	57	28%	60
R3	48	57	18%	65	35%	60
R4	49	58	18%	68	40%	60
R5	54	66	23%	70	29%	60
R6	44	48	10%	54	22%	60
R7	54	66	24%	72	34%	60
R8	42	45	7%	47	13%	60
R9	46	55	19%	65	40%	60
R10	46	53	14%	69	50%	60

Note: All values include a background PM concentration of 38.4 µg/m³.

Table B.4 b Predicted Annual TSP Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	53	60	12%	60
R2	49	57	15%	60
R3	57	65	14%	60
R4	58	68	19%	60
R5	66	70	5%	60
R6	48	54	11%	60
R7	66	72	8%	60
R8	45	47	6%	60
R9	55	65	18%	60
R10	53	69	32%	60

Note: All values include a background TSP concentration of 38.4 µg/m³.

Table B.5 a Model Predicted Maximum 24-hr NO_x Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	142	105	-26%	105	-26%	200
R2	140	104	-26%	104	-25%	200
R3	173	112	-35%	112	-35%	200
R4	154	107	-30%	107	-30%	200
R5	184	114	-38%	113	-38%	200
R6	134	102	-23%	102	-23%	200
R7	175	111	-36%	111	-36%	200
R8	119	99	-17%	99	-17%	200
R9	138	106	-23%	106	-23%	200
R10	143	104	-27%	105	-27%	200

Note: All values include a conservative background NO_x concentration of 93.4 µg/m³.

Table B.5 b Predicted Maximum 24-hr NO_x Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	105	105	0.01%	200
R2	104	104	0.14%	200
R3	112	112	0.10%	200
R4	107	107	-0.03%	200
R5	114	113	-0.24%	200
R6	102	102	0.01%	200
R7	111	111	-0.11%	200
R8	99	99	-0.09%	200
R9	106	106	0.12%	200
R10	104	105	0.28%	200

Note: All values include a conservative background NO_x concentration of 93.4 µg/m³.

Table B.6 a Model Predicted Maximum 1-hr NO_x Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	327	159	-51%	159	-51%	400
R2	432	184	-58%	184	-58%	400
R3	515	205	-60%	204	-60%	400
R4	451	187	-59%	186	-59%	400
R5	409	176	-57%	174	-57%	400
R6	386	172	-56%	171	-56%	400
R7	502	196	-61%	195	-61%	400
R8	283	147	-48%	146	-48%	400
R9	332	171	-49%	170	-49%	400
R10	411	174	-58%	174	-58%	400

Note: All values include a conservative background NO_x concentration of 108.2 µg/m³.

Table B.6 b Predicted Maximum 1-hr NO_x Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	159	159	0.00%	400
R2	184	184	0.00%	400
R3	205	204	-0.28%	400
R4	187	186	-0.50%	400
R5	176	174	-0.96%	400
R6	172	171	-0.55%	400
R7	196	195	-0.86%	400
R8	147	146	-0.38%	400
R9	171	170	-0.22%	400
R10	174	174	-0.32%	400

Note: All values include a conservative background NO_x concentration of 108.2 µg/m³.

Table B.7 a Model Predicted Maximum 8-hr CO Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	1090	1142	5%	1142	5%	15,700
R2	1090	1164	7%	1164	7%	15,700
R3	1527	1644	8%	1644	8%	15,700
R4	1217	1263	4%	1263	4%	15,700
R5	1520	1565	3%	1564	3%	15,700
R6	1041	1073	3%	1073	3%	15,700
R7	1560	1630	4%	1629	4%	15,700
R8	815	830	2%	830	2%	15,700
R9	996	1146	15%	1164	17%	15,700
R10	1186	1211	2%	1211	2%	15,700

Note: All values include a conservative background CO concentration of 483.6 µg/m³.

Table B.7 b Predicted Maximum 8-hr CO Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	1142	1142	-0.03%	15,700
R2	1164	1164	-0.01%	15,700
R3	1644	1644	0.00%	15,700
R4	1263	1263	-0.01%	15,700
R5	1565	1564	-0.01%	15,700
R6	1073	1073	-0.01%	15,700
R7	1630	1629	-0.02%	15,700
R8	830	830	-0.01%	15,700
R9	1146	1164	1.58%	15,700
R10	1211	1211	-0.02%	15,700

Note: All values include a conservative background CO concentration of 483.6 µg/m³.

Table B.8 a Model Predicted Maximum 1-hr CO Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	1959	2078	6%	2078	6%	36,200
R2	2659	2874	8%	2874	8%	36,200
R3	3193	3495	9%	3495	9%	36,200
R4	2770	2924	6%	2924	6%	36,200
R5	2491	2585	4%	2583	4%	36,200
R6	2343	2466	5%	2465	5%	36,200
R7	3068	3225	5%	3224	5%	36,200
R8	1624	1671	3%	1671	3%	36,200
R9	2054	2543	24%	2543	24%	36,200
R10	2458	2531	3%	2530	3%	36,200

Note: All values include a conservative background CO concentration of 492.4 µg/m³.

Table B.8 b Predicted Maximum 1-hr CO Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	2078	2078	0%	36,200
R2	2874	2874	0%	36,200
R3	3495	3495	0%	36,200
R4	2924	2924	0%	36,200
R5	2585	2583	-0.04%	36,200
R6	2466	2465	-0.05%	36,200
R7	3225	3224	-0.04%	36,200
R8	1671	1671	0%	36,200
R9	2543	2543	0%	36,200
R10	2531	2530	-0.05%	36,200

Note: All values include conservative background CO concentration of 492.4 µg/m³.

Table B.9 a Model Predicted Maximum 24-hr Acetaldehyde Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	4.1	4.1	0%	4.1	-0.27%	500
R2	4.1	4.1	0%	4.1	-0.20%	500
R3	4.1	4.1	0%	4.1	-0.34%	500
R4	4.1	4.1	0%	4.1	-0.34%	500
R5	4.2	4.1	-1%	4.1	-0.65%	500
R6	4.1	4.1	0%	4.1	-0.25%	500
R7	4.1	4.1	0%	4.1	-0.51%	500
R8	4.0	4.0	0%	4.0	-0.17%	500
R9	4.1	4.1	0%	4.1	0.12%	500
R10	4.1	4.1	0%	4.1	-0.24%	500

Note: All values include a conservative background Acetaldehyde concentration of 4.0 µg/m³.

Table B.9 b Predicted Maximum 24-hr Acetaldehyde Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	4.1	4.1	0.02%	500
R2	4.1	4.1	0.05%	500
R3	4.1	4.1	0.02%	500
R4	4.1	4.1	0.00%	500
R5	4.1	4.1	-0.05%	500
R6	4.1	4.1	0.02%	500
R7	4.1	4.1	-0.02%	500
R8	4.0	4.0	0.00%	500
R9	4.1	4.1	0.05%	500
R10	4.1	4.1	0.07%	500

Note: All values include a conservative background Acetaldehyde concentration of 4.0 µg/m³.

Table B.10 a Model Predicted Maximum 1-hr Acetaldehyde Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	$\mu\text{g}/\text{m}^3$	$\mu\text{g}/\text{m}^3$	% change from Existing	$\mu\text{g}/\text{m}^3$	% change from Existing	$\mu\text{g}/\text{m}^3$
R1	4.4	4.3	-1%	4.3	-1%	n/a
R2	4.6	4.5	-2%	4.5	-2%	n/a
R3	4.7	4.6	-2%	4.6	-2%	n/a
R4	4.6	4.5	-2%	4.5	-2%	n/a
R5	4.5	4.4	-2%	4.4	-2%	n/a
R6	4.5	4.4	-2%	4.4	-2%	n/a
R7	4.7	4.6	-2%	4.6	-2%	n/a
R8	4.3	4.2	-1%	4.2	-1%	n/a
R9	4.4	4.4	0%	4.4	0%	n/a
R10	4.5	4.4	-2%	4.4	-2%	n/a

Note: All values include a conservative background Acetaldehyde concentration of $4.0 \mu\text{g}/\text{m}^3$.

Table B.10 b Predicted Maximum 1-hr Acetaldehyde Comparison of Future Scenarios

Receptor	Future Without Transitway ($\mu\text{g}/\text{m}^3$)	Future With Transitway ($\mu\text{g}/\text{m}^3$)	% Change from Without Transitway	AAQC ($\mu\text{g}/\text{m}^3$)
R1	4.3	4.3	-0.1%	n/a
R2	4.5	4.5	0%	n/a
R3	4.6	4.6	-0.1%	n/a
R4	4.5	4.5	-0.2%	n/a
R5	4.4	4.4	-0.3%	n/a
R6	4.4	4.4	0%	n/a
R7	4.6	4.6	-0.2%	n/a
R8	4.2	4.2	-0.1%	n/a
R9	4.4	4.4	0%	n/a
R10	4.4	4.4	0%	n/a

Note: All values include a conservative background Acetaldehyde concentration of $4.0 \mu\text{g}/\text{m}^3$.

Table B.11 a Model Predicted Maximum 24-hr Acrolein Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	0.71	0.71	0%	0.71	0%	0.4
R2	0.71	0.71	0%	0.71	0%	0.4
R3	0.72	0.71	0%	0.71	0%	0.4
R4	0.71	0.71	0%	0.71	0%	0.4
R5	0.71	0.72	0%	0.71	0%	0.4
R6	0.71	0.71	0%	0.71	0%	0.4
R7	0.72	0.71	0%	0.71	0%	0.4
R8	0.71	0.70	0%	0.70	0%	0.4
R9	0.71	0.71	0%	0.71	0%	0.4
R10	0.71	0.71	0%	0.71	0%	0.4

Note: All values include a conservative background acrolein concentration of 0.7 µg/m³.

Table B.11 b Predicted Maximum 24-hr Acrolein Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	0.71	0.71	0%	0.4
R2	0.71	0.71	0%	0.4
R3	0.71	0.71	0%	0.4
R4	0.71	0.71	0%	0.4
R5	0.72	0.71	0%	0.4
R6	0.71	0.71	0%	0.4
R7	0.71	0.71	0%	0.4
R8	0.70	0.70	0%	0.4
R9	0.71	0.71	0%	0.4
R10	0.71	0.71	0%	0.4

Note: All values include a conservative background acrolein concentration of 0.7 µg/m³.

Table B.12 a Model Predicted Maximum 1-hr Acrolein Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	$\mu\text{g}/\text{m}^3$	$\mu\text{g}/\text{m}^3$	% change from Existing	$\mu\text{g}/\text{m}^3$	% change from Existing	$\mu\text{g}/\text{m}^3$
R1	0.75	0.74	-1%	0.74	-1%	4.5
R2	0.76	0.76	-1%	0.76	-1%	4.5
R3	0.78	0.77	-2%	0.77	-2%	4.5
R4	0.77	0.76	-2%	0.76	-2%	4.5
R5	0.76	0.75	-1%	0.75	-1%	4.5
R6	0.76	0.75	-1%	0.75	-1%	4.5
R7	0.78	0.77	-2%	0.76	-2%	4.5
R8	0.74	0.73	-1%	0.73	-1%	4.5
R9	0.74	0.75	1%	0.75	1%	4.5
R10	0.76	0.75	-2%	0.75	-2%	4.5

Note: All values include a conservative background acrolein concentration of $0.7 \mu\text{g}/\text{m}^3$.

Table B.12 b Predicted Maximum 1-hr Acrolein Comparison of Future Scenarios

Receptor	Future Without Transitway ($\mu\text{g}/\text{m}^3$)	Future With Transitway ($\mu\text{g}/\text{m}^3$)	% Change from Without Transitway	AAQC ($\mu\text{g}/\text{m}^3$)
R1	0.74	0.74	0%	4.5
R2	0.76	0.76	-0.1%	4.5
R3	0.77	0.77	0%	4.5
R4	0.76	0.76	-0.3%	4.5
R5	0.75	0.75	-0.1%	4.5
R6	0.75	0.75	0%	4.5
R7	0.77	0.76	-0.3%	4.5
R8	0.73	0.73	-0.1%	4.5
R9	0.75	0.75	0%	4.5
R10	0.75	0.75	0%	4.5

Note: All values include a conservative background acrolein concentration of $0.7 \mu\text{g}/\text{m}^3$.

Table B.13 a Model Predicted Maximum 24-hr Benzene Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	$\mu\text{g}/\text{m}^3$	$\mu\text{g}/\text{m}^3$	% change from Existing	$\mu\text{g}/\text{m}^3$	% change from Existing	$\mu\text{g}/\text{m}^3$
R1	4.8	4.7	-2%	4.7	-2%	2.3
R2	4.8	4.7	-1%	4.7	-1%	2.3
R3	5.1	5.0	-2%	5.0	-2%	2.3
R4	4.9	4.8	-2%	4.8	-2%	2.3
R5	5.2	5.0	-3%	5.0	-3%	2.3
R6	4.7	4.7	-1%	4.7	-1%	2.3
R7	5.1	5.0	-3%	5.0	-3%	2.3
R8	4.6	4.6	-1%	4.6	-1%	2.3
R9	4.8	4.8	0%	4.8	0%	2.3
R10	4.8	4.7	-2%	4.7	-2%	2.3

Note: All values include a conservative background Benzene concentration of $4.4 \mu\text{g}/\text{m}^3$.

Table B.13 b Predicted Maximum 24-hr Benzene Comparison of Future Scenarios

Receptor	Future Without Transitway ($\mu\text{g}/\text{m}^3$)	Future With Transitway ($\mu\text{g}/\text{m}^3$)	% Change from Without Transitway	AAQC ($\mu\text{g}/\text{m}^3$)
R1	4.7	4.7	0.0%	2.3
R2	4.7	4.7	0.0%	2.3
R3	5.0	5.0	0.0%	2.3
R4	4.8	4.8	0.0%	2.3
R5	5.0	5.0	0.0%	2.3
R6	4.7	4.7	0.0%	2.3
R7	5.0	5.0	0.0%	2.3
R8	4.6	4.6	0.0%	2.3
R9	4.8	4.8	0.0%	2.3
R10	4.7	4.7	0.0%	2.3

Note: All values include a conservative background Benzene concentration of $4.4 \mu\text{g}/\text{m}^3$.

Table B.14 a Model Predicted Maximum 1-hr Benzene Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	6.3	6.0	-5%	6.0	-5%	n/a
R2	7.2	6.7	-6%	6.7	-7%	n/a
R3	7.9	7.3	-7%	7.3	-7%	n/a
R4	7.3	6.8	-7%	6.8	-7%	n/a
R5	7.0	6.5	-7%	6.5	-8%	n/a
R6	6.8	6.3	-7%	6.3	-7%	n/a
R7	7.7	7.1	-8%	7.1	-8%	n/a
R8	5.9	5.6	-5%	5.6	-5%	n/a
R9	6.4	6.4	0%	6.4	0%	n/a
R10	6.9	6.4	-8%	6.4	-8%	n/a

Note: All values include a conservative background Benzene concentration of 4.4 µg/m³.

Table B.14 b Predicted Maximum 1-hr Benzene Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	6.0	6.0	0%	n/a
R2	6.7	6.7	0%	n/a
R3	7.3	7.3	0%	n/a
R4	6.8	6.8	0%	n/a
R5	6.5	6.5	0%	n/a
R6	6.3	6.3	0%	n/a
R7	7.1	7.1	0%	n/a
R8	5.6	5.6	0%	n/a
R9	6.4	6.4	0%	n/a
R10	6.4	6.4	0%	n/a

Note: All values include a conservative background Benzene concentration of 4.4 µg/m³.

Table B.15 a Model Predicted Maximum 24-hr 1, 3-Butadiene Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	21.05	21.04	-0.1%	21.04	-0.06%	10.0
R2	21.05	21.04	-0.1%	21.04	-0.05%	10.0
R3	21.09	21.07	-0.1%	21.07	-0.08%	10.0
R4	21.06	21.05	-0.1%	21.05	-0.07%	10.0
R5	21.10	21.07	-0.1%	21.07	-0.12%	10.0
R6	21.04	21.03	-0.1%	21.03	-0.05%	10.0
R7	21.09	21.07	-0.1%	21.07	-0.09%	10.0
R8	21.03	21.02	0.0%	21.02	-0.03%	10.0
R9	21.05	21.05	0.0%	21.05	-0.01%	10.0
R10	21.05	21.04	-0.1%	21.04	-0.06%	10.0

Note: All values include a conservative background 1, 3 Butadiene concentration of 21.0 µg/m³.

Table B.15 b Predicted Maximum 24-hr 1, 3-Butadiene Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	21.04	21.04	0%	10.0
R2	21.04	21.04	0.01%	10.0
R3	21.07	21.07	0%	10.0
R4	21.05	21.05	0%	10.0
R5	21.07	21.07	0%	10.0
R6	21.03	21.03	0%	10.0
R7	21.07	21.07	0%	10.0
R8	21.02	21.02	0%	10.0
R9	21.05	21.05	0%	10.0
R10	21.04	21.04	0.01%	10.0

Note: All values include a conservative background 1, 3 Butadiene concentration of 21.0 µg/m³.

Table B.16 a Model Predicted Maximum 1-hr 1, 3-Butadiene Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	21.2	21.2	-0.2%	21.2	-0.3%	n/a
R2	21.3	21.3	-0.4%	21.3	-0.4%	n/a
R3	21.4	21.3	-0.4%	21.3	-0.4%	n/a
R4	21.4	21.3	-0.4%	21.3	-0.4%	n/a
R5	21.3	21.2	-0.4%	21.2	-0.4%	n/a
R6	21.3	21.2	-0.3%	21.2	-0.3%	n/a
R7	21.4	21.3	-0.5%	21.3	-0.5%	n/a
R8	21.2	21.1	-0.2%	21.1	-0.2%	n/a
R9	21.2	21.2	-0.1%	21.2	-0.1%	n/a
R10	21.3	21.2	-0.4%	21.2	-0.4%	n/a

Note: All values include a conservative background 1, 3 Butadiene concentration of 21.0 µg/m³.

Table B.16 b Predicted Maximum 1-hr 1, 3-Butadiene Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway (µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	21.2	21.2	-0.005%	n/a
R2	21.3	21.3	0.0%	n/a
R3	21.3	21.3	-0.005%	n/a
R4	21.3	21.3	-0.009%	n/a
R5	21.2	21.2	-0.014%	n/a
R6	21.2	21.2	-0.005%	n/a
R7	21.3	21.3	-0.009%	n/a
R8	21.1	21.1	-0.005%	n/a
R9	21.2	21.2	-0.005%	n/a
R10	21.2	21.2	-0.005%	n/a

Note: All values include a conservative background 1, 3 Butadiene concentration of 21.0 µg/m³.

Table B.17 a Model Predicted Maximum 24-hr Formaldehyde Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	6.2	6.2	-0.6%	6.2	-0.5%	65
R2	6.2	6.2	-0.5%	6.2	-0.4%	65
R3	6.3	6.3	-0.8%	6.3	-0.7%	65
R4	6.2	6.2	-0.7%	6.2	-0.7%	65
R5	6.4	6.3	-1.1%	6.3	-1.2%	65
R6	6.2	6.1	-0.5%	6.1	-0.5%	65
R7	6.3	6.3	-0.9%	6.3	-1.0%	65
R8	6.1	6.1	-0.3%	6.1	-0.3%	65
R9	6.2	6.2	0%	6.2	0%	65
R10	6.2	6.2	-0.6%	6.2	-0.5%	65

Note: All values include a conservative background Formaldehyde concentration of 6.0 µg/m³.

Table B.17 b Predicted Maximum 24-hr Formaldehyde Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway(µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	6.2	6.2	0.03%	65
R2	6.2	6.2	0.08%	65
R3	6.3	6.3	0.05%	65
R4	6.2	6.2	0.02%	65
R5	6.3	6.3	-0.08%	65
R6	6.1	6.1	0.02%	65
R7	6.3	6.3	-0.06%	65
R8	6.1	6.1	0%	65
R9	6.2	6.2	0.08%	65
R10	6.2	6.2	0.16%	65

Note: All values include a conservative background Formaldehyde concentration of 6.0 µg/m³.

Table B.18 a Model Predicted Maximum 1-hr Formaldehyde Concentrations

Receptor	Existing Conditions	Future Without Transitway		Future With Transitway		AAQC
	µg/m ³	µg/m ³	% change from Existing	µg/m ³	% change from Existing	µg/m ³
R1	6.9	6.7	-2.3%	6.7	-2.3%	n/a
R2	7.3	7.1	-3.0%	7.1	-3.1%	n/a
R3	7.7	7.4	-3.4%	7.4	-3.5%	n/a
R4	7.4	7.1	-3.4%	7.1	-3.6%	n/a
R5	7.2	7.0	-3.3%	7.0	-3.8%	n/a
R6	7.1	6.9	-2.9%	6.9	-3.0%	n/a
R7	7.6	7.3	-3.9%	7.3	-4.3%	n/a
R8	6.7	6.6	-2.1%	6.6	-2.2%	n/a
R9	6.9	6.9	-0.3%	6.9	-0.4%	n/a
R10	7.2	7.0	-3.4%	7.0	-3.4%	n/a

Note: All values include a conservative background Formaldehyde concentration of 6.0 µg/m³.

Table B.18 b Predicted Maximum 24-hr Formaldehyde Comparison of Future Scenarios

Receptor	Future Without Transitway (µg/m ³)	Future With Transitway(µg/m ³)	% Change from Without Transitway	AAQC (µg/m ³)
R1	6.7	6.7	-0.07%	n/a
R2	7.1	7.1	-0.04%	n/a
R3	7.4	7.4	-0.05%	n/a
R4	7.1	7.1	-0.20%	n/a
R5	7.0	7.0	-0.49%	n/a
R6	6.9	6.9	-0.07%	n/a
R7	7.3	7.3	-0.41%	n/a
R8	6.6	6.6	-0.11%	n/a
R9	6.9	6.9	-0.03%	n/a
R10	7.0	7.0	0.01%	n/a

Note: All values include a conservative background Formaldehyde concentration of 6.0 µg/m³.

APPENDIX C

CAL3QHCR SAMPLE MODEL INPUT (EXISTING CONDITIONS PM₁₀)

Air Quality Impact Assessment for the 407 Transitway (Highway 400 to Kennedy Road)

'407 Transitway EA Base Case - PM10' 60.0 108.0 0.3 0.3 2091 1.0 0 01 01 93 12 31 93 61587 93 72528 93 0 0 'U' R1' 621620.1 4850635.0 1.5 R2' 622555.0 4853280.2 1.5 R3' 623075.1 4853538.5 1.5 R4' 626149.4 4854776.7 1.5 R5' 627212.2 4854978.1 1.5 R6' 628204.1 4855443.8 1.5 R7' 628959.9 4855146.5 1.5 R8' 629922.7 4854562.6 1.5 R9' 634796.4 4856357.3 1.5 R10' 630335.1 4854901.2 1.5 R11' 617752.7 4848792.2 1.5 R12' 617848.2 4848821.1 1.5 ... R2091' 625846.0 4855004.0 1.5 2 'P' 1 1 1 1 1 2 " 70 1 1 'FF1' 'AG' 617646.5 4848796.9 617902.4 4848876.5 1.0 24.4 2 1 'FF2' 'AG' 617902.4 4848876.5 618818.7 4849161.6 1.0 20.7 3 1 'FF3' 'AG' 618818.7 4849161.6 619626.0 4849445.8 1.0 20.7 4 1 'FF4' 'BR' 619626.0 4849445.8 620399.2 4849717.5 11.0 24.4 5 1 'FF5' 'AG' 620399.2 4849717.5 620888.0 4849894.0 1.0 20.7 6 1 'FF6' 'AG' 620888.0 4849894.0 621317.1 4850096.1 1.0 20.7 7 1 'FF7' 'AG' 621317.1 4850096.1 621718.7 4850407.2 1.0 24.4 8 1 'FF8' 'AG' 621718.7 4850407.2 622030.1 4850807.1 1.0 20.7 9 1 'FF9' 'AG' 622030.1 4850807.1 622230.0 4851323.8 1.0 20.7 10 1 'FF10' 'AG' 622230.0 4851323.8 622279.9 4851856.6 1.0 20.7 11 1 'FF11' 'AG' 622279.9 4851856.6 622300.5 4852291.4 1.0 20.7 12 1 'FF12' 'AG' 622300.5 4852291.4 622475.8 4852748.1 1.0 20.7 13 1	'FF13' 'AG' 622475.8 4852748.1 622752.3 4853081.5 1.0 24.4 14 1 'FF14' 'AG' 622752.3 4853081.5 623002.1 4853279.5 1.0 24.4 15 1 'FF15' 'AG' 623002.1 4853279.5 623414.3 4853529.1 1.0 24.4 16 1 'FF16' 'AG' 623414.3 4853529.1 623689.5 4853654.5 1.0 24.4 17 1 'FF17' 'AG' 623689.5 4853654.5 624316.7 4853859.2 1.0 20.7 18 1 'FF18' 'AG' 624316.7 4853859.2 624943.3 4854067.5 1.0 24.4 19 1 'FF19' 'AG' 624943.3 4854067.5 625718.4 4854349.2 1.0 24.4 20 1 'FF20' 'BR' 625718.4 4854349.2 626335.2 4854644.6 9.0 20.7 21 1 'FF21' 'BR' 626335.2 4854644.6 626838.6 4854950.2 9.0 24.4 22 1 'FF22' 'BR' 626838.6 4854950.2 627427.7 4855142.9 9.0 24.4 23 1 'FF23' 'AG' 627427.7 4855142.9 628144.8 4855113.0 1.0 20.7 24 1 'FF24' 'AG' 628144.8 4855113.0 628702.7 4855029.7 1.0 24.4 25 1 'FF25' 'AG' 628702.7 4855029.7 629414.0 4854971.9 1.0 24.4 26 1 'FF26' 'AG' 629414.0 4854971.9 630204.9 4855042.8 1.0 20.7 27 1 'FF27' 'AG' 630204.9 4855042.8 631178.2 4855268.4 1.0 20.7 28 1 'FF28' 'AG' 631178.2 4855268.4 631542.1 4855354.4 1.0 20.7 29 1 'FF29' 'AG' 631542.1 4855354.4 632179.0 4855508.8 1.0 17.0 30 1 'FF30' 'AG' 632179.0 4855508.8 633062.3 4855698.6 1.0 20.7 31 1 'FF31' 'AG' 633062.3 4855698.6 633622.9 4855841.6 1.0 20.7 32 1 'FF32' 'AG' 633622.9 4855841.6 634192.7 4856007.0 1.0 20.7 33 1	'FF33' 'AG' 634192.7 4856007.0 635028.3 4856273.2 1.0 20.7 34 1 'FF34' 'AG' 635028.3 4856273.2 635455.3 4856419.9 1.0 20.7 35 1 'FF35' 'AG' 635455.3 4856419.9 636026.6 4856619.7 1.0 17.0 36 1 'FF36' 'AG' 636026.6 4856619.7 635445.0 4856457.6 1.0 20.7 37 1 'FF37' 'AG' 635445.0 4856457.6 635016.6 4856311.4 1.0 20.7 38 1 'FF38' 'AG' 635016.6 4856311.4 634186.9 4856044.6 1.0 20.7 39 1 'FF39' 'AG' 634186.9 4856044.6 633612.5 4855881.3 1.0 20.7 40 1 'FF40' 'AG' 633612.5 4855881.3 633055.6 4855739.6 1.0 17.0 41 1 'FF41' 'AG' 633055.6 4855739.6 632171.5 4855547.3 1.0 20.7 42 1 'FF42' 'AG' 632171.5 4855547.3 631534.6 4855393.4 1.0 17.0 43 1 'FF43' 'AG' 631534.6 4855393.4 631170.8 4855305.4 1.0 20.7 44 1 'FF44' 'AG' 631170.8 4855305.4 630196.8 4855081.8 1.0 20.7 45 1 'FF45' 'AG' 630196.8 4855081.8 629414.3 4855017.6 1.0 24.4 46 1 'FF46' 'AG' 629414.3 4855017.6 628707.8 4855072.2 1.0 24.4 47 1 'FF47' 'AG' 628707.8 4855072.2 628135.3 4855156.7 1.0 20.7 48 1 'FF48' 'AG' 628135.3 4855156.7 627421.1 4855185.1 1.0 24.4 49 1 'FF49' 'BR' 627421.1 4855185.1 626821.7 4854987.6 9.0 24.4 50 1 'FF50' 'BR' 626821.7 4854987.6 626327.6 4854691.1 9.0 20.7 51 1 'FF51' 'BR' 626327.6 4854691.1 625708.1 4854389.6 9.0 24.4 52 1 'FF52' 'AG' 625708.1 4854389.6 624928.5 4854109.2 1.0 24.4 53 1	'FF53' 'AG' 624928.5 4854109.2 624310.1 4853902.9 1.0 20.7 54 1 'FF54' 'AG' 624310.1 4853902.9 623676.1 4853697.0 1.0 24.4 55 1 'FF55' 'AG' 623676.1 4853697.0 623397.8 4853569.1 1.0 24.4 56 1 'FF56' 'AG' 623397.8 4853569.1 622979.3 4853315.4 1.0 24.4 57 1 'FF57' 'AG' 622979.3 4853315.4 622729.1 4853114.2 1.0 24.4 58 1 'FF58' 'AG' 622729.1 4853114.2 622464.7 4852806.0 1.0 24.4 59 1 'FF59' 'AG' 622464.7 4852806.0 622259.5 4852297.8 1.0 24.7 60 1 'FF60' 'AG' 622259.5 4852297.8 622239.5 4851857.3 1.0 20.7 61 1 'FF61' 'AG' 622239.5 4851857.3 622194.4 4851332.9 1.0 20.7 62 1 'FF62' 'AG' 622194.4 4851332.9 622000.3 4850831.4 1.0 20.7 63 1 'FF63' 'AG' 622000.3 4850831.4 621710.2 4850455.5 1.0 20.7 64 1 'FF64' 'AG' 621710.2 4850455.5 621300.6 4850132.1 1.0 24.4 65 1 'FF65' 'AG' 621300.6 4850132.1 620880.8 4849933.2 1.0 20.7 66 1 'FF66' 'AG' 620880.8 4849933.2 620386.1 4849756.9 1.0 24.4 67 1 'FF67' 'BR' 620386.1 4849756.9 619614.7 4849481.8 11.0 24.4 68 1 'FF68' 'AG' 619614.7 4849481.8 618806.4 4849194.9 1.0 20.7 69 1 'FF69' 'AG' 618806.4 4849194.9 617894.1 4848911.1 1.0 20.7 70 1 'FF70' 'AG' 617894.1 4848911.1 617641.4 4848831.9 1.0 24.4 1 0.0 1 175 0.622 2 175 0.622 3 178 0.602 4 178 0.602 5 178 0.602 6 175 0.558	7 175 0.558 8 175 0.558 9 175 0.558 10 175 0.558 11 175 0.558 12 175 0.558 13 171 0.57 14 171 0.57 15 171 0.57 16 171 0.57 17 171 0.57 18 174 0.572 19 174 0.572 20 174 0.572 21 168 0.565 22 168 0.565 23 168 0.565 24 164 0.587 25 164 0.587 26 164 0.587 27 145 0.604 28 125 0.549 29 125 0.549 30 121 0.535 31 121 0.535 32 121 0.535 33 120 0.536 34 120 0.536 35 120 0.536 36 111 0.532 37 111 0.532 38 111 0.532 39 112 0.537 40 112 0.537 41 112 0.537 42 116 0.553 43 116 0.553 44 140 0.618 45 157 0.594 46 157 0.594 47 157 0.594 48 159 0.577 49 159 0.577 50 159 0.577 51 165 0.583 52 165 0.583 53 165 0.583 54 162 0.578 55 162 0.578 56 162 0.578 57 162 0.578 58 162 0.578 59 168 0.569 60 168 0.569 61 168 0.569 62 168 0.569 63 168 0.569 64 168 0.569 65 168 0.569 66 171 0.618	67 171 0.618 68 171 0.618 69 168 0.633 70 168 0.633 2 0.0 1 86 0.63 2 86 0.63 3 88 0.602 4 88 0.602 5 88 0.602 6 89 0.558 7 89 0.558 8 89 0.558 9 89 0.558 10 89 0.558 11 89 0.558 12 89 0.558 13 87 0.57 14 87 0.57 15 87 0.57 16 87 0.57 17 87 0.57 18 83 0.578 19 83 0.578 20 83 0.578 21 80 0.573 22 80 0.573 23 80 0.573 24 81 0.59 25 81 0.59 26 81 0.59 27 71 0.618 28 63 0.549 29 63 0.549 30 61 0.534 31 61 0.534 32 61 0.534 33 59 0.545 34 59 0.545 35 59 0.545 36 55 0.532 37 55 0.532 38 55 0.532 39 56 0.546 40 56 0.546 41 56 0.546 42 58 0.562 43 58 0.562 44 69 0.624 45 77 0.606 46 77 0.606 47 77 0.606 48 76 0.581 49 76 0.581 50 76 0.581 51 79 0.585 52 79 0.585 53 79 0.585 54 82 0.583 55 82 0.583	56 82 0.583 57 82 0.583 58 82 0.583 59 85 0.575 60 85 0.575 61 85 0.575 62 85 0.575 63 85 0.575 64 85 0.575 65 85 0.575 66 84 0.626 67 84 0.626 68 84 0.626 69 83 0.634 70 83 0.634 3 0.0 1 66 0.629 2 66 0.629 3 67 0.611 4 67 0.611 5 67 0.611 6 60 0.559 7 60 0.559 8 60 0.559 9 60 0.559 10 60 0.559 11 60 0.559 12 60 0.559 13 58 0.583 14 58 0.583 15 58 0.583 16 58 0.583 17 58 0.583 18 51 0.576 19 51 0.576 20 51 0.576 21 49 0.575 22 49 0.575 23 49 0.575 24 48 0.587 25 48 0.587 26 48 0.587 27 42 0.618 28 45 0.549 29 45 0.549 30 43 0.549 31 43 0.549 32 43 0.549 33 43 0.534 34 43 0.534 35 43 0.534 36 39 0.551 37 39 0.551 38 39 0.551 39 40 0.546 40 40 0.546 41 40 0.546 42 41 0.574 43 41 0.574 44 41 0.618
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Air Quality Impact Assessment for the 407 Transitway (Highway 400 to Kennedy Road)

45 46 0.594	34 37 0.528	23 121 0.561	12 538 0.556	1 2372 0.618	61 1995 0.566	50 4244 0.572
46 46 0.594	35 37 0.528	24 120 0.592	13 525 0.57	2 2372 0.618	62 1995 0.566	51 4403 0.579
47 46 0.594	36 34 0.531	25 120 0.592	14 525 0.57	3 2416 0.597	63 1995 0.566	52 4403 0.579
48 46 0.596	37 34 0.531	26 120 0.592	15 525 0.57	4 2416 0.597	64 1995 0.566	53 4403 0.579
49 46 0.596	38 34 0.531	27 106 0.611	16 525 0.57	5 2416 0.597	65 1995 0.566	54 4453 0.574
50 46 0.596	39 33 0.542	28 77 0.549	17 525 0.57	6 2078 0.555	66 2321 0.612	55 4453 0.574
51 48 0.596	40 33 0.542	29 77 0.549	18 508 0.569	7 2078 0.555	67 2321 0.612	56 4453 0.574
52 48 0.596	41 33 0.542	30 74 0.543	19 508 0.569	8 2078 0.555	68 2321 0.612	57 4453 0.574
53 48 0.596	42 34 0.564	31 74 0.543	20 508 0.569	9 2078 0.555	69 2277 0.63	58 4453 0.574
54 55 0.59	43 34 0.564	32 74 0.543	21 491 0.561	10 2078 0.555	70 2277 0.63	59 4615 0.566
55 55 0.59	44 46 0.635	33 70 0.533	22 491 0.561	11 2078 0.555	8 0.0	60 4615 0.566
56 55 0.59	45 52 0.602	34 70 0.533	23 491 0.561	12 2078 0.555	1 5161 0.618	61 4615 0.566
57 55 0.59	46 52 0.602	35 70 0.533	24 480 0.586	13 2028 0.568	2 5161 0.618	62 4615 0.566
58 55 0.59	47 52 0.602	36 64 0.542	25 480 0.586	14 2028 0.568	3 5257 0.597	63 4615 0.566
59 57 0.582	48 51 0.587	37 64 0.542	26 480 0.586	15 2028 0.568	4 5257 0.597	64 4615 0.566
60 57 0.582	49 51 0.587	38 64 0.542	27 425 0.602	16 2028 0.568	5 5257 0.597	65 4615 0.566
61 57 0.582	50 51 0.587	39 69 0.537	28 361 0.548	17 2028 0.568	6 4806 0.555	66 5051 0.612
62 57 0.582	51 53 0.592	40 69 0.537	29 361 0.548	18 2006 0.568	7 4806 0.555	67 5051 0.612
63 57 0.582	52 53 0.592	41 69 0.537	30 349 0.535	19 2006 0.568	8 4806 0.555	68 5051 0.612
64 57 0.582	53 53 0.592	42 71 0.56	31 349 0.535	20 2006 0.568	9 4806 0.555	69 4955 0.629
65 57 0.582	54 56 0.578	43 71 0.56	32 349 0.535	21 1938 0.561	10 4806 0.555	70 4955 0.629
66 65 0.615	55 56 0.578	44 103 0.617	33 336 0.53	22 1938 0.561	11 4806 0.555	9 0.0
67 65 0.615	56 56 0.578	45 115 0.599	34 336 0.53	23 1938 0.561	12 4806 0.555	1 6495 0.618
68 65 0.615	57 56 0.578	46 115 0.599	35 336 0.53	24 1933 0.584	13 4692 0.568	2 6495 0.618
69 63 0.647	58 56 0.578	47 115 0.599	36 310 0.528	25 1933 0.584	14 4692 0.568	3 6616 0.597
70 63 0.647	59 58 0.571	48 114 0.578	37 310 0.528	26 1933 0.584	15 4692 0.568	4 6616 0.597
4 0.0	60 58 0.571	49 114 0.578	38 310 0.528	27 1708 0.602	16 4692 0.568	5 6616 0.597
1 62 0.631	61 58 0.571	50 114 0.578	39 324 0.533	28 1535 0.548	17 4692 0.568	6 6103 0.555
2 62 0.631	62 58 0.571	51 118 0.587	40 324 0.533	29 1535 0.548	18 4640 0.568	7 6103 0.555
3 63 0.612	63 58 0.571	52 118 0.587	41 324 0.533	30 1486 0.534	19 4640 0.568	8 6103 0.555
4 63 0.612	64 58 0.571	53 118 0.587	42 335 0.551	31 1486 0.534	20 4640 0.568	9 6103 0.555
5 63 0.612	65 58 0.571	54 123 0.577	43 335 0.551	32 1486 0.534	21 4483 0.561	10 6103 0.555
6 60 0.568	66 61 0.618	55 123 0.577	44 411 0.613	33 1408 0.528	22 4483 0.561	11 6103 0.555
7 60 0.568	67 61 0.618	56 123 0.577	45 459 0.595	34 1408 0.528	23 4483 0.561	12 6103 0.555
8 60 0.568	68 61 0.618	57 123 0.577	46 459 0.595	35 1408 0.528	24 4559 0.584	13 5957 0.568
9 60 0.568	69 60 0.632	58 123 0.577	47 459 0.595	36 1300 0.525	25 4559 0.584	14 5957 0.568
10 60 0.568	70 60 0.632	59 127 0.573	48 464 0.575	37 1300 0.525	26 4559 0.584	15 5957 0.568
11 60 0.568	5 0.0	60 127 0.573	49 464 0.575	38 1300 0.525	27 4029 0.602	16 5957 0.568
12 60 0.568	1 157 0.625	61 127 0.573	50 464 0.575	39 1379 0.533	28 3811 0.548	17 5957 0.568
13 59 0.573	2 157 0.625	62 127 0.573	51 482 0.58	40 1379 0.533	29 3811 0.548	18 6012 0.568
14 59 0.573	3 160 0.602	63 127 0.573	52 482 0.58	41 1379 0.533	30 3689 0.533	19 6012 0.568
15 59 0.573	4 160 0.602	64 127 0.573	53 482 0.58	42 1427 0.55	31 3689 0.533	20 6012 0.568
16 59 0.573	5 160 0.602	65 127 0.573	54 499 0.574	43 1427 0.55	32 3689 0.533	21 5809 0.561
17 59 0.573	6 133 0.556	66 154 0.616	55 499 0.574	44 1655 0.611	33 3438 0.528	22 5809 0.561
18 56 0.578	7 133 0.556	67 154 0.616	56 499 0.574	45 1847 0.594	34 3438 0.528	23 5809 0.561
19 56 0.578	8 133 0.556	68 154 0.616	57 499 0.574	46 1847 0.594	35 3438 0.528	24 5982 0.584
20 56 0.578	9 133 0.556	69 151 0.634	58 499 0.574	47 1847 0.594	36 3175 0.525	25 5982 0.584
21 54 0.573	10 133 0.556	70 151 0.634	59 517 0.566	48 1835 0.572	37 3175 0.525	26 5982 0.584
22 54 0.573	11 133 0.556	6 0.0	60 517 0.566	49 1835 0.572	38 3175 0.525	27 5287 0.602
23 54 0.573	12 133 0.556	1 595 0.62	61 517 0.566	50 1835 0.572	39 3424 0.532	28 4842 0.548
24 54 0.601	13 129 0.576	2 595 0.62	62 517 0.566	51 1903 0.579	40 3424 0.532	29 4842 0.548
25 54 0.601	14 129 0.576	3 606 0.598	63 517 0.566	52 1903 0.579	41 3424 0.532	30 4688 0.533
26 54 0.601	15 129 0.576	4 606 0.598	64 517 0.566	53 1903 0.579	42 3542 0.549	31 4688 0.533
27 48 0.613	16 129 0.576	5 606 0.598	65 517 0.566	54 1925 0.574	43 3542 0.549	32 4688 0.533
28 37 0.549	17 129 0.576	6 538 0.556	66 583 0.612	55 1925 0.574	44 3904 0.611	33 4145 0.528
29 37 0.549	18 125 0.571	7 538 0.556	67 583 0.612	56 1925 0.574	45 4357 0.593	34 4145 0.528
30 35 0.56	19 125 0.571	8 538 0.556	68 583 0.612	57 1925 0.574	46 4357 0.593	35 4145 0.528
31 35 0.56	20 125 0.571	9 538 0.556	69 571 0.631	58 1925 0.574	47 4357 0.593	36 3828 0.525
32 35 0.56	21 121 0.561	10 538 0.556	70 571 0.631	59 1995 0.566	48 4244 0.572	37 3828 0.525
33 37 0.528	22 121 0.561	11 538 0.556	7 0.0	60 1995 0.566	49 4244 0.572	38 3828 0.525

Air Quality Impact Assessment for the 407 Transitway (Highway 400 to Kennedy Road)

39 4351 0.532	28 2691 0.548	17 2526 0.568	6 2519 0.555	66 2583 0.612	55 2264 0.574	44 2263 0.611
40 4351 0.532	29 2691 0.548	18 2590 0.568	7 2519 0.555	67 2583 0.612	56 2264 0.574	45 2525 0.594
41 4351 0.532	30 2605 0.533	19 2590 0.568	8 2519 0.555	68 2583 0.612	57 2264 0.574	46 2525 0.594
42 4501 0.549	31 2605 0.533	20 2590 0.568	9 2519 0.555	69 2534 0.63	58 2264 0.574	47 2525 0.594
43 4501 0.549	32 2605 0.533	21 2502 0.561	10 2519 0.555	70 2534 0.63	59 2347 0.566	48 2443 0.573
44 5123 0.611	33 2282 0.528	22 2502 0.561	11 2519 0.555	13 0.0	60 2347 0.566	49 2443 0.573
45 5717 0.594	34 2282 0.528	23 2502 0.561	12 2519 0.555	1 2602 0.619	61 2347 0.566	50 2443 0.573
46 5717 0.594	35 2282 0.528	24 2495 0.584	13 2459 0.568	2 2602 0.619	62 2347 0.566	51 2535 0.579
47 5717 0.594	36 2108 0.525	25 2495 0.584	14 2459 0.568	3 2651 0.597	63 2347 0.566	52 2535 0.579
48 5499 0.572	37 2108 0.525	26 2495 0.584	15 2459 0.568	4 2651 0.597	64 2347 0.566	53 2535 0.579
49 5499 0.572	38 2108 0.525	27 2205 0.602	16 2459 0.568	5 2651 0.597	65 2347 0.566	54 2441 0.574
50 5499 0.572	39 2418 0.532	28 1725 0.548	17 2459 0.568	6 2444 0.555	66 2547 0.612	55 2441 0.574
51 5705 0.579	40 2418 0.532	29 1725 0.548	18 2531 0.568	7 2444 0.555	67 2547 0.612	56 2441 0.574
52 5705 0.579	41 2418 0.532	30 1670 0.533	19 2531 0.568	8 2444 0.555	68 2547 0.612	57 2441 0.574
53 5705 0.579	42 2501 0.55	31 1670 0.533	20 2531 0.568	9 2444 0.555	69 2498 0.63	58 2441 0.574
54 5654 0.574	43 2501 0.55	32 1670 0.533	21 2445 0.561	10 2444 0.555	70 2498 0.63	59 2530 0.566
55 5654 0.574	44 3114 0.611	33 1438 0.528	22 2445 0.561	11 2444 0.555	14 0.0	60 2530 0.566
56 5654 0.574	45 3475 0.594	34 1438 0.528	23 2445 0.561	12 2444 0.555	1 2807 0.618	61 2530 0.566
57 5654 0.574	46 3475 0.594	35 1438 0.528	24 2507 0.584	13 2385 0.568	2 2807 0.618	62 2530 0.566
58 5654 0.574	47 3475 0.594	36 1328 0.525	25 2507 0.584	14 2385 0.568	3 2859 0.597	63 2530 0.566
59 5860 0.566	48 3393 0.572	37 1328 0.525	26 2507 0.584	15 2385 0.568	4 2859 0.597	64 2530 0.566
60 5860 0.566	49 3393 0.572	38 1328 0.525	27 2216 0.602	16 2385 0.568	5 2859 0.597	65 2530 0.566
61 5860 0.566	50 3393 0.572	39 1549 0.533	28 1694 0.548	17 2385 0.568	6 2635 0.555	66 2747 0.612
62 5860 0.566	51 3520 0.579	40 1549 0.533	29 1694 0.548	18 2509 0.568	7 2635 0.555	67 2747 0.612
63 5860 0.566	52 3520 0.579	41 1549 0.533	30 1640 0.533	19 2509 0.568	8 2635 0.555	68 2747 0.612
64 5860 0.566	53 3520 0.579	42 1603 0.55	31 1640 0.533	20 2509 0.568	9 2635 0.555	69 2695 0.629
65 5860 0.566	54 3506 0.574	43 1603 0.55	32 1640 0.533	21 2424 0.561	10 2635 0.555	70 2695 0.629
66 6356 0.612	55 3506 0.574	44 2137 0.611	33 1342 0.528	22 2424 0.561	11 2635 0.555	15 0.0
67 6356 0.612	56 3506 0.574	45 2384 0.594	34 1342 0.528	23 2424 0.561	12 2635 0.555	1 3249 0.619
68 6356 0.612	57 3506 0.574	46 2384 0.594	35 1342 0.528	24 2490 0.584	13 2572 0.568	2 3249 0.619
69 6236 0.629	58 3506 0.574	47 2384 0.594	36 1239 0.525	25 2490 0.584	14 2572 0.568	3 3310 0.597
70 6236 0.629	59 3633 0.566	48 2369 0.573	37 1239 0.525	26 2490 0.584	15 2572 0.568	4 3310 0.597
10 0.0	60 3633 0.566	49 2369 0.573	38 1239 0.525	27 2200 0.602	16 2572 0.568	5 3310 0.597
1 3864 0.618	61 3633 0.566	50 2369 0.573	39 1522 0.533	28 1647 0.548	17 2572 0.568	6 3055 0.555
2 3864 0.618	62 3633 0.566	51 2458 0.579	40 1522 0.533	29 1647 0.548	18 2671 0.569	7 3055 0.555
3 3936 0.597	63 3633 0.566	52 2458 0.579	41 1522 0.533	30 1594 0.534	19 2671 0.569	8 3055 0.555
4 3936 0.597	64 3633 0.566	53 2458 0.579	42 1575 0.549	31 1594 0.534	20 2671 0.569	9 3055 0.555
5 3936 0.597	65 3633 0.566	54 2397 0.574	43 1575 0.549	32 1594 0.534	21 2581 0.561	10 3055 0.555
6 3784 0.555	66 3781 0.612	55 2397 0.574	44 2147 0.611	33 1382 0.528	22 2581 0.561	11 3055 0.555
7 3784 0.555	67 3781 0.612	56 2397 0.574	45 2396 0.594	34 1382 0.528	23 2581 0.561	12 3055 0.555
8 3784 0.555	68 3781 0.612	57 2397 0.574	46 2396 0.594	35 1382 0.528	24 2642 0.584	13 2982 0.568
9 3784 0.555	69 3709 0.63	58 2397 0.574	47 2396 0.594	36 1276 0.525	25 2642 0.584	14 2982 0.568
10 3784 0.555	70 3709 0.63	59 2485 0.566	48 2315 0.573	37 1276 0.525	26 2642 0.584	15 2982 0.568
11 3784 0.555	11 0.0	60 2485 0.566	49 2315 0.573	38 1276 0.525	27 2335 0.602	16 2982 0.568
12 3784 0.555	1 2706 0.619	61 2485 0.566	50 2315 0.573	39 1480 0.532	28 1706 0.548	17 2982 0.568
13 3693 0.568	2 2706 0.619	62 2485 0.566	51 2402 0.579	40 1480 0.532	29 1706 0.548	18 3014 0.568
14 3693 0.568	3 2757 0.597	63 2485 0.566	52 2402 0.579	41 1480 0.532	30 1652 0.533	19 3014 0.568
15 3693 0.568	4 2757 0.597	64 2485 0.566	53 2402 0.579	42 1531 0.55	31 1652 0.533	20 3014 0.568
16 3693 0.568	5 2757 0.597	65 2485 0.566	54 2334 0.574	43 1531 0.55	32 1652 0.533	21 2912 0.561
17 3693 0.568	6 2588 0.555	66 2648 0.613	55 2334 0.574	44 2132 0.611	33 1424 0.528	22 2912 0.561
18 3709 0.568	7 2588 0.555	67 2648 0.613	56 2334 0.574	45 2379 0.594	34 1424 0.528	23 2912 0.561
19 3709 0.568	8 2588 0.555	68 2648 0.613	57 2334 0.574	46 2379 0.594	35 1424 0.528	24 2937 0.584
20 3709 0.568	9 2588 0.555	69 2598 0.63	58 2334 0.574	47 2379 0.594	36 1315 0.526	25 2937 0.584
21 3584 0.561	10 2588 0.555	70 2598 0.63	59 2419 0.566	48 2295 0.573	37 1315 0.526	26 2937 0.584
22 3584 0.561	11 2588 0.555	12 0.0	60 2419 0.566	49 2295 0.573	38 1315 0.526	27 2595 0.602
23 3584 0.561	12 2588 0.555	1 2640 0.618	61 2419 0.566	50 2295 0.573	39 1533 0.532	28 1980 0.548
24 3636 0.584	13 2526 0.568	2 2640 0.618	62 2419 0.566	51 2381 0.579	40 1533 0.532	29 1980 0.548
25 3636 0.584	14 2526 0.568	3 2689 0.597	63 2419 0.566	52 2381 0.579	41 1533 0.532	30 1917 0.533
26 3636 0.584	15 2526 0.568	4 2689 0.597	64 2419 0.566	53 2381 0.579	42 1586 0.549	31 1917 0.533
27 3214 0.602	16 2526 0.568	5 2689 0.597	65 2419 0.566	54 2264 0.574	43 1586 0.549	32 1917 0.533

Air Quality Impact Assessment for the 407 Transitway (Highway 400 to Kennedy Road)

33 1646 0.528	22 3949 0.561	11 5818 0.555	18 0.0	60 5989 0.566	49 3326 0.572	38 1156 0.526
34 1646 0.528	23 3949 0.561	12 5818 0.555	1 6552 0.618	61 5989 0.566	50 3326 0.572	39 1208 0.532
35 1646 0.528	24 4067 0.584	13 5680 0.568	2 6552 0.618	62 5989 0.566	51 3450 0.579	40 1208 0.532
36 1520 0.525	25 4067 0.584	14 5680 0.568	3 6675 0.596	63 5989 0.566	52 3450 0.579	41 1208 0.532
37 1520 0.525	26 4067 0.584	15 5680 0.568	4 6675 0.596	64 5989 0.566	53 3450 0.579	42 1249 0.55
38 1520 0.525	27 3595 0.602	16 5680 0.568	5 6675 0.596	65 5989 0.566	54 3471 0.574	43 1249 0.55
39 1779 0.532	28 2787 0.548	17 5680 0.568	6 6237 0.555	66 6412 0.612	55 3471 0.574	44 1529 0.611
40 1779 0.532	29 2787 0.548	18 5568 0.568	7 6237 0.555	67 6412 0.612	56 3471 0.574	45 1706 0.594
41 1779 0.532	30 2698 0.533	19 5568 0.568	8 6237 0.555	68 6412 0.612	57 3471 0.574	46 1706 0.594
42 1840 0.55	31 2698 0.533	20 5568 0.568	9 6237 0.555	69 6290 0.629	58 3471 0.574	47 1706 0.594
43 1840 0.55	32 2698 0.533	21 5380 0.561	10 6237 0.555	70 6290 0.629	59 3597 0.566	48 1653 0.573
44 2515 0.611	33 2487 0.528	22 5380 0.561	11 6237 0.555	19 0.0	60 3597 0.566	49 1653 0.573
45 2807 0.593	34 2487 0.528	23 5380 0.561	12 6237 0.555	1 3839 0.618	61 3597 0.566	50 1653 0.573
46 2807 0.593	35 2487 0.528	24 5466 0.584	13 6088 0.568	2 3839 0.618	62 3597 0.566	51 1715 0.579
47 2807 0.593	36 2296 0.525	25 5466 0.584	14 6088 0.568	3 3910 0.597	63 3597 0.566	52 1715 0.579
48 2756 0.573	37 2296 0.525	26 5466 0.584	15 6088 0.568	4 3910 0.597	64 3597 0.566	53 1715 0.579
49 2756 0.573	38 2296 0.525	27 4831 0.602	16 6088 0.568	5 3910 0.597	65 3597 0.566	54 1663 0.574
50 2756 0.573	39 2504 0.532	28 4166 0.548	17 6088 0.568	6 3746 0.555	66 3757 0.612	55 1663 0.574
51 2860 0.579	40 2504 0.532	29 4166 0.548	18 5887 0.568	7 3746 0.555	67 3757 0.612	56 1663 0.574
52 2860 0.579	41 2504 0.532	30 4033 0.533	19 5887 0.568	8 3746 0.555	68 3757 0.612	57 1663 0.574
53 2860 0.579	42 2590 0.55	31 4033 0.533	20 5887 0.568	9 3746 0.555	69 3685 0.63	58 1663 0.574
54 2831 0.574	43 2590 0.55	32 4033 0.533	21 5687 0.561	10 3746 0.555	70 3685 0.63	59 1723 0.566
55 2831 0.574	44 3483 0.611	33 3726 0.528	22 5687 0.561	11 3746 0.555	20 0.0	60 1723 0.566
56 2831 0.574	45 3887 0.594	34 3726 0.528	23 5687 0.561	12 3746 0.555	1 1823 0.619	61 1723 0.566
57 2831 0.574	46 3887 0.594	35 3726 0.528	24 5813 0.584	13 3657 0.568	2 1823 0.619	62 1723 0.566
58 2831 0.574	47 3887 0.594	36 3441 0.525	25 5813 0.584	14 3657 0.568	3 1857 0.597	63 1723 0.566
59 2934 0.566	48 3739 0.572	37 3441 0.525	26 5813 0.584	15 3657 0.568	4 1857 0.597	64 1723 0.566
60 2934 0.566	49 3739 0.572	38 3441 0.525	27 5138 0.602	16 3657 0.568	5 1857 0.597	65 1723 0.566
61 2934 0.566	50 3739 0.572	39 3743 0.532	28 4651 0.548	17 3657 0.568	6 1794 0.556	66 1784 0.613
62 2934 0.566	51 3879 0.579	40 3743 0.532	29 4651 0.548	18 3636 0.568	7 1794 0.556	67 1784 0.613
63 2934 0.566	52 3879 0.579	41 3743 0.532	30 4503 0.533	19 3636 0.568	8 1794 0.556	68 1784 0.613
64 2934 0.566	53 3879 0.579	42 3872 0.549	31 4503 0.533	20 3636 0.568	9 1794 0.556	69 1751 0.629
65 2934 0.566	54 3797 0.574	43 3872 0.549	32 4503 0.533	21 3513 0.561	10 1794 0.556	70 1751 0.629
66 3180 0.612	55 3797 0.574	44 4681 0.611	33 3996 0.528	22 3513 0.561	11 1794 0.556	21 0.0
67 3180 0.612	56 3797 0.574	45 5224 0.593	34 3996 0.528	23 3513 0.561	12 1794 0.556	1 1139 0.619
68 3180 0.612	57 3797 0.574	46 5224 0.593	35 3996 0.528	24 3543 0.584	13 1752 0.568	2 1139 0.619
69 3119 0.63	58 3797 0.574	47 5224 0.593	36 3690 0.525	25 3543 0.584	14 1752 0.568	3 1160 0.597
70 3119 0.63	59 3935 0.566	48 5093 0.573	37 3690 0.525	26 3543 0.584	15 1752 0.568	4 1160 0.597
16 0.0	60 3935 0.566	49 5093 0.573	38 3690 0.525	27 3132 0.602	16 1752 0.568	5 1160 0.597
1 4355 0.619	61 3935 0.566	50 5093 0.573	39 4179 0.532	28 2691 0.548	17 1752 0.568	6 1140 0.556
2 4355 0.619	62 3935 0.566	51 5284 0.579	40 4179 0.532	29 2691 0.548	18 1807 0.569	7 1140 0.556
3 4437 0.596	63 3935 0.566	52 5284 0.579	41 4179 0.532	30 2606 0.533	19 1807 0.569	8 1140 0.556
4 4437 0.596	64 3935 0.566	53 5284 0.579	42 4323 0.549	31 2606 0.533	20 1807 0.569	9 1140 0.556
5 4437 0.596	65 3935 0.566	54 5391 0.574	43 4323 0.549	32 2606 0.533	21 1746 0.561	10 1140 0.556
6 4098 0.555	66 4262 0.612	55 5391 0.574	44 4979 0.611	33 2406 0.528	22 1746 0.561	11 1140 0.556
7 4098 0.555	67 4262 0.612	56 5391 0.574	45 5556 0.593	34 2406 0.528	23 1746 0.561	12 1140 0.556
8 4098 0.555	68 4262 0.612	57 5391 0.574	46 5556 0.593	35 2406 0.528	24 1785 0.584	13 1113 0.568
9 4098 0.555	69 4181 0.63	58 5391 0.574	47 5556 0.593	36 2222 0.525	25 1785 0.584	14 1113 0.568
10 4098 0.555	70 4181 0.63	59 5587 0.566	48 5384 0.573	37 2222 0.525	26 1785 0.584	15 1113 0.568
11 4098 0.555	17 0.0	60 5587 0.566	49 5384 0.573	38 2222 0.525	27 1577 0.603	16 1113 0.568
12 4098 0.555	1 6151 0.618	61 5587 0.566	50 5384 0.573	39 2418 0.532	28 1344 0.548	17 1113 0.568
13 4001 0.568	2 6151 0.618	62 5587 0.566	51 5586 0.579	40 2418 0.532	29 1344 0.548	18 1142 0.569
14 4001 0.568	3 6266 0.597	63 5587 0.566	52 5586 0.579	41 2418 0.532	30 1301 0.533	19 1142 0.569
15 4001 0.568	4 6266 0.597	64 5587 0.566	53 5586 0.579	42 2502 0.549	31 1301 0.533	20 1142 0.569
16 4001 0.568	5 6266 0.597	65 5587 0.566	54 5779 0.574	43 2502 0.549	32 1301 0.533	21 1103 0.561
17 4001 0.568	6 5818 0.555	66 6020 0.612	55 5779 0.574	44 3035 0.611	33 1252 0.528	22 1103 0.561
18 4088 0.568	7 5818 0.555	67 6020 0.612	56 5779 0.574	45 3387 0.593	34 1252 0.528	23 1103 0.561
19 4088 0.568	8 5818 0.555	68 6020 0.612	57 5779 0.574	46 3387 0.593	35 1252 0.528	24 1140 0.584
20 4088 0.568	9 5818 0.555	69 5906 0.629	58 5779 0.574	47 3387 0.593	36 1156 0.526	25 1140 0.584
21 3949 0.561	10 5818 0.555	70 5906 0.629	59 5989 0.566	48 3326 0.572	37 1156 0.526	26 1140 0.584

Air Quality Impact Assessment for the 407 Transitway (Highway 400 to Kennedy Road)

27 1007 0.603	16 959 0.569	5 666 0.598	65 613 0.566	54 352 0.574	43 365 0.379	32 182 0.372
28 893 0.548	17 959 0.569	6 638 0.556	66 640 0.613	55 352 0.574	44 422 0.397	33 170 0.371
29 893 0.548	18 952 0.569	7 638 0.556	67 640 0.613	56 352 0.574	45 457 0.395	34 170 0.371
30 864 0.534	19 952 0.569	8 638 0.556	68 640 0.613	57 352 0.574	46 457 0.395	35 170 0.371
31 864 0.534	20 952 0.569	9 638 0.556	69 628 0.63	58 352 0.574	47 457 0.395	36 176 0.373
32 864 0.534	21 920 0.562	10 638 0.556	70 628 0.63	59 364 0.569	48 462 0.393	37 176 0.373
33 837 0.528	22 920 0.562	11 638 0.556	24 0.0	60 364 0.569	49 462 0.393	38 176 0.373
34 837 0.528	23 920 0.562	12 638 0.556	1 366 0.62	61 364 0.569	50 462 0.393	39 186 0.373
35 837 0.528	24 910 0.584	13 623 0.569	2 366 0.62	62 364 0.569	51 482 0.395	40 186 0.373
36 773 0.526	25 910 0.584	14 623 0.569	3 373 0.597	63 364 0.569	52 482 0.395	41 186 0.373
37 773 0.526	26 910 0.584	15 623 0.569	4 373 0.597	64 364 0.569	53 482 0.395	42 186 0.382
38 773 0.526	27 804 0.602	16 623 0.569	5 373 0.597	65 364 0.569	54 479 0.397	43 186 0.382
39 802 0.533	28 722 0.548	17 623 0.569	6 380 0.555	66 358 0.614	55 479 0.397	44 233 0.397
40 802 0.533	29 722 0.548	18 635 0.569	7 380 0.555	67 358 0.614	56 479 0.397	45 252 0.395
41 802 0.533	30 699 0.533	19 635 0.569	8 380 0.555	68 358 0.614	57 479 0.397	46 252 0.395
42 830 0.55	31 699 0.533	20 635 0.569	9 380 0.555	69 351 0.632	58 479 0.397	47 252 0.395
43 830 0.55	32 699 0.533	21 614 0.561	10 380 0.555	70 351 0.632	59 496 0.394	48 243 0.391
44 976 0.611	33 672 0.528	22 614 0.561	11 380 0.555	1 0.0	60 496 0.394	49 243 0.391
45 1089 0.594	34 672 0.528	23 614 0.561	12 380 0.555	1 480 0.414	61 496 0.394	50 243 0.391
46 1089 0.594	35 672 0.528	24 624 0.585	13 370 0.571	2 480 0.414	62 496 0.394	51 253 0.396
47 1089 0.594	36 620 0.527	25 624 0.585	14 370 0.571	3 499 0.406	63 496 0.394	52 253 0.396
48 1044 0.573	37 620 0.527	26 624 0.585	15 370 0.571	4 499 0.406	64 496 0.394	53 253 0.396
49 1044 0.573	38 620 0.527	27 551 0.604	16 370 0.571	5 499 0.406	65 496 0.394	54 252 0.397
50 1044 0.573	39 648 0.533	28 471 0.548	17 370 0.571	6 463 0.39	66 528 0.409	55 252 0.397
51 1084 0.579	40 648 0.533	29 471 0.548	18 371 0.569	7 463 0.39	67 528 0.409	56 252 0.397
52 1084 0.579	41 648 0.533	30 456 0.533	19 371 0.569	8 463 0.39	68 528 0.409	57 252 0.397
53 1084 0.579	42 671 0.55	31 456 0.533	20 371 0.569	9 463 0.39	69 501 0.418	58 252 0.397
54 1056 0.574	43 671 0.55	32 456 0.533	21 358 0.563	10 463 0.39	70 501 0.418	59 261 0.393
55 1056 0.574	44 779 0.611	33 453 0.529	22 358 0.563	11 463 0.39	2 0.0	60 261 0.393
56 1056 0.574	45 869 0.594	34 453 0.529	23 358 0.563	12 463 0.39	1 256 0.417	61 261 0.393
57 1056 0.574	46 869 0.594	35 453 0.529	24 372 0.587	13 457 0.39	2 256 0.417	62 261 0.393
58 1056 0.574	47 869 0.594	36 418 0.527	25 372 0.587	14 457 0.39	3 267 0.406	63 261 0.393
59 1095 0.566	48 871 0.573	37 418 0.527	26 372 0.587	15 457 0.39	4 267 0.406	64 261 0.393
60 1095 0.566	49 871 0.573	38 418 0.527	27 329 0.604	16 457 0.39	5 267 0.406	65 261 0.393
61 1095 0.566	50 871 0.573	39 423 0.533	28 303 0.549	17 457 0.39	6 244 0.389	66 282 0.41
62 1095 0.566	51 904 0.579	40 423 0.533	29 303 0.549	18 473 0.387	7 244 0.389	67 282 0.41
63 1095 0.566	52 904 0.579	41 423 0.533	30 293 0.536	19 473 0.387	8 244 0.389	68 282 0.41
64 1095 0.566	53 904 0.579	42 437 0.552	31 293 0.536	20 473 0.387	9 244 0.389	69 268 0.418
65 1095 0.566	54 910 0.574	43 437 0.552	32 293 0.536	21 454 0.381	10 244 0.389	70 268 0.418
66 1114 0.613	55 910 0.574	44 534 0.612	33 288 0.528	22 454 0.381	11 244 0.389	3 0.0
67 1114 0.613	56 910 0.574	45 596 0.595	34 288 0.528	23 454 0.381	12 244 0.389	1 139 0.416
68 1114 0.613	57 910 0.574	46 596 0.595	35 288 0.528	24 445 0.389	13 240 0.391	2 139 0.416
69 1093 0.63	58 910 0.574	47 596 0.595	36 266 0.526	25 445 0.389	14 240 0.391	3 144 0.411
70 1093 0.63	59 943 0.567	48 581 0.573	37 266 0.526	26 445 0.389	15 240 0.391	4 144 0.411
22 0.0	60 943 0.567	49 581 0.573	38 266 0.526	27 405 0.389	16 240 0.391	5 144 0.411
1 979 0.618	61 943 0.567	50 581 0.573	39 272 0.535	28 361 0.377	17 240 0.391	6 131 0.392
2 979 0.618	62 943 0.567	51 603 0.579	40 272 0.535	29 361 0.377	18 248 0.389	7 131 0.392
3 997 0.597	63 943 0.567	52 603 0.579	41 272 0.535	30 356 0.373	19 248 0.389	8 131 0.392
4 997 0.597	64 943 0.567	53 603 0.579	42 282 0.55	31 356 0.373	20 248 0.389	9 131 0.392
5 997 0.597	65 943 0.567	54 591 0.575	43 282 0.55	32 356 0.373	21 238 0.383	10 131 0.392
6 982 0.556	66 958 0.612	55 591 0.575	44 319 0.612	33 331 0.367	22 238 0.383	11 131 0.392
7 982 0.556	67 958 0.612	56 591 0.575	45 356 0.595	34 331 0.367	23 238 0.383	12 131 0.392
8 982 0.556	68 958 0.612	57 591 0.575	46 356 0.595	35 331 0.367	24 245 0.391	13 129 0.393
9 982 0.556	69 939 0.63	58 591 0.575	47 356 0.595	36 342 0.371	25 245 0.391	14 129 0.393
10 982 0.556	70 939 0.63	59 613 0.566	48 339 0.574	37 342 0.371	26 245 0.391	15 129 0.393
11 982 0.556	23 0.0	60 613 0.566	49 339 0.574	38 342 0.371	27 223 0.391	16 129 0.393
12 982 0.556	1 654 0.619	61 613 0.566	50 339 0.574	39 364 0.373	28 184 0.38	17 129 0.393
13 959 0.569	2 654 0.619	62 613 0.566	51 352 0.58	40 364 0.373	29 184 0.38	18 136 0.389
14 959 0.569	3 666 0.598	63 613 0.566	52 352 0.58	41 364 0.373	30 182 0.372	19 136 0.389
15 959 0.569	4 666 0.598	64 613 0.566	53 352 0.58	42 365 0.379	31 182 0.372	20 136 0.389

Air Quality Impact Assessment for the 407 Transitway (Highway 400 to Kennedy Road)

21 130 0.387	10 99 0.393	70 112 0.425	59 104 0.397	48 155 0.395	37 265 0.371	26 652 0.388
22 130 0.387	11 99 0.393	5 0.0	60 104 0.397	49 155 0.395	38 265 0.371	27 593 0.388
23 130 0.387	12 99 0.393	1 105 0.417	61 104 0.397	50 155 0.395	39 285 0.375	28 512 0.377
24 135 0.391	13 98 0.39	2 105 0.417	62 104 0.397	51 162 0.396	40 285 0.375	29 512 0.377
25 135 0.391	14 98 0.39	3 109 0.41	63 104 0.397	52 162 0.396	41 285 0.375	30 505 0.372
26 135 0.391	15 98 0.39	4 109 0.41	64 104 0.397	53 162 0.396	42 286 0.38	31 505 0.372
27 123 0.39	16 98 0.39	5 109 0.41	65 104 0.397	54 178 0.398	43 286 0.38	32 505 0.372
28 107 0.382	17 98 0.39	6 97 0.394	66 116 0.408	55 178 0.398	44 358 0.398	33 457 0.368
29 107 0.382	18 102 0.393	7 97 0.394	67 116 0.408	56 178 0.398	45 388 0.395	34 457 0.368
30 106 0.374	19 102 0.393	8 97 0.394	68 116 0.408	57 178 0.398	46 388 0.395	35 457 0.368
31 106 0.374	20 102 0.393	9 97 0.394	69 109 0.426	58 178 0.398	47 388 0.395	36 472 0.372
32 106 0.374	21 98 0.386	10 97 0.394	70 109 0.426	59 184 0.396	48 400 0.392	37 472 0.372
33 98 0.369	22 98 0.386	11 97 0.394	6 0.0	60 184 0.396	49 400 0.392	38 472 0.372
34 98 0.369	23 98 0.386	12 97 0.394	1 191 0.417	61 184 0.396	50 400 0.392	39 516 0.373
35 98 0.369	24 92 0.393	13 96 0.391	2 191 0.417	62 184 0.396	51 417 0.395	40 516 0.373
36 101 0.374	25 92 0.393	14 96 0.391	3 199 0.407	63 184 0.396	52 417 0.395	41 516 0.373
37 101 0.374	26 92 0.393	15 96 0.391	4 199 0.407	64 184 0.396	53 417 0.395	42 517 0.38
38 101 0.374	27 84 0.39	16 96 0.391	5 199 0.407	65 184 0.396	54 433 0.397	43 517 0.38
39 108 0.377	28 78 0.387	17 96 0.391	6 172 0.391	66 211 0.408	55 433 0.397	44 617 0.398
40 108 0.377	29 78 0.387	18 92 0.394	7 172 0.391	67 211 0.408	56 433 0.397	45 669 0.394
41 108 0.377	30 77 0.381	19 92 0.394	8 172 0.391	68 211 0.408	57 433 0.397	46 669 0.394
42 108 0.386	31 77 0.381	20 92 0.394	9 172 0.391	69 199 0.422	58 433 0.397	47 669 0.394
43 108 0.386	32 77 0.381	21 89 0.381	10 172 0.391	70 199 0.422	59 448 0.395	48 677 0.391
44 128 0.4	33 75 0.373	22 89 0.381	11 172 0.391	7 0.0	60 448 0.395	49 677 0.391
45 139 0.395	34 75 0.373	23 89 0.381	12 172 0.391	1 456 0.415	61 448 0.395	50 677 0.391
46 139 0.395	35 75 0.373	24 84 0.394	13 170 0.389	2 456 0.415	62 448 0.395	51 705 0.396
47 139 0.395	36 78 0.371	25 84 0.394	14 170 0.389	3 475 0.406	63 448 0.395	52 705 0.396
48 133 0.394	37 78 0.371	26 84 0.394	15 170 0.389	4 475 0.406	64 448 0.395	53 705 0.396
49 133 0.394	38 78 0.371	27 76 0.399	16 170 0.389	5 475 0.406	65 448 0.395	54 745 0.396
50 133 0.394	39 79 0.379	28 62 0.377	17 170 0.389	6 419 0.389	66 503 0.408	55 745 0.396
51 139 0.395	40 79 0.379	29 62 0.377	18 159 0.388	7 419 0.389	67 503 0.408	56 745 0.396
52 139 0.395	41 79 0.379	30 61 0.375	19 159 0.388	8 419 0.389	68 503 0.408	57 745 0.396
53 139 0.395	42 79 0.387	31 61 0.375	20 159 0.388	9 419 0.389	69 476 0.419	58 745 0.396
54 135 0.402	43 79 0.387	32 61 0.375	21 152 0.386	10 419 0.389	70 476 0.419	59 771 0.393
55 135 0.402	44 87 0.403	33 55 0.379	22 152 0.386	11 419 0.389	8 0.0	60 771 0.393
56 135 0.402	45 94 0.403	34 55 0.379	23 152 0.386	12 419 0.389	1 764 0.414	61 771 0.393
57 135 0.402	46 94 0.403	35 55 0.379	24 148 0.393	13 413 0.39	2 764 0.414	62 771 0.393
58 135 0.402	47 94 0.403	36 57 0.38	25 148 0.393	14 413 0.39	3 794 0.406	63 771 0.393
59 140 0.397	48 100 0.395	37 57 0.38	26 148 0.393	15 413 0.39	4 794 0.406	64 771 0.393
60 140 0.397	49 100 0.395	38 57 0.38	27 135 0.391	16 413 0.39	5 794 0.406	65 771 0.393
61 140 0.397	50 100 0.395	39 62 0.38	28 109 0.378	17 413 0.39	6 721 0.389	66 841 0.408
62 140 0.397	51 104 0.4	40 62 0.38	29 109 0.378	18 409 0.387	7 721 0.389	67 841 0.408
63 140 0.397	52 104 0.4	41 62 0.38	30 107 0.377	19 409 0.387	8 721 0.389	68 841 0.408
64 140 0.397	53 104 0.4	42 62 0.389	31 107 0.377	20 409 0.387	9 721 0.389	69 797 0.418
65 140 0.397	54 102 0.404	43 62 0.389	32 107 0.377	21 392 0.383	10 721 0.389	70 797 0.418
66 153 0.411	55 102 0.404	44 80 0.398	33 100 0.373	22 392 0.383	11 721 0.389	9 0.0
67 153 0.411	56 102 0.404	45 86 0.403	34 100 0.373	23 392 0.383	12 721 0.389	1 1168 0.414
68 153 0.411	57 102 0.404	46 86 0.403	35 100 0.373	24 378 0.389	13 710 0.39	2 1168 0.414
69 145 0.421	58 102 0.404	47 86 0.403	36 104 0.371	25 378 0.389	14 710 0.39	3 1215 0.406
70 145 0.421	59 106 0.397	48 90 0.398	37 104 0.371	26 378 0.389	15 710 0.39	4 1215 0.406
4 0.0	60 106 0.397	49 90 0.398	38 104 0.371	27 344 0.389	16 710 0.39	5 1215 0.406
1 108 0.415	61 106 0.397	50 90 0.398	39 110 0.373	28 283 0.378	17 710 0.39	6 1147 0.389
2 108 0.415	62 106 0.397	51 94 0.4	40 110 0.373	29 283 0.378	18 693 0.386	7 1147 0.389
3 112 0.409	63 106 0.397	52 94 0.4	41 110 0.373	30 279 0.373	19 693 0.386	8 1147 0.389
4 112 0.409	64 106 0.397	53 94 0.4	42 110 0.382	31 279 0.373	20 693 0.386	9 1147 0.389
5 112 0.409	65 106 0.397	54 100 0.404	43 110 0.382	32 279 0.373	21 664 0.382	10 1147 0.389
6 99 0.393	66 119 0.408	55 100 0.404	44 141 0.397	33 256 0.369	22 664 0.382	11 1147 0.389
7 99 0.393	67 119 0.408	56 100 0.404	45 152 0.399	34 256 0.369	23 664 0.382	12 1147 0.389
8 99 0.393	68 119 0.408	57 100 0.404	46 152 0.399	35 256 0.369	24 652 0.388	13 1131 0.389
9 99 0.393	69 112 0.425	58 100 0.404	47 152 0.399	36 265 0.371	25 652 0.388	14 1131 0.389

Air Quality Impact Assessment for the 407 Transitway (Highway 400 to Kennedy Road)

15 1131 0.389	4 1473 0.406	64 1490 0.393	53 1636 0.395	42 1307 0.38	31 1354 0.371	20 1915 0.386
16 1131 0.389	5 1473 0.406	65 1490 0.393	54 1608 0.396	43 1307 0.38	32 1354 0.371	21 1837 0.38
17 1131 0.389	6 1392 0.389	66 1560 0.408	55 1608 0.396	44 1583 0.397	33 1247 0.367	22 1837 0.38
18 1157 0.386	7 1392 0.389	67 1560 0.408	56 1608 0.396	45 1714 0.394	34 1247 0.367	23 1837 0.38
19 1157 0.386	8 1392 0.389	68 1560 0.408	57 1608 0.396	46 1714 0.394	35 1247 0.367	24 1833 0.388
20 1157 0.386	9 1392 0.389	69 1479 0.418	58 1608 0.396	47 1714 0.394	36 1288 0.371	25 1833 0.388
21 1110 0.381	10 1392 0.389	70 1479 0.418	59 1665 0.393	48 1709 0.391	37 1288 0.371	26 1833 0.388
22 1110 0.381	11 1392 0.389	11 0.0	60 1665 0.393	49 1709 0.391	38 1288 0.371	27 1668 0.388
23 1110 0.381	12 1392 0.389	1 1585 0.414	61 1665 0.393	50 1709 0.391	39 1383 0.373	28 1417 0.376
24 1122 0.388	13 1373 0.389	2 1585 0.414	62 1665 0.393	51 1780 0.395	40 1383 0.373	29 1417 0.376
25 1122 0.388	14 1373 0.389	3 1648 0.406	63 1665 0.393	52 1780 0.395	41 1383 0.373	30 1399 0.371
26 1122 0.388	15 1373 0.389	4 1648 0.406	64 1665 0.393	53 1780 0.395	42 1386 0.379	31 1399 0.371
27 1021 0.388	16 1373 0.389	5 1648 0.406	65 1665 0.393	54 1767 0.396	43 1386 0.379	32 1399 0.371
28 890 0.376	17 1373 0.389	6 1556 0.389	66 1745 0.408	55 1767 0.396	44 1679 0.397	33 1299 0.367
29 890 0.376	18 1395 0.386	7 1556 0.389	67 1745 0.408	56 1767 0.396	45 1817 0.395	34 1299 0.367
30 878 0.371	19 1395 0.386	8 1556 0.389	68 1745 0.408	57 1767 0.396	46 1817 0.395	35 1299 0.367
31 878 0.371	20 1395 0.386	9 1556 0.389	69 1654 0.418	58 1767 0.396	47 1817 0.395	36 1341 0.371
32 878 0.371	21 1338 0.381	10 1556 0.389	70 1654 0.418	59 1829 0.393	48 1785 0.391	37 1341 0.371
33 792 0.367	22 1338 0.381	11 1556 0.389	12 0.0	60 1829 0.393	49 1785 0.391	38 1341 0.371
34 792 0.367	23 1338 0.381	12 1556 0.389	1 1715 0.414	61 1829 0.393	50 1785 0.391	39 1428 0.373
35 792 0.367	24 1380 0.388	13 1534 0.389	2 1715 0.414	62 1829 0.393	51 1860 0.395	40 1428 0.373
36 818 0.371	25 1380 0.388	14 1534 0.389	3 1783 0.406	63 1829 0.393	52 1860 0.395	41 1428 0.373
37 818 0.371	26 1380 0.388	15 1534 0.389	4 1783 0.406	64 1829 0.393	53 1860 0.395	42 1431 0.379
38 818 0.371	27 1255 0.388	16 1534 0.389	5 1783 0.406	65 1829 0.393	54 1863 0.396	43 1431 0.379
39 896 0.373	28 1081 0.377	17 1534 0.389	6 1710 0.389	66 1888 0.408	55 1863 0.396	44 1737 0.397
40 896 0.373	29 1081 0.377	18 1607 0.386	7 1710 0.389	67 1888 0.408	56 1863 0.396	45 1881 0.394
41 896 0.373	30 1067 0.371	19 1607 0.386	8 1710 0.389	68 1888 0.408	57 1863 0.396	46 1881 0.394
42 898 0.38	31 1067 0.371	20 1607 0.386	9 1710 0.389	69 1789 0.418	58 1863 0.396	47 1881 0.394
43 898 0.38	32 1067 0.371	21 1542 0.381	10 1710 0.389	70 1789 0.418	59 1929 0.393	48 1871 0.391
44 1063 0.397	33 985 0.368	22 1542 0.381	11 1710 0.389	13 0.0	60 1929 0.393	49 1871 0.391
45 1151 0.395	34 985 0.368	23 1542 0.381	12 1710 0.389	1 1835 0.414	61 1929 0.393	50 1871 0.391
46 1151 0.395	35 985 0.368	24 1544 0.388	13 1686 0.389	2 1835 0.414	62 1929 0.393	51 1949 0.395
47 1151 0.395	36 1018 0.371	25 1544 0.388	14 1686 0.389	3 1908 0.406	63 1929 0.393	52 1949 0.395
48 1131 0.391	37 1018 0.371	26 1544 0.388	15 1686 0.389	4 1908 0.406	64 1929 0.393	53 1949 0.395
49 1131 0.391	38 1018 0.371	27 1405 0.388	16 1686 0.389	5 1908 0.406	65 1929 0.393	54 1876 0.396
50 1131 0.391	39 1090 0.373	28 1222 0.377	17 1686 0.389	6 1803 0.389	66 2021 0.408	55 1876 0.396
51 1178 0.395	40 1090 0.373	29 1222 0.377	18 1748 0.386	7 1803 0.389	67 2021 0.408	56 1876 0.396
52 1178 0.395	41 1090 0.373	30 1206 0.371	19 1748 0.386	8 1803 0.389	68 2021 0.408	57 1876 0.396
53 1178 0.395	42 1092 0.379	31 1206 0.371	20 1748 0.386	9 1803 0.389	69 1915 0.418	58 1876 0.396
54 1185 0.397	43 1092 0.379	32 1206 0.371	21 1677 0.381	10 1803 0.389	70 1915 0.418	59 1943 0.393
55 1185 0.397	44 1307 0.397	33 1108 0.367	22 1677 0.381	11 1803 0.389	14 0.0	60 1943 0.393
56 1185 0.397	45 1415 0.395	34 1108 0.367	23 1677 0.381	12 1803 0.389	1 1791 0.414	61 1943 0.393
57 1185 0.397	46 1415 0.395	35 1108 0.367	24 1671 0.388	13 1778 0.389	2 1791 0.414	62 1943 0.393
58 1185 0.397	47 1415 0.395	36 1144 0.371	25 1671 0.388	14 1778 0.389	3 1862 0.406	63 1943 0.393
59 1227 0.393	48 1363 0.391	37 1144 0.371	26 1671 0.388	15 1778 0.389	4 1862 0.406	64 1943 0.393
60 1227 0.393	49 1363 0.391	38 1144 0.371	27 1520 0.388	16 1778 0.389	5 1862 0.406	65 1943 0.393
61 1227 0.393	50 1363 0.391	39 1232 0.373	28 1294 0.377	17 1778 0.389	6 1816 0.389	66 1972 0.408
62 1227 0.393	51 1420 0.395	40 1232 0.373	29 1294 0.377	18 1827 0.386	7 1816 0.389	67 1972 0.408
63 1227 0.393	52 1420 0.395	41 1232 0.373	30 1278 0.371	19 1827 0.386	8 1816 0.389	68 1972 0.408
64 1227 0.393	53 1420 0.395	42 1234 0.38	31 1278 0.371	20 1827 0.386	9 1816 0.389	69 1869 0.418
65 1227 0.393	54 1439 0.396	43 1234 0.38	32 1278 0.371	21 1752 0.381	10 1816 0.389	70 1869 0.418
66 1287 0.408	55 1439 0.396	44 1463 0.397	33 1195 0.367	22 1752 0.381	11 1816 0.389	15 0.0
67 1287 0.408	56 1439 0.396	45 1584 0.394	34 1195 0.367	23 1752 0.381	12 1816 0.389	1 1857 0.414
68 1287 0.408	57 1439 0.396	46 1584 0.394	35 1195 0.367	24 1772 0.387	13 1790 0.389	2 1857 0.414
69 1219 0.418	58 1439 0.396	47 1584 0.394	36 1234 0.371	25 1772 0.387	14 1790 0.389	3 1932 0.405
70 1219 0.418	59 1490 0.393	48 1571 0.391	37 1234 0.371	26 1772 0.387	15 1790 0.389	4 1932 0.405
10 0.0	60 1490 0.393	49 1571 0.391	38 1234 0.371	27 1612 0.388	16 1790 0.389	5 1932 0.405
1 1417 0.414	61 1490 0.393	50 1571 0.391	39 1304 0.373	28 1372 0.377	17 1790 0.389	6 1841 0.389
2 1417 0.414	62 1490 0.393	51 1636 0.395	40 1304 0.373	29 1372 0.377	18 1915 0.386	7 1841 0.389
3 1473 0.406	63 1490 0.393	52 1636 0.395	41 1304 0.373	30 1354 0.371	19 1915 0.386	8 1841 0.389

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9 1841 0.389	69 1938 0.418	58 1977 0.396	47 1875 0.394	36 1444 0.371	25 1843 0.388	14 1278 0.389
10 1841 0.389	70 1938 0.418	59 2047 0.393	48 1868 0.391	37 1444 0.371	26 1843 0.388	15 1278 0.389
11 1841 0.389	16 0.0	60 2047 0.393	49 1868 0.391	38 1444 0.371	27 1677 0.388	16 1278 0.389
12 1841 0.389	1 1900 0.414	61 2047 0.393	50 1868 0.391	39 1541 0.373	28 1432 0.377	17 1278 0.389
13 1815 0.389	2 1900 0.414	62 2047 0.393	51 1946 0.395	40 1541 0.373	29 1432 0.377	18 1318 0.386
14 1815 0.389	3 1976 0.406	63 2047 0.393	52 1946 0.395	41 1541 0.373	30 1414 0.371	19 1318 0.386
15 1815 0.389	4 1976 0.406	64 2047 0.393	53 1946 0.395	42 1544 0.38	31 1414 0.371	20 1318 0.386
16 1815 0.389	5 1976 0.406	65 2047 0.393	54 1933 0.396	43 1544 0.38	32 1414 0.371	21 1265 0.38
17 1815 0.389	6 1913 0.389	66 2093 0.408	55 1933 0.396	44 1840 0.397	33 1327 0.367	22 1265 0.38
18 1886 0.386	7 1913 0.389	67 2093 0.408	56 1933 0.396	45 1992 0.395	34 1327 0.367	23 1265 0.38
19 1886 0.386	8 1913 0.389	68 2093 0.408	57 1933 0.396	46 1992 0.395	35 1327 0.367	24 1259 0.388
20 1886 0.386	9 1913 0.389	69 1983 0.418	58 1933 0.396	47 1992 0.395	36 1371 0.371	25 1259 0.388
21 1810 0.38	10 1913 0.389	70 1983 0.418	59 2002 0.393	48 1965 0.391	37 1371 0.371	26 1259 0.388
22 1810 0.38	11 1913 0.389	17 0.0	60 2002 0.393	49 1965 0.391	38 1371 0.371	27 1146 0.388
23 1810 0.38	12 1913 0.389	1 1856 0.414	61 2002 0.393	50 1965 0.391	39 1443 0.373	28 974 0.376
24 1834 0.388	13 1886 0.389	2 1856 0.414	62 2002 0.393	51 2047 0.395	40 1443 0.373	29 974 0.376
25 1834 0.388	14 1886 0.389	3 1931 0.405	63 2002 0.393	52 2047 0.395	41 1443 0.373	30 961 0.371
26 1834 0.388	15 1886 0.389	4 1931 0.405	64 2002 0.393	53 2047 0.395	42 1447 0.379	31 961 0.371
27 1669 0.388	16 1886 0.389	5 1931 0.405	65 2002 0.393	54 2035 0.396	43 1447 0.379	32 961 0.371
28 1425 0.376	17 1886 0.389	6 1871 0.389	66 2045 0.408	55 2035 0.396	44 1746 0.397	33 913 0.367
29 1425 0.376	18 1906 0.386	7 1871 0.389	67 2045 0.408	56 2035 0.396	45 1891 0.395	34 913 0.367
30 1406 0.371	19 1906 0.386	8 1871 0.389	68 2045 0.408	57 2035 0.396	46 1891 0.395	35 913 0.367
31 1406 0.371	20 1906 0.386	9 1871 0.389	69 1937 0.418	58 2035 0.396	47 1891 0.395	36 943 0.371
32 1406 0.371	21 1828 0.381	10 1871 0.389	70 1937 0.418	59 2107 0.393	48 1886 0.391	37 943 0.371
33 1320 0.367	22 1828 0.381	11 1871 0.389	18 0.0	60 2107 0.393	49 1886 0.391	38 943 0.371
34 1320 0.367	23 1828 0.381	12 1871 0.389	1 1971 0.414	61 2107 0.393	50 1886 0.391	39 982 0.373
35 1320 0.367	24 1830 0.388	13 1845 0.389	2 1971 0.414	62 2107 0.393	51 1965 0.395	40 982 0.373
36 1364 0.371	25 1830 0.388	14 1845 0.389	3 2050 0.406	63 2107 0.393	52 1965 0.395	41 982 0.373
37 1364 0.371	26 1830 0.388	15 1845 0.389	4 2050 0.406	64 2107 0.393	53 1965 0.395	42 984 0.379
38 1364 0.371	27 1665 0.388	16 1845 0.389	5 2050 0.406	65 2107 0.393	54 1913 0.396	43 984 0.379
39 1436 0.373	28 1444 0.376	17 1845 0.389	6 1969 0.389	66 2171 0.408	55 1913 0.396	44 1193 0.397
40 1436 0.373	29 1444 0.376	18 1912 0.386	7 1969 0.389	67 2171 0.408	56 1913 0.396	45 1292 0.395
41 1436 0.373	30 1426 0.371	19 1912 0.386	8 1969 0.389	68 2171 0.408	57 1913 0.396	46 1292 0.395
42 1439 0.379	31 1426 0.371	20 1912 0.386	9 1969 0.389	69 2057 0.418	58 1913 0.396	47 1292 0.395
43 1439 0.379	32 1426 0.371	21 1834 0.381	10 1969 0.389	70 2057 0.418	59 1981 0.393	48 1288 0.391
44 1738 0.397	33 1318 0.367	22 1834 0.381	11 1969 0.389	19 0.0	60 1981 0.393	49 1288 0.391
45 1881 0.395	34 1318 0.367	23 1834 0.381	12 1969 0.389	1 1840 0.414	61 1981 0.393	50 1288 0.391
46 1881 0.395	35 1318 0.367	24 1827 0.388	13 1942 0.389	2 1840 0.414	62 1981 0.393	51 1342 0.395
47 1881 0.395	36 1362 0.371	25 1827 0.388	14 1942 0.389	3 1913 0.406	63 1981 0.393	52 1342 0.395
48 1844 0.391	37 1362 0.371	26 1827 0.388	15 1942 0.389	4 1913 0.406	64 1981 0.393	53 1342 0.395
49 1844 0.391	38 1362 0.371	27 1663 0.388	16 1942 0.389	5 1913 0.406	65 1981 0.393	54 1339 0.397
50 1844 0.391	39 1456 0.373	28 1466 0.376	17 1942 0.389	6 1852 0.388	66 2026 0.408	55 1339 0.397
51 1921 0.395	40 1456 0.373	29 1466 0.376	18 2011 0.386	7 1852 0.388	67 2026 0.408	56 1339 0.397
52 1921 0.395	41 1456 0.373	30 1447 0.371	19 2011 0.386	8 1852 0.388	68 2026 0.408	57 1339 0.397
53 1921 0.395	42 1459 0.379	31 1447 0.371	20 2011 0.386	9 1852 0.388	69 1920 0.418	58 1339 0.397
54 1902 0.396	43 1459 0.379	32 1447 0.371	21 1929 0.381	10 1852 0.388	70 1920 0.418	59 1387 0.393
55 1902 0.396	44 1734 0.397	33 1340 0.368	22 1929 0.381	11 1852 0.388	20 0.0	60 1387 0.393
56 1902 0.396	45 1878 0.394	34 1340 0.368	23 1929 0.381	12 1852 0.388	1 1269 0.414	61 1387 0.393
57 1902 0.396	46 1878 0.394	35 1340 0.368	24 1942 0.388	13 1825 0.389	2 1269 0.414	62 1387 0.393
58 1902 0.396	47 1878 0.394	36 1385 0.371	25 1942 0.388	14 1825 0.389	3 1320 0.406	63 1387 0.393
59 1969 0.393	48 1863 0.391	37 1385 0.371	26 1942 0.388	15 1825 0.389	4 1320 0.406	64 1387 0.393
60 1969 0.393	49 1863 0.391	38 1385 0.371	27 1767 0.388	16 1825 0.389	5 1320 0.406	65 1387 0.393
61 1969 0.393	50 1863 0.391	39 1477 0.373	28 1529 0.376	17 1825 0.389	6 1296 0.389	66 1398 0.408
62 1969 0.393	51 1940 0.395	40 1477 0.373	29 1529 0.376	18 1930 0.386	7 1296 0.389	67 1398 0.408
63 1969 0.393	52 1940 0.395	41 1477 0.373	30 1509 0.371	19 1930 0.386	8 1296 0.389	68 1398 0.408
64 1969 0.393	53 1940 0.395	42 1480 0.379	31 1509 0.371	20 1930 0.386	9 1296 0.389	69 1325 0.418
65 1969 0.393	54 1977 0.396	43 1480 0.379	32 1509 0.371	21 1852 0.38	10 1296 0.389	70 1325 0.418
66 2046 0.408	55 1977 0.396	44 1731 0.397	33 1398 0.367	22 1852 0.38	11 1296 0.389	21 0.0
67 2046 0.408	56 1977 0.396	45 1875 0.394	34 1398 0.367	23 1852 0.38	12 1296 0.389	1 822 0.414
68 2046 0.408	57 1977 0.396	46 1875 0.394	35 1398 0.367	24 1843 0.388	13 1278 0.389	2 822 0.414

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3 855 0.406	63 895 0.393	52 754 0.395	41 632 0.373	30 603 0.371
4 855 0.406	64 895 0.393	53 754 0.395	42 634 0.379	31 603 0.371
5 855 0.406	65 895 0.393	54 728 0.396	43 634 0.379	32 603 0.371
6 836 0.389	66 905 0.408	55 728 0.396	44 713 0.397	33 561 0.367
7 836 0.389	67 905 0.408	56 728 0.396	45 772 0.395	34 561 0.367
8 836 0.389	68 905 0.408	57 728 0.396	46 772 0.395	35 561 0.367
9 836 0.389	69 858 0.418	58 728 0.396	47 772 0.395	36 579 0.372
10 836 0.389	70 858 0.418	59 753 0.394	48 775 0.391	37 579 0.372
11 836 0.389	22 0.0	60 753 0.394	49 775 0.391	38 579 0.372
12 836 0.389	1 687 0.414	61 753 0.394	50 775 0.391	39 616 0.373
13 824 0.39	2 687 0.414	62 753 0.394	51 807 0.395	40 616 0.373
14 824 0.39	3 714 0.406	63 753 0.394	52 807 0.395	41 616 0.373
15 824 0.39	4 714 0.406	64 753 0.394	53 807 0.395	42 617 0.38
16 824 0.39	5 714 0.406	65 753 0.394	54 762 0.397	43 617 0.38
17 824 0.39	6 704 0.389	66 756 0.409	55 762 0.397	44 675 0.397
18 886 0.386	7 704 0.389	67 756 0.409	56 762 0.397	45 731 0.395
19 886 0.386	8 704 0.389	68 756 0.409	57 762 0.397	46 731 0.395
20 886 0.386	9 704 0.389	69 717 0.418	58 762 0.397	47 731 0.395
21 850 0.381	10 704 0.389	70 717 0.418	59 789 0.394	48 755 0.392
22 850 0.381	11 704 0.389	23 0.0	60 789 0.394	49 755 0.392
23 850 0.381	12 704 0.389	1 709 0.414	61 789 0.394	50 755 0.392
24 842 0.388	13 694 0.39	2 709 0.414	62 789 0.394	51 787 0.395
25 842 0.388	14 694 0.39	3 737 0.407	63 789 0.394	52 787 0.395
26 842 0.388	15 694 0.39	4 737 0.407	64 789 0.394	53 787 0.395
27 766 0.389	16 694 0.39	5 737 0.407	65 789 0.394	54 762 0.397
28 660 0.377	17 694 0.39	6 737 0.39	66 781 0.408	55 762 0.397
29 660 0.377	18 740 0.387	7 737 0.39	67 781 0.408	56 762 0.397
30 651 0.372	19 740 0.387	8 737 0.39	68 781 0.408	57 762 0.397
31 651 0.372	20 740 0.387	9 737 0.39	69 740 0.418	58 762 0.397
32 651 0.372	21 710 0.381	10 737 0.39	70 740 0.418	59 789 0.394
33 611 0.367	22 710 0.381	11 737 0.39	24 0.0	60 789 0.394
34 611 0.367	23 710 0.381	12 737 0.39	1 714 0.415	61 789 0.394
35 611 0.367	24 698 0.388	13 727 0.39	2 714 0.415	62 789 0.394
36 631 0.371	25 698 0.388	14 727 0.39	3 743 0.406	63 789 0.394
37 631 0.371	26 698 0.388	15 727 0.39	4 743 0.406	64 789 0.394
38 631 0.371	27 635 0.388	16 727 0.39	5 743 0.406	65 789 0.394
39 665 0.373	28 580 0.376	17 727 0.39	6 737 0.39	66 787 0.408
40 665 0.373	29 580 0.376	18 792 0.387	7 737 0.39	67 787 0.408
41 665 0.373	30 572 0.372	19 792 0.387	8 737 0.39	68 787 0.408
42 667 0.379	31 572 0.372	20 792 0.387	9 737 0.39	69 745 0.419
43 667 0.379	32 572 0.372	21 760 0.381	10 737 0.39	70 745 0.419
44 798 0.397	33 541 0.368	22 760 0.381	11 737 0.39	
45 864 0.395	34 541 0.368	23 760 0.381	12 737 0.39	
46 864 0.395	35 541 0.368	24 753 0.388	13 727 0.39	
47 864 0.395	36 559 0.372	25 753 0.388	14 727 0.39	
48 866 0.391	37 559 0.372	26 753 0.388	15 727 0.39	
49 866 0.391	38 559 0.372	27 685 0.388	16 727 0.39	
50 866 0.391	39 584 0.373	28 627 0.377	17 727 0.39	
51 902 0.395	40 584 0.373	29 627 0.377	18 773 0.386	
52 902 0.395	41 584 0.373	30 619 0.372	19 773 0.386	
53 902 0.395	42 585 0.38	31 619 0.372	20 773 0.386	
54 864 0.397	43 585 0.38	32 619 0.372	21 741 0.381	
55 864 0.397	44 661 0.397	33 571 0.367	22 741 0.381	
56 864 0.397	45 716 0.395	34 571 0.367	23 741 0.381	
57 864 0.397	46 716 0.395	35 571 0.367	24 713 0.388	
58 864 0.397	47 716 0.395	36 589 0.372	25 713 0.388	
59 895 0.393	48 724 0.391	37 589 0.372	26 713 0.388	
60 895 0.393	49 724 0.391	38 589 0.372	27 648 0.389	
61 895 0.393	50 724 0.391	39 632 0.373	28 611 0.377	
62 895 0.393	51 754 0.395	40 632 0.373	29 611 0.377	

APPENDIX D

BUS STATION MODELLING

D.1 INTRODUCTION

To assess the impact on air quality in the study area from the addition of bus stations for the Future With Transitway (2031) scenario, two stations, GO Barrie (Concord) and Leslie, were modelled due to their close proximity to sensitive receptor locations (R1 and R10, respectively, outlined in Section 4.5). All other station locations are situated at much greater distances from sensitive areas, therefore, the GO Barrie (Concord) and Leslie stations were considered to be worst-case scenarios. If predicted air quality impacts are determined to be minimal at these two stations, then the impacts of the remaining five stations on local air quality will also be minimal.

The atmospheric dispersion model used for the bus station assessment was the U.S. EPA Industrial Source Complex Short Term Version 3 (ISCST3) model, which is described in further detail in Section E.3. The maximum 24-hour model predicted concentrations were added to CAL3QHCR results (including ambient background) to determine the cumulative effect of the Transitway and the bus stations at specific receptor locations (i.e., R1 and R10). Only nitrogen oxides (NO_x) and total suspended particulate (TSP) were modelled as indicators of the impact on air quality.

D.2 ATMOSPHERIC EMISSIONS

D.2.1 DESCRIPTION OF ASSESSMENT SCENARIOS

Leslie Station

Leslie Station will be situated just west of Leslie Street. It is considered to be an intermodal station as it will eventually connect with a proposed Light Rail Transit (LRT) system that will travel north/south on Leslie Street. There are also two (2) proposed parking lots west of Leslie Street and south of the Transitway. As well, there will be a passenger pick-up and drop-off (PPUDO) area located in the larger of the two parking lots. Refer to the main Environmental Project Report (EPR) for the undertaking for a detailed description of the design of this station.

Only emissions from additional vehicular traffic entering/exiting the parking lots will be considered in this scenario. Idling emissions from buses on the Transitway will not be considered as it is expected that one (1) bus will pass through the station every minute during peak travel hours.

GO Barrie (Concord) Station

GO Barrie (Concord) Station will be situated east of the existing GO Barrie rail line. It has been planned that this station will connect with existing VIVA transit buses. There are two proposed parking lots east of the GO Barrie line and north of the Transitway. As well, there will be a passenger pick-up and drop-off (PPUDO) area located in the larger of the two parking lots. A roadway will also be built leading to the parking lots. Again, refer to the main Environmental Project Report (EPR) for the undertaking for a detailed description of the design of this station.

As with Leslie Station, only emissions from additional vehicular traffic entering/exiting the parking lots will be considered in this scenario. Idling emissions from Transitway buses will not be considered as it is expected that one (1) bus will pass through the station every minute during peak travel hours.

D.2.2 EMISSIONS ESTIMATION

In order to be conservative, a maximum emissions scenario was developed to capture expected worst-case maximum daily emissions from the Leslie and GO Barrie (Concord) stations. The worst-case scenario was based upon maximum 24-hour AADT volumes entering/exiting the parking lots provided by IBI Group.

The same emissions estimating methods used for CAL3QHCR modelling were used for this assessment. However, since the speed travelled by vehicles entering/exiting the parking lots will be much less than the posted speed limit on Highway 407 and the Transitway (100 km/h), different MOBILE6C emission factors were used. Typical speeds in parking lots are approximately 25 km/h; however, only MOBILE6C emission factors for either 4 or 40 km/h were available. The TSP emission factors are the same for either speed, but the NO_x emission factor is higher for 40 km/h, therefore, it was selected as it is the more conservative value. MOBILE6C emission factors used in this assessment are shown in the following table.

Table D.1 MOBILE6C Tailpipe Emission Factors for 2031

Cars	
TSP	NO_x
0.01659	0.18828
Trucks/Buses	
TSP	NO_x
0.02187	0.26098

Note: Emission factors are in g/VKT (grams per vehicle kilometre travelled).

D.3 AIR DISPERSION MODELLING

The Industrial Source Complex Short Term Version 3 (ISCST3) model was used with the projected emissions to predict total suspended particulate (TSP) concentrations, as well as nitrogen oxide (NO_x) concentrations, at discrete receptors in the areas surrounding the stations. This model was developed for the U.S. Environmental Protection Agency (U.S. EPA) and was designed specifically to determine downwind air concentrations and deposition rates of various airborne pollutants from industrial sources. The ISCST3 model simulates the dispersion of pollutants by advecting a plume of material with an assumed Gaussian profile. The dilution of the plume as it travels downstream is calculated based on wind speed and mixing caused by atmospheric conditions.

An example ISCST3 input file is provided in Attachment A.

D.3.1 ISCST3 SETTINGS

Emissions from the parking lots were designated as “VOLUME” sources in ISCST3, which applies the total emission rate to a volume of air. In addition, connecting roadways (GO Barrie (Concord) Station only) were designated as “LINE” sources which is a series of volume sources spread evenly out over the length of the source. Emissions from the roadway are divided equally among the generated volume sources. The modelling configurations for both the GO Barrie (Concord) and Leslie Station are shown in Figure E.1 and Figure E2, respectively. Note that the Transitway and Highway 407 CAL3QHCR sources (in blue) were included for reference only – they were not included in ISCST3 modelling.

All contaminants modelled used 24-hour total emissions, with the exception of NO_x, which also has a 1-hour total. The emission rate of NO_x used was the same during the 1-hour period as each hour of the 24-hour periods; therefore, it was not necessary to perform separate model runs for 1-hour and 24-hour averaging times.

The variable emissions option was selected in ISCST3 so that an hourly profile of the parking lot emissions was considered by the model. It was assumed that there are two peak hours of emissions between 7 a.m. and 8 a.m. and 5 p.m. and 6 p.m. when the largest volume of vehicles enter and exit the parking lots at the beginning and end of a typical weekday. Two shoulder hours, before and after the AM and PM peaks, were also considered and were assumed to have fewer vehicles entering/exiting the parking lots. For all remaining hours of the day, emissions were set to zero.

D.3.2 METEOROLOGICAL DATA

The ISCST3 model uses hourly meteorological data records to define the conditions for plume rise, transport and dispersion. The model estimates the concentration or deposition value for each source-receptor combination, for each hour of input meteorology, and calculates short-term averages, such as one-hour, eight-hour and 24-hour periods. The hourly averages can also be combined into longer averages (1-month, seasonal, annual or period).

In this assessment, the ISCST3 model was run using the same meteorological data set that was used for CAL3QHCR modelling. Refer to Section 4.3 for a description of this meteorological data set. Again, the worst case meteorological year, 1993, was used to complete this assessment.

D.3.2 TERRAIN

Terrain was considered to be flat for this assessment.

D.3.3 DISCRETE/SENSITIVE RECEPTORS

Discrete receptors as well as the same sensitive receptors used in the CAL3QHCR modelling, R1 and R10, were used in this assessment so that model predicted results could be summed with previous CAL3QHCR results to obtain a cumulative concentration at these locations. Recall that R1 is a residential area located west of the GO Barrie (Concord) Station and R10 is a high school located east of Leslie Street at Highway 407 and south of the Transitway. The locations of the discrete receptors are shown by red markers in Figures E.1 and E.2.

Figure D.1 GO Barrie (Concord) Station Modelling Configuration

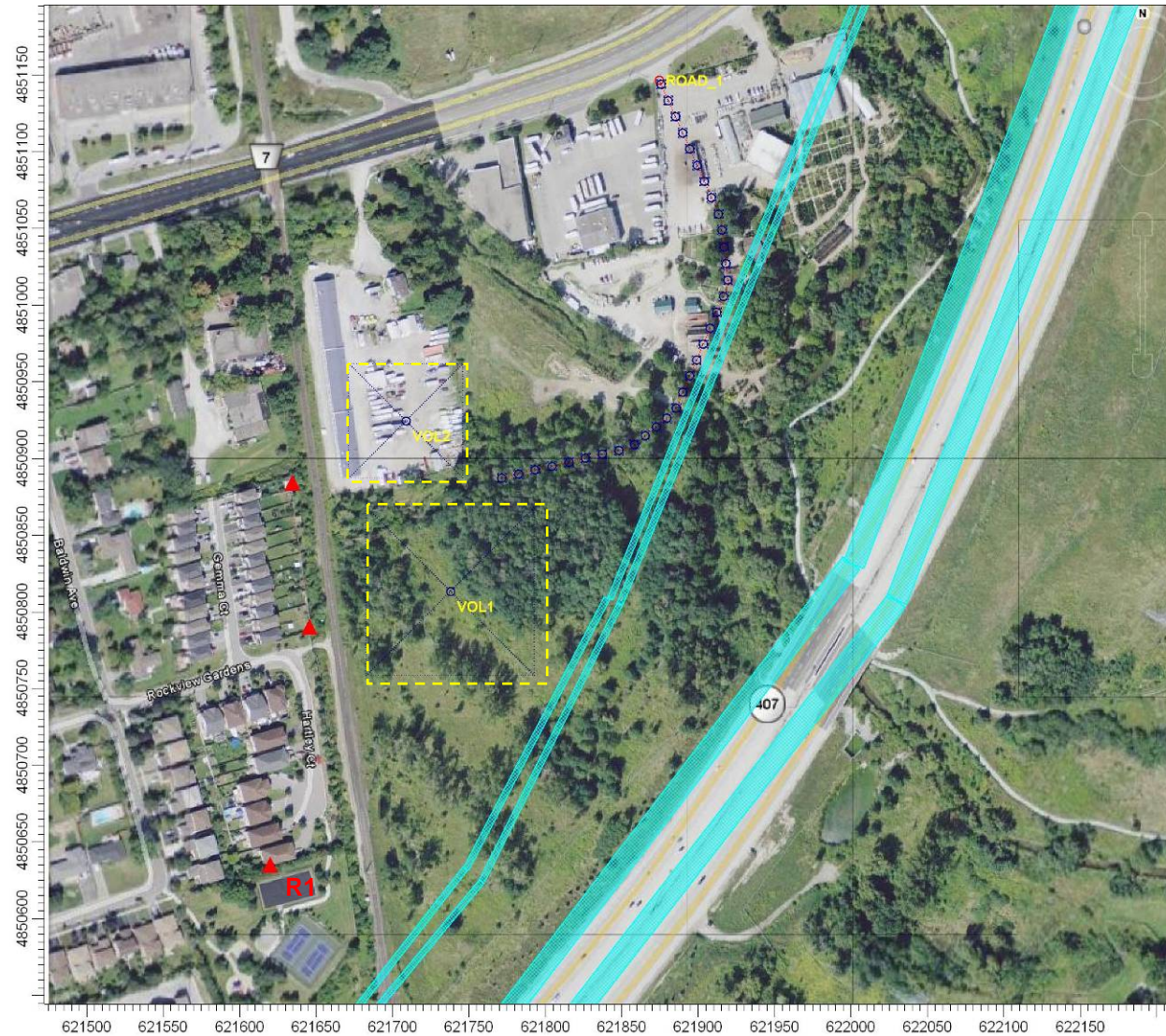
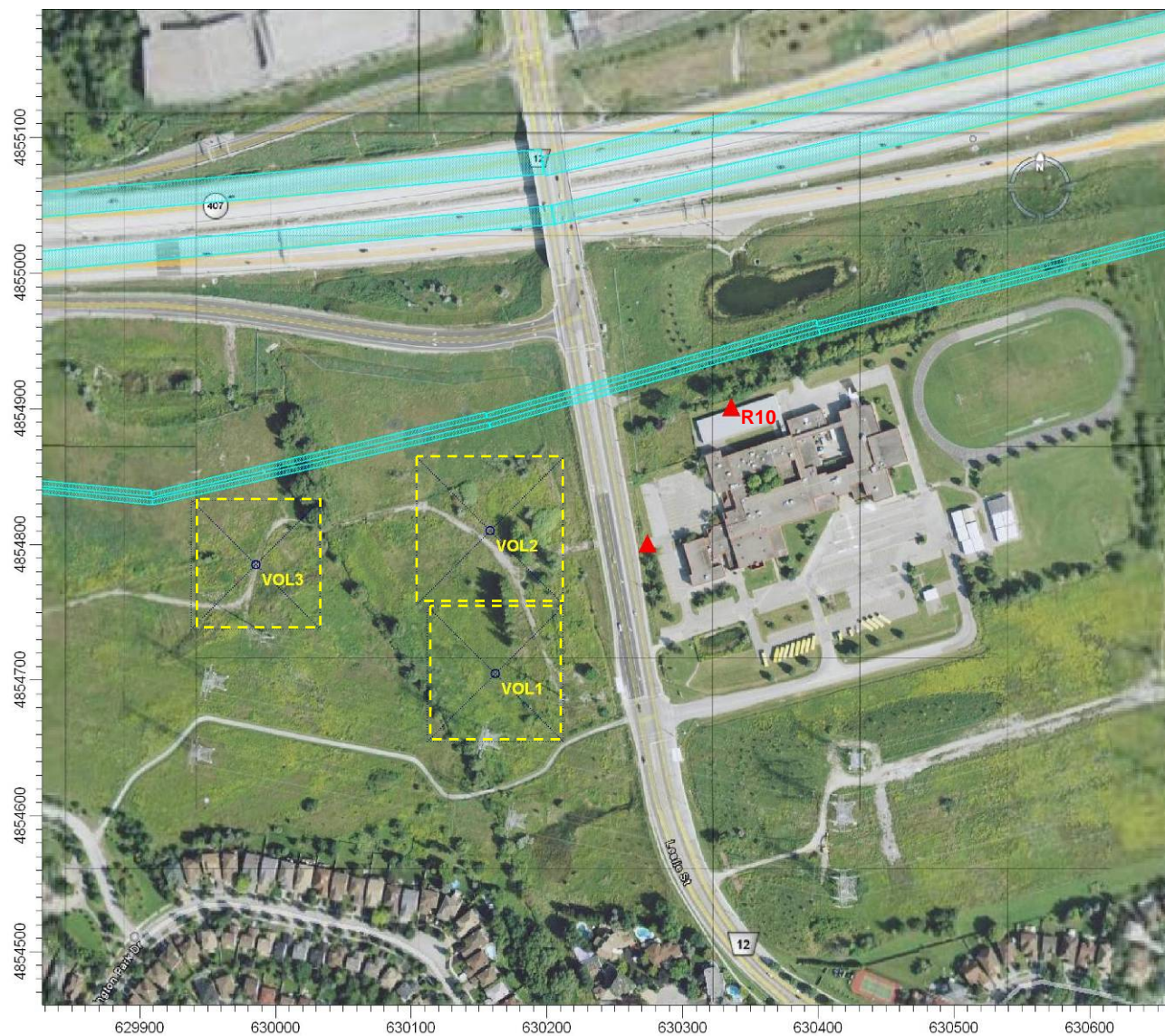


Figure D.2 Leslie Station Modelling Configuration



D.4 RESULTS

The results from the air dispersion modelling have been presented in tabular form for the discrete receptor locations outlined in the above figures.

Results are presented separately for each contaminant.

D.4.1 TABULAR RESULTS – NO_x

Table E.4.2 presents the maximum modelled concentrations of NO_x (1- and 24-hour) at both the GO Barrie (Concord) and Leslie stations. As can be seen in the table, maximum predicted NO_x concentrations for both averaging periods are small at only about 1% of the 1-hour NO_x criteria of 400 µg/m³ and 0.1% of the 24-hour criteria of 200 µg/m³ for both stations. Furthermore, these concentrations are only a fraction of the maximum 1- and 24-hour NO_x concentrations predicted at receptors R1 (GO Barrie (Concord)) and R10 (Leslie). For example, the maximum predicted 24-hour NO_x concentration by the CAL3QHCR modelling at R1 was 105 µg/m³ (Table 5.2), so the addition of GO Barrie (Concord) station emissions would add an insignificant 0.20 µg/m³ or (0.19%) to CAL3QHCR predicted concentrations. Note that the maximum predicted concentrations for each station and the maximums presented in Table 5.2 would not necessarily occur on the same day and therefore represent a worst-case scenario.

In all, the station assessment has shown that the impact of bus station emissions on NO_x levels in the study area, and at sensitive receptors in particular, is insignificant compared CAL3QHCR results. Similarly, the impact on other gases (i.e., CO, VOCs) would also be insignificant.

Table D.4.2 Maximum Modelled 1- and 24-hour NO_x Concentrations

Station	Receptor	Max 1-hr NO _x Concentration (µg/m ³)	Max 24-hr NO _x Concentration (µg/m ³)
GO Barrie (Concord)	Residences on Hartley Crt. (R1)	4.24	0.20
	Residences on south end of Gemma Crt.	4.12	0.25
	Residences on north end of Gemma Crt.	3.53	0.21
Leslie	High School West Property Line	2.5	0.24
	High School North Property Line (R10)	5.0	0.11

D.4.2 TABULAR RESULTS – TSP

Table E.4.3 presents the maximum modelled 24-hour concentrations of TSP at both the GO Barrie (Concord) and Leslie stations. As can be seen in the Table, maximum predicted TSP concentrations are less than approximately 7% of the 24-hour MOE criteria of $120 \mu\text{g}/\text{m}^3$ for both stations. As shown in Tables B.3a and B.3b in Appendix B, the maximum model predicted TSP concentration at R1 was $139 \mu\text{g}/\text{m}^3$ and $181 \mu\text{g}/\text{m}^3$ at R10. Therefore, the stations would increase the concentration by 4% at R1 and by 2% at R10. As noted previously in the NO_x discussion, the maximum predicted concentrations at R1 and R10 for each station assessment and the concentrations predicted by CAL3QHCR would not necessarily occur on the same day and therefore represent a worst-case scenario. Although seemingly insignificant at 4 and 2%, the contribution of the stations to TSP levels may cause additional exceedances since TSP levels were already predicted to be substantially high at R1 and R10 by the CAL3QHCR modelling (Section 5.5). As a result, the cumulative effect of the Transitway and the bus stations were examined in more detail. This analysis is presented below.

Table D.4.3 Maximum Modelled 24-hour TSP Concentrations

Station	Receptor	Max 24-hr TSP Concentration ($\mu\text{g}/\text{m}^3$)
GO Barrie (Concord)	Residences on Hartley Crt. (R1)	5.3
	Residences on south end of Gemma Crt.	7.5
	Residences on north end of Gemma Crt.	8.0
Leslie	High School West Property Line	6.7
	High School North Property Line (R10)	3.2

Refined TSP Station Assessment

To better understand the cumulative effect of the stations on TSP concentrations near the GO Barrie (Concord) and Leslie stations, ISCST3 concentrations for receptors R1 and R10 were summed on a daily basis with CAL3QHCR predicted concentrations for the future scenario (2031) with the Transitway (including background) for 1993.

Table E.4.4 presents the cumulative TSP modelling results for R1 and R10. As can be seen in the table, the maximum 24-hour concentrations and the number of exceedances do not change when ISCST3 daily concentrations are added to CAL3QHCR concentrations. This indicates that the maximum predicted concentrations at R1 and R10 resulting from station emissions did not occur on the same day as the maximums resulting from Transitway emissions. In other words,

this assessment shows that it is conservative to sum the maximum predicted concentrations from the station assessments to the maximum CAL3QHCR concentrations.

Table D.4.4. Cumulative 24-hour TSP Concentrations at R1 and R10

Receptor	Station Only		Future with Transitway		Future with Transitway & Station	
	Max 24-hr Concentration ($\mu\text{g}/\text{m}^3$)	Exceedances	Max 24-hr Concentration* ($\mu\text{g}/\text{m}^3$)	Exceedances	Max 24-hr Concentration* ($\mu\text{g}/\text{m}^3$)	Exceedances
R1	5.3	0	139	21	139	21
R10	3.2	0	174	87	174	87

*Concentration includes a background 24-hr TSP concentration of $70.2 \mu\text{g}/\text{m}^3$

Note: Exceedances based on the 24-hour MOE criteria of $120 \mu\text{g}/\text{m}^3$

Since the refined assessment showed that there were no additional exceedances at R1 and R10 and that the maximum concentrations did not increase when the stations were considered in the Future With Transitway (2031) scenario, it can be concluded that the impact of the bus stations on TSP levels in the study area, and at sensitive receptors in particular, is also insignificant. Similarly, the impact on other particulate size fractions (i.e., PM_{10} and $\text{PM}_{2.5}$) would also be insignificant.

D.5 CONCLUSION

In sum, the station assessment has shown that the impact of bus station parking lots and PPUDO areas on air quality in the study area are negligible compared to the impacts predicted by previous CAL3QHCR modelling. In particular, 24-hour NO_x concentrations increased by less than 0.2% at both R1 and R10 when the GO Barrie (Concord) and Leslie Stations were considered. TSP concentrations were shown to increase by 2% at R10 and 4% at R1 when ISCST3 and CAL3QHCR predicted maximums were summed. However, a refined assessment of TSP showed that these predicted increases were conservative. When predicted concentrations from each model were summed on a daily basis, it was shown that the maximums did not occur on the same day and that there were no additional exceedances predicted at R1 or R10 when station emissions were considered.

As previously discussed, GO Barrie (Concord) Station and Leslie Station were chosen for the station assessment since they were considered to represent the worst-case scenarios due to their close proximity to sensitive areas. Since the impact was determined to be insignificant, it can also be concluded that the remaining five stations (Jane, Bathurst, Yonge, Woodbine/Rodick and Kennedy) would also not significantly increase contaminant concentrations in surrounding areas.

ATTACHMENT A

**EXAMPLE ISCST3 INPUT FILE
(GO Barrie (Concord) – PM)**

Air Quality Impact Assessment for the 407 Transitway (Highway 400 to Kennedy Road)

```

**
*****
**
**
** ISCST3 Input Produced by:
** AERMOD View Ver. 6.4.0
** Lakes Environmental Software Inc.
** Date: 2010/04/28
** File: D:\300000 Projects\34573-2
407ETR\34573-2 Station
Modelling\ISC\GoBarrie\GoBarrie.INP
**
*****
*
**
**
*****
** ISCST3 Control Pathway
*****
*
**
**
CO STARTING
  TITLEONE GO Barrie Stn Modelling
  TITLETWO PM
  MODELOPT DFAULT CONC NOCMPL URBAN
  AVERTIME 24
  POLLUTID TSP
  TERRHGTs FLAT
  RUNORNOT RUN
CO FINISHED
**
*****
*
** ISCST3 Source Pathway
*****
*
**
**
SO STARTING
** Source Location **
** Source ID - Type - X Coord. - Y
Coord. **
  LOCATION VOL1 VOLUME 621738.210
4850813.153
** DESCRSRC 400 parking space lot
  LOCATION VOL2 VOLUME 621708.995
4850924.357
** DESCRSRC 200 parking space lot

** Line Source represented by Separated
Volume Sources
** -----
** LINE Source ID = ROAD_1
** DESCRSRC Entrance road to parking
lots
** Length of Side = 6.00
** Emission Rate = 0.359
** Vertical Dimension = 2.00
** SZINIT = 0.93
** Nodes = 6
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0.0
** 621914.81, 4851056.31, 0.00, 0.00,
5.38
** 621920.07, 4851012.91, 0.00, 0.00,
5.09
** 621884.57, 4850930.07, 0.00, 0.00,
5.25
** 621856.30, 4850907.06, 0.00, 0.00,
4.24
** 621768.85, 4850886.68, 0.00, 0.00,
5.22
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4851133.195
  LOCATION L0000003 VOLUME 621885.330
4851122.630
  LOCATION L0000004 VOLUME 621890.040
4851112.065
  LOCATION L0000005 VOLUME 621894.750
4851101.500
  LOCATION L0000006 VOLUME 621899.460
4851090.935
  LOCATION L0000007 VOLUME 621904.170
4851080.370
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4851059.240
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4851048.603
  LOCATION L0000011 VOLUME 621917.078
4851037.728
  LOCATION L0000012 VOLUME 621918.391
4851026.853

LOCATION L0000013 VOLUME 621919.703
4851015.978
LOCATION L0000014 VOLUME 621916.805
4851005.383
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4850953.508
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4850943.133
LOCATION L0000021 VOLUME 621885.742
4850932.758
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LOCATION L0000023 VOLUME 621872.764
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LOCATION L0000024 VOLUME 621865.701
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LOCATION L0000026 VOLUME 621848.304
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LOCATION L0000027 VOLUME 621837.374
4850902.560
LOCATION L0000028 VOLUME 621826.444
4850899.997
LOCATION L0000029 VOLUME 621815.515
4850897.435
LOCATION L0000030 VOLUME 621804.585
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LOCATION L0000031 VOLUME 621793.655
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LOCATION L0000032 VOLUME 621782.725
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LOCATION L0000033 VOLUME 621771.796
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** End of Line Source
** Source Parameters **
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  SRCPARAM VOL2 0.0724 1.000 17.442
0.465
  SRCPARAM L0000001 0.0108787879 0.00
5.38 0.93

```


Air Quality Impact Assessment for the 407 Transitway (Highway 400 to Kennedy Road)

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 SRCPARAM L0000003 0.0108787879 0.00
 5.38 0.93
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 5.25 0.93
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 5.25 0.93
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 SRCPARAM L0000023 0.0108787879 0.00
 4.24 0.93
 SRCPARAM L0000024 0.0108787879 0.00
 4.24 0.93
 SRCPARAM L0000025 0.0108787879 0.00
 4.24 0.93
 SRCPARAM L0000026 0.0108787879 0.00
 5.22 0.93

SRCPARAM L0000027 0.0108787879 0.00
 5.22 0.93
 SRCPARAM L0000028 0.0108787879 0.00
 5.22 0.93
 SRCPARAM L0000029 0.0108787879 0.00
 5.22 0.93
 SRCPARAM L0000030 0.0108787879 0.00
 5.22 0.93
 SRCPARAM L0000031 0.0108787879 0.00
 5.22 0.93
 SRCPARAM L0000032 0.0108787879 0.00
 5.22 0.93
 SRCPARAM L0000033 0.0108787879 0.00
 5.22 0.93

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 of-Day"
 ** Variable Emission Scenario:
 "Scenario 1"
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 0.0 0.0 0.0 0.0
 EMISFACT L0000002 HROFDY 0.0 0.0 0.0
 0.0 0.0 0.0
 EMISFACT L0000002 HROFDY 0.22 1.0
 0.22 0.0 0.0 0.0
 EMISFACT L0000002 HROFDY 0.0 0.0 0.0
 0.0 0.34 1.0
 EMISFACT L0000002 HROFDY 0.34 0.0
 0.0 0.0 0.0 0.0
 EMISFACT L0000003 HROFDY 0.0 0.0 0.0
 0.0 0.0 0.0
 EMISFACT L0000003 HROFDY 0.22 1.0
 0.22 0.0 0.0 0.0
 EMISFACT L0000003 HROFDY 0.0 0.0 0.0
 0.0 0.34 1.0
 EMISFACT L0000003 HROFDY 0.34 0.0
 0.0 0.0 0.0 0.0
 EMISFACT L0000004 HROFDY 0.0 0.0 0.0
 0.0 0.0 0.0
 EMISFACT L0000004 HROFDY 0.22 1.0
 0.22 0.0 0.0 0.0
 EMISFACT L0000004 HROFDY 0.0 0.0 0.0
 0.0 0.34 1.0
 EMISFACT L0000004 HROFDY 0.34 0.0
 0.0 0.0 0.0 0.0

EMISFACT L0000005 HROFDY 0.0 0.0 0.0
 0.0 0.0 0.0
 EMISFACT L0000005 HROFDY 0.22 1.0
 0.22 0.0 0.0 0.0
 EMISFACT L0000005 HROFDY 0.0 0.0 0.0
 0.0 0.34 1.0
 EMISFACT L0000005 HROFDY 0.34 0.0
 0.0 0.0 0.0 0.0
 EMISFACT L0000006 HROFDY 0.0 0.0 0.0
 0.0 0.0 0.0
 EMISFACT L0000006 HROFDY 0.22 1.0
 0.22 0.0 0.0 0.0
 EMISFACT L0000006 HROFDY 0.0 0.0 0.0
 0.0 0.34 1.0
 EMISFACT L0000006 HROFDY 0.34 0.0
 0.0 0.0 0.0 0.0
 EMISFACT L0000007 HROFDY 0.0 0.0 0.0
 0.0 0.0 0.0
 EMISFACT L0000007 HROFDY 0.22 1.0
 0.22 0.0 0.0 0.0
 EMISFACT L0000007 HROFDY 0.0 0.0 0.0
 0.0 0.34 1.0
 EMISFACT L0000007 HROFDY 0.34 0.0
 0.0 0.0 0.0 0.0
 EMISFACT L0000008 HROFDY 0.0 0.0 0.0
 0.0 0.0 0.0
 EMISFACT L0000008 HROFDY 0.22 1.0
 0.22 0.0 0.0 0.0
 EMISFACT L0000008 HROFDY 0.0 0.0 0.0
 0.0 0.34 1.0
 EMISFACT L0000008 HROFDY 0.34 0.0
 0.0 0.0 0.0 0.0
 EMISFACT L0000009 HROFDY 0.0 0.0 0.0
 0.0 0.0 0.0
 EMISFACT L0000009 HROFDY 0.22 1.0
 0.22 0.0 0.0 0.0
 EMISFACT L0000009 HROFDY 0.0 0.0 0.0
 0.0 0.34 1.0
 EMISFACT L0000009 HROFDY 0.34 0.0
 0.0 0.0 0.0 0.0
 EMISFACT L0000010 HROFDY 0.0 0.0 0.0
 0.0 0.0 0.0
 EMISFACT L0000010 HROFDY 0.22 1.0
 0.22 0.0 0.0 0.0
 EMISFACT L0000010 HROFDY 0.0 0.0 0.0
 0.0 0.34 1.0
 EMISFACT L0000010 HROFDY 0.34 0.0
 0.0 0.0 0.0 0.0
 EMISFACT L0000011 HROFDY 0.0 0.0 0.0
 0.0 0.0 0.0

Air Quality Impact Assessment for the 407 Transitway (Highway 400 to Kennedy Road)

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EMISFACT L0000030 HROFDY 0.0 0.0 0.0
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EMISFACT L0000030 HROFDY 0.22 1.0
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EMISFACT L0000030 HROFDY 0.0 0.0 0.0
0.0 0.34 1.0
EMISFACT L0000030 HROFDY 0.34 0.0
0.0 0.0 0.0 0.0
EMISFACT L0000031 HROFDY 0.0 0.0 0.0
0.0 0.0 0.0
EMISFACT L0000031 HROFDY 0.22 1.0
0.22 0.0 0.0 0.0
EMISFACT L0000031 HROFDY 0.0 0.0 0.0
0.0 0.34 1.0
EMISFACT L0000031 HROFDY 0.34 0.0
0.0 0.0 0.0 0.0
EMISFACT L0000032 HROFDY 0.0 0.0 0.0
0.0 0.0 0.0
EMISFACT L0000032 HROFDY 0.22 1.0
0.22 0.0 0.0 0.0
EMISFACT L0000032 HROFDY 0.0 0.0 0.0
0.0 0.34 1.0
EMISFACT L0000032 HROFDY 0.34 0.0
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EMISFACT L0000033 HROFDY 0.0 0.0 0.0
0.0 0.0 0.0
EMISFACT L0000033 HROFDY 0.22 1.0
0.22 0.0 0.0 0.0
EMISFACT L0000033 HROFDY 0.0 0.0 0.0
0.0 0.34 1.0
EMISFACT L0000033 HROFDY 0.34 0.0
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EMISFACT VOL1 HROFDY 0.0 0.0 0.0 0.0
0.0 0.0
EMISFACT VOL1 HROFDY 0.22 1.0 0.22
0.0 0.0 0.0
EMISFACT VOL1 HROFDY 0.0 0.0 0.0 0.0
0.34 1.0
EMISFACT VOL1 HROFDY 0.34 0.0 0.0
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EMISFACT VOL2 HROFDY 0.0 0.0 0.0 0.0
0.0 0.0
EMISFACT VOL2 HROFDY 0.22 1.0 0.22
0.0 0.0 0.0
EMISFACT VOL2 HROFDY 0.0 0.0 0.0 0.0
0.34 1.0
EMISFACT VOL2 HROFDY 0.34 0.0 0.0
0.0 0.0 0.0
SRCGROUP ROAD_1 L0000001 L0000002
L0000003 L0000004 L0000005 L0000006

```

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SRCGROUP ROAD_1 L0000007 L0000008
L0000009 L0000010 L0000011 L0000012
SRCGROUP ROAD_1 L0000013 L0000014
L0000015 L0000016 L0000017 L0000018
SRCGROUP ROAD_1 L0000019 L0000020
L0000021 L0000022 L0000023 L0000024
SRCGROUP ROAD_1 L0000025 L0000026
L0000027 L0000028 L0000029 L0000030
SRCGROUP ROAD_1 L0000031 L0000032
L0000033
SRCGROUP VOL1 VOL1
SRCGROUP VOL2 VOL2
SRCGROUP ALL
SO FINISHED
**
*****
*
** ISCST3 Receptor Pathway
*****
*
**
**
RE STARTING
** DESCRREC " " " "
DISCCART 621620.10 4850635.02
DISCCART 621645.99 4850789.91
DISCCART 621634.73 4850883.98
RE FINISHED
**
*****
*
** ISCST3 Meteorology Pathway
*****
*
**
**
ME STARTING
INPUTFIL D:\300000~1\34573-
~1\347DB8~1\METDAT~1\Tor93.met
ANEMHGHT 10 METERS
SURFDATA 61587 1993 TORONTO
UAIRDATA 72528 1993
ME FINISHED
**
*****
*
** ISCST3 Output Pathway
*****
*
**
**

```

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OU STARTING
RECTABLE ALLAVE 1ST
RECTABLE 24 1ST
MAXTABLE ALLAVE 100
MAXIFILE 24 ALL 120
GoBarrie.IS\PM24.MAX
POSTFILE 24 ALL PLOT
GoBarrie.IS\93PM.POS
** Auto-Generated Plotfiles
PLOTFILE 24 ALL 1ST
GoBarrie.IS\24H1GALL.PLT
PLOTFILE 24 ROAD_1 1ST
GoBarrie.IS\24H1G001.PLT
PLOTFILE 24 VOL1 1ST
GoBarrie.IS\24H1G002.PLT
PLOTFILE 24 VOL2 1ST
GoBarrie.IS\24H1G003.PLT
OU FINISHED
**
*****
*
** Project Parameters
*****
*
** PROJCTN CoordinateSystemUTM
** DESCPTN UTM: Universal Transverse
Mercator
** DATUM North American Datum 1983
** DTMRGN CONUS
** ZONE 17
**

```


APPENDIX E

RESULTS OF GREENHOUSE GAS BURDEN ANALYSIS

Table E.1 CO₂ Pollutant Burden

Scenario	CO₂ Pollutant Burden in kilotonnes/year	% Change from Existing Conditions in kilotonnes/year
Existing Conditions (2008)	342	-
Future Without Transitway (2031)	628	+84%
Future With Transitway (2031)	626	+83%

Table E.2 CH₄ Pollutant Burden

Scenario	CH₄ Pollutant Burden in tonnes/year	% Change from Existing Conditions in tonnes/year
Existing Conditions (2008)	24	-
Future Without Transitway (2031)	22	-12%
Future With Transitway (2031)	22	-12%

Table E.3 N₂O Pollutant Burden

Scenario	N₂O Pollutant Burden in tonnes/year	% Change from Existing Conditions in tonnes/year
Existing Conditions (2008)	7	-
Future Without Transitway (2031)	12	+76%
Future With Transitway (2031)	12	+76%